FEATURES
Low Cost 3.3 V-CMOS Mixed-Signal Front End (MxFE ${ }^{\text {TM }}$ ) Converter for Broadband Modems 10-/12-Bit D/A Converter (TxDAC+ ${ }^{\circledR}$ )

64/32 MSPS Input Word Rate $2 \times / 4 \times$ Interpolating LPF or BPF Transmit Filter 128 MSPS DAC Output Update Rate Wide ( 26 MHz ) Transmit Bandwidth Power-Down Mode
10-/12-Bit, 50 MSPS A/D Converter
Fourth Order Low-Pass Filter 12 MHz or 26 MHz with Bypass
-6 dB to +36 dB Programmable Gain Amplifier
Internal Clock Multiplier (PLL)
Clock Outputs
Voltage Regulator Controller
48-Lead LOFP Package

## APPLICATIONS

Powerline Networking
Home Phone Networking
xDSL
Broadband Wireless
Home RF

## PRODUCT DESCRIPTION

The AD 9875 is a single supply Broadband modem mixedsignal front end (M xFE) IC. The devices contain a transmit path Interpolation Filter and DAC, and a receive path PGA, LPF and ADC supporting a variety of Broadband modem applications. Also on-chip is a PLL clock multiplier that provides all required clocks from a single crystal or clock input. T he AD 9875 provides 10-bit converter performance on both the $T x$ and $R x$ paths.

The TxDAC + uses a selectable digital $2 \times$ or $4 \times$ interpolation low-pass or band-pass filter to further oversample transmit data and reduce the complexity of analog reconstruction filtering. T he transmit path signal bandwidth can be as high as 26 M Hz at an input data rate of 64 M SPS . The 10-bit DAC provides differential current outputs for optimum noise and distortion performance. The DAC full-scale current can be adjusted from 2 mA to 20 mA by a single resistor, providing 20 dB of additional gain range.
The receive path consists of a PGA, LPF , and ADC. The two-stage PGA has a gain range of -6 dB to +36 dB , and is programmable in 2 dB steps, adding 42 dB of dynamic range to the receive path.

FUNCTIONAL BLOCK DIAGRAM


The receive path LPF cutoff frequency can be programmed to either 12 M Hz or 26 M Hz . The filter cutoff frequency can also be tuned or bypassed where filter requirements differ. The 10-bit ADC uses a multistage differential pipeline architecture to achieve excellent dynamic performance with low power consumption.

The AD 9875 provides a voltage regulator controller (VRC) that can be used with an external power M OSFET transistor to form a cost-effective 1.3 V linear regulator.

The digital transmit and receive ports are each multiplexed to a bus width of $5 / 6$ bits and are clocked at a frequency of twice the 10-bit word rate.

The AD 9875 ADC and/or D AC can also be used at higher sampling rates as high as 64 M SPS in a 5-bit resolution nonmultiplexed mode.

The AD 9875 is pin-compatible with the 12 -bit AD 9876. Both are available in a space-saving 48 -lead LQFP package. They are specified over the industrial $\left(-40^{\circ} \mathrm{C}\right.$ to $\left.+85^{\circ} \mathrm{C}\right)$ temperature range.

[^0]REV. 0
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 $100 \Omega$ DAC single-ended load, unless otherwise noted. )

| Parameter | Temp | Test Level | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OSC IN CHARACTERISTICS <br> Frequency Range Duty Cycle Input C apacitance Input Impedance | $\begin{aligned} & \text { Full } \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \text { II } \\ & \text { II } \\ & \text { III } \\ & \text { III } \end{aligned}$ | $\begin{aligned} & 10 \\ & 40 \end{aligned}$ | $\begin{aligned} & 50 \\ & 3 \\ & 100 \\ & \hline \end{aligned}$ | $\begin{aligned} & 64 \\ & 60 \end{aligned}$ | $\begin{aligned} & \mathrm{MHz} \\ & \% \\ & \mathrm{pF} \\ & \mathrm{M} \Omega \end{aligned}$ |
| CLOCK OUTPUT CHARACTERISTICS CLKA Jitter ( $\mathrm{f}_{\mathrm{CLKA}}$ D erived from PLL) CLKA Duty Cycle CLKB Jitter ( $\mathrm{f}_{\mathrm{CLK}}$ D erived from PLL) CLK B Duty Cycle | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 1 I I \\ & I I I \\ & I I I \\ & I I I \end{aligned}$ |  | $\begin{aligned} & 14 \\ & 50 \pm 5 \\ & 33 \\ & 50 \pm 5 \end{aligned}$ |  | $\begin{aligned} & \text { ps rms } \\ & \% \\ & \text { ps rms } \\ & \% \end{aligned}$ |
| TxCHARACTERISTICS <br> Tx Path L atency, $4 \times$ Interpolation Interpolation Filter Bandwidth ( -0.1 dB ) <br> $4 \times$ Interpolation, LPF <br> $2 \times$ Interpolation, LPF <br> TxDAC <br> Resolution <br> Conversion R ate <br> Full-Scale Output Current <br> Voltage C ompliance Range <br> Gain Error <br> Output Offset <br> Differential Nonlinearity <br> Integral N onlinearity <br> Output C apacitance <br> Phase N oise @ 1 kH z Offset, 10 M Hz Signal <br> Signal-to-N oise and Distortion (SINAD) <br> 10 M Hz Analog Out AD 9875 ( $20 \mathrm{M} \mathrm{Hz} \mathrm{BW)}$ <br> Wideband SF DR (to N yquist, $64 \mathrm{M} \mathrm{Hz} \mathrm{M} \mathrm{ax)}$ <br> 5 M Hz A nalog 0 ut <br> 10 MHz Analog Out <br> N arrowband SFDR (3 M Hz Window): <br> 10 MHz Analog Out <br> IM D (f1 = 6.9 M Hz, f2 = 7.1 M Hz ) | Full <br> Full Full <br> Full Full Full Full Full Full $25^{\circ} \mathrm{C}$ $25^{\circ} \mathrm{C}$ $25^{\circ} \mathrm{C}$ $25^{\circ} \mathrm{C}$ <br> Full $25^{\circ} \mathrm{C}$ $25^{\circ} \mathrm{C}$ $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ $25^{\circ} \mathrm{C}$ | II <br> II <br> II <br> II <br> II <br> II <br> II <br> 11 <br> II <br> III <br> III <br> III <br> III <br> I <br> III <br> III <br> III <br> III <br> III | $\begin{aligned} & 10 \\ & 2 \\ & -0.5 \\ & -5 \\ & 0 \end{aligned}$ | $\begin{aligned} & 82 \\ & 13 \\ & 26 \\ & 10 \\ & 10 \\ & 10 \\ & \pm 2 \\ & 7 \\ & 0.5 \\ & 5 \\ & -90 \\ & \\ & 61 \\ & 78 \\ & 72 \\ & 80 \\ & 80 \\ & -76 \end{aligned}$ | $\begin{aligned} & 128 \\ & 20 \\ & +1.5 \\ & +5 \\ & 19 \\ & 1 \end{aligned}$ | $f_{\text {DAC }}$ Cycles <br> M Hz <br> MHz <br> Bits <br> MHz <br> mA <br> V <br> \% FS <br> $\mu \mathrm{A}$ <br> LSB <br> LSB <br> pF <br> $\mathrm{dBc} / \mathrm{Hz}$ <br> dB <br> dBc <br> dBc <br> dBc <br> dBFS |
| RxPATH CHARACTERISTICS <br> Resolution <br> Conversion Rate <br> Pipeline D elay, ADC Clock C ycles <br> DC Accuracy <br> Differential N onlinearity <br> Integral N onlinearity <br> D ynamic Performance $\left(\mathrm{A}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}, \mathrm{f}=5 \mathrm{M} \mathrm{~Hz}\right)$ <br> @ $\mathrm{f}_{\text {OSCIN }}=32 \mathrm{MHz}$ <br> Signal-to-N oise and Distortion Ratio (SIN AD) <br> Effective N umber of Bits (ENOB) <br> Signal-to-N oise Ratio (SN R) <br> T otal Harmonic D istortion (THD) <br> Spurious Free D ynamic Range (SF DR) <br> D ynamic Performance $\left(\mathrm{A}_{\mathrm{IN}}=-0.5 \mathrm{dBFS}, \mathrm{f}=10 \mathrm{M} \mathrm{~Hz}\right)$ <br> @ $F_{\text {PLLB } / 2}=50 \mathrm{MHz}$ <br> Signal-to-N oise and Distortion Ratio (SINAD) <br> Effective N umber of Bits (EN OB) <br> Signal-to-N oise Ratio (SNR) <br> T otal H armonic D istortion (THD) <br> Spurious Free D ynamic Range (SF D R) | Full Full Full $25^{\circ} \mathrm{C}$ $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ | 11 II <br> II <br> II <br> III <br> III <br> III <br> III <br> III <br> III <br> III <br> III <br> III <br> III | $\begin{aligned} & 7.5 \\ & \\ & -1.0 \\ & -2.0 \end{aligned}$ | 10 <br> 5.5 <br> $\pm 0.25$ <br> $\pm 0.5$ <br> 59.6 <br> 9.5 <br> 60 <br> -65 <br> 68 <br> 54 <br> 8.6 <br> 55 <br> -61 <br> 68 | $\begin{aligned} & 55 \\ & \\ & +1.0 \\ & +2.0 \end{aligned}$ | Bits <br> M Hz <br> Cycles <br> LSB <br> LSB <br> dB <br> Bits <br> dB <br> dB <br> dB <br> dB <br> Bits <br> dB <br> dB <br> dB |


| Parameter | Temp | Test Level | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Rx PATH GAIN/OFFSET <br> M inimum Programmable $G$ ain $M$ aximum Programmable $G$ ain <br> ( $12 \mathrm{M} \mathrm{H} \mathrm{z} \mathrm{F} \mathrm{ilter)}$ <br> (26 M Hz F ilter) <br> G ain Step Size <br> G ain Step Accuracy <br> Gain Range Error Offset Error, PGA Gain = $0 \mathrm{~dB}($ AD 9875) Absolute Gain Error, PGA Gain $=0 \mathrm{~dB}$ | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | III <br> III <br> III <br> III <br> III <br> III <br> III <br> III |  | $\begin{aligned} & -6 \\ & \\ & 36 \\ & 30 \\ & 2 \\ & \pm 0.4 \\ & \pm 1.0 \\ & \pm 4.0 \\ & \pm 0.8 \end{aligned}$ |  | dB <br> dB <br> dB <br> dB <br> dB <br> dB <br> LSB <br> dB |
| Rx PATH INPUT CHARACTERISTICS <br> Input Voltage Range <br> Input C apacitance <br> Differential Input Resistance <br> Input Bandwidth (-3 dB) <br> Input Referred $N$ oise (at +36 dB Gain with Filter) Input Referred N oise (at -6 dB Gain with Filter) Common-M ode Rejection | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | III <br> III <br> III <br> III <br> III <br> III <br> III |  | $\begin{aligned} & 4 \\ & 4 \\ & 270 \\ & 50 \\ & 16 \\ & 684 \\ & 40 \end{aligned}$ |  | Vppd pF $\Omega$ M Hz $\mu \mathrm{V}$ rms $\mu \mathrm{V}$ rms dB |
| Rx PATH LPF (Low Cutoff Frequency) <br> Cutoff Frequency <br> Cutoff F requency Variation <br> Attenuation @ 22 MHz <br> Passband Ripple <br> Group Delay Variation <br> Settling Time (to $1 \% \mathrm{FS}, \mathrm{M}$ in to M ax G ain C hange) <br> Total Harmonic Distortion at M ax G ain (THD) | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | III <br> III <br> III <br> III <br> III <br> III <br> III |  | $\begin{aligned} & 12 \\ & \pm 7 \\ & 20 \\ & \pm 1.0 \\ & 30 \\ & \\ & 150 \\ & -68 \end{aligned}$ |  | M Hz <br> \% <br> dB <br> dB <br> ns <br> ns <br> dBc |
| Rx PATH LPF (H igh C utoff F requency) <br> Cutoff Frequency <br> Cutoff F requency Variation <br> Attenuation @ 44 MHz <br> Passband Ripple <br> Group Delay Variation <br> Settling Time <br> (to $1 \% \mathrm{FS}, \mathrm{M}$ in to M ax G ain C hange) <br> T otal H armonic Distortion at M ax G ain (THD) | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | III <br> III <br> III <br> III <br> III <br> III <br> III |  | $\begin{aligned} & 26 \\ & \pm 7 \\ & 20 \\ & \pm 1.2 \\ & 15 \\ & 80 \\ & -65 \end{aligned}$ |  | M Hz <br> \% <br> dB <br> dB <br> ns <br> ns <br> dBc |
| RxPATH DIGITAL HPF <br> Latency (ADC Clock Source Cycles) <br> Roll-Off in Stopband $-3 d B$ Frequency | Full Full Full | $\begin{aligned} & \text { II } \\ & \text { II } \end{aligned}$ |  | $\begin{aligned} & 1 \\ & 6 \\ & f_{\mathrm{ADC}} / 400 \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \text { Cycle } \\ & \text { dB/Octave } \\ & \mathrm{Hz} \end{aligned}$ |
| ```RxPATH DISTORTION PERFORMANCE IM D: f1 = 6.9 M Hz,f2 = 7.1 M Hz 12 M Hz Filter: 0 dB : 30 dB 28 M Hz Filter: 0 dB : 30 dB``` | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \text { III } \\ & \text { III } \\ & \text { III } \\ & \text { III } \end{aligned}$ |  | $\begin{aligned} & -65 \\ & -57 \\ & -65 \\ & -56 \end{aligned}$ |  | dBc <br> dBc <br> dBc <br> dBc |
| POWER-DOWN/DISABLETIMING <br> Power-U p D elay (Power-D own-to-Active) <br> DAC <br> PLL <br> ADC <br> PGA <br> LPF <br> Interpolator <br> VRC <br> M inimum RESET Pulsewidth Low ( $\mathrm{t}_{\text {RL }}$ ) <br> DAC Iout Off after Tx QUIET Asserted <br> DAC Iout On after TxQUIET D easserted <br> Power-D own Delay (Active-to-Power-D own) <br> DAC <br> Interpolator | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & \text { Full } \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & 11 \\ & \text { II } \\ & \text { II } \\ & \text { II } \\ & \text { II } \\ & \text { II } \\ & 1 I \\ & I I \\ & I I \\ & I I \end{aligned}$ |  |  | $\begin{aligned} & 40 \\ & 10 \\ & 1000 \\ & 1 \\ & 1 \\ & 200 \\ & 2 \\ & 5 \\ & 200 \\ & 1 \\ & 400 \\ & 200 \end{aligned}$ | $\mu S$ $\mu S$ $\mu S$ $\mu S$ $\mu S$ ns $\mu \mathrm{S}$ $\mathrm{f}_{\text {OSCIN }}$ Cycle ns $\mu \mathrm{S}$ ns ns |
| REV. 0 |  | - |  |  |  |  |

AD9875- SPECIFICATIONS ${ }_{\text {(cortinued) }}$

| Parameter | Temp | Test Level | Min | Typ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TxPATH INTERFACE <br> M aximum Input N ibble R ate, $2 \times$ Interp. <br> Tx-Set Up Time ( $\mathrm{t}_{\mathrm{su}}$ ) <br> Tx-H old Time ( $\mathrm{t}_{\mathrm{HD}}$ ) | $\begin{aligned} & \text { Full } \\ & \text { Full } \\ & \text { Full } \end{aligned}$ | $\begin{aligned} & \text { II } \\ & \text { II } \\ & \text { II } \end{aligned}$ | $\begin{aligned} & 128 \\ & 3.0 \\ & 0 \end{aligned}$ |  |  | M Hz <br> ns <br> ns |
| RxPATH INTERFACE <br> M aximum Output Nibble Rate <br> Rx-D ataValid Time ( $\mathrm{t}_{\mathrm{vT}}$ ) <br> Rx-D ata H old Time ( $\mathrm{t}_{\mathrm{HT}}$ ) | Full <br> Full <br> Full | $\begin{aligned} & \text { I } \\ & \text { II } \\ & \text { II } \end{aligned}$ | $\begin{aligned} & 110 \\ & 1.5 \end{aligned}$ |  | 3.0 | M Hz ns ns |
| CMOS LOGIC INPUTS Logic "1" Voltage Logic " 0 " Voltage Logic "1" Current Logic "0" Current Input C apacitance | Full Full Full Full $25^{\circ} \mathrm{C}$ | $\begin{aligned} & 11 \\ & 11 \\ & I I \\ & I I \\ & I I I \end{aligned}$ | $\mathrm{V}_{\text {DRVD }}$ | 3 | $\begin{aligned} & 0.4 \\ & 12 \\ & 12 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mu \mathrm{~A} \\ & \mu \mathrm{~A} \\ & \mu \mathrm{~F} \end{aligned}$ |
| CMOS LOGIC OUTPUTS (1 mA Load) <br> Logic "1" Voltage <br> Logic "0" Voltage <br> Digital Output Rise/F all T ime | Full <br> Full <br> Full | $\begin{aligned} & \text { II } \\ & \text { II } \\ & \text { II } \end{aligned}$ | $\begin{aligned} & V_{\text {DRVD }} \\ & 1.5 \end{aligned}$ |  | $\begin{aligned} & 0.4 \\ & 2.5 \end{aligned}$ | $\begin{aligned} & \text { V } \\ & \text { V } \end{aligned}$ ns |
| ```POWER SUPPLY All Blocks Powered Up Is_total (T otal Supply Current) Is_total (Tx_QUIET Pin Asserted) D ígital Supply C urrent (I IRVDD + I IVDDD Analog Supply Current (I IVDD ) Power Consumption of Functional Blocks: RxLPF ADC and FPGA Rx R eference Interpolator DAC PLL-B PLL-A Voltage R egulator C ontroller All Blocks Powered D own Supply Current IS, foscin = 32 M Hz Supply Current Is, foscin Idle Power Supply R ejection Tx Path ( }\Delta\mp@subsup{\textrm{V}}{5}{}=\pm10% Rx Path ( }\Delta\mp@subsup{V}{S}{}=\pm10%``` | Full $25^{\circ} \mathrm{C}$ $25^{\circ} \mathrm{C}$ $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ <br> Full <br> Full <br> $25^{\circ} \mathrm{C}$ <br> $25^{\circ} \mathrm{C}$ | I <br> III <br> III <br> III <br> III <br> III <br> III <br> III <br> III <br> III <br> III <br> III <br> II <br> II <br> III <br> III |  | $\begin{aligned} & 262 \\ & 172 \\ & 77 \\ & 185 \\ & 110 \\ & 55 \\ & 2 \\ & 33 \\ & 18 \\ & 8 \\ & 24 \\ & 1 \end{aligned}$ | $288$ $22$ $12$ | mA <br> mA <br> mA <br> mA <br> mA <br> mA <br> mA <br> mA <br> mA <br> mA <br> mA <br> mA <br> mA <br> mA <br> $d B$ <br> dB |
| SERIAL CONTROL BUS <br> M aximum SCLK Frequency ( $\mathrm{f}_{\mathrm{SCLK}}$ ) <br> Clock Pulsewidth High ( $\mathrm{t}_{\mathrm{pwH}}$ ) <br> Clock Pulsewidth Low ( $\mathrm{t}_{\text {pw }}$ ) <br> Clock Rise/F all T ime <br> D ata/C hip-Select Setup Time ( $\mathrm{t}_{\mathrm{D}}$ ) <br> D ata H old Time ( $\mathrm{t}_{\mathrm{DH}}$ ) <br> D ata Valid Time ( $\mathrm{t}_{\mathrm{DV}}$ ) | Full <br> Full <br> Full <br> Full <br> Full <br> Full <br> Full | II II II II II II II | $\begin{aligned} & 25 \\ & 18 \\ & 18 \\ & 25 \\ & 0 \end{aligned}$ |  | 1 20 | M Hz <br> ns <br> ns <br> ms <br> ns <br> ns <br> ns |
| RECEIVE-TO-TRANSMIT ISOLATION <br> ( 10 M Hz, Full-Scale Sinewave Output/Output) <br> Isolation: Tx Path to Rx Path, G ain $=+36 \mathrm{~dB}$ <br> Isolation: Rx Path to $T \times$ Path, $G$ ain $=-6 \mathrm{~dB}$ | $\begin{aligned} & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \end{aligned}$ | $\begin{aligned} & \text { III } \\ & \text { III } \end{aligned}$ |  | $\begin{aligned} & -75 \\ & -70 \end{aligned}$ |  | $\begin{aligned} & \mathrm{dB} \\ & \mathrm{~dB} \end{aligned}$ |
| VOLTAGE REGULATOR CONTROLLER Output Voltage ( $\mathrm{V}_{\mathrm{FB}}$ with SI2301 C onnected) Line Regulation ( $\Delta \mathrm{V}_{\mathrm{FB} \%} / \Delta \mathrm{V}_{\text {DVDD\% }} \times 100 \%$ ) Load Regulation ( $\Delta \mathrm{V}_{\mathrm{FB}} / \Delta \mathrm{I}_{\text {LOAD }}$ ) M aximum Load C urrent (I LOAD) | $\begin{aligned} & \text { Full } \\ & 25^{\circ} \mathrm{C} \\ & 25^{\circ} \mathrm{C} \\ & \text { Full } \end{aligned}$ | $\begin{aligned} & \text { I } \\ & \text { III } \\ & \text { III } \\ & \text { II } \end{aligned}$ | $\begin{aligned} & 1.25 \\ & 250 \end{aligned}$ | $\begin{aligned} & 1.30 \\ & 100 \\ & 60 \end{aligned}$ | 1.35 | $\begin{aligned} & \mathrm{V} \\ & \% \\ & \mathrm{~m} \Omega \\ & \mathrm{~mA} \end{aligned}$ |

[^1]ABSOLUTE MAXIMUM RATINGS*
Power Supply ( $\mathrm{V}_{\mathrm{S}}$ ) ..... 3.9 V
Digital Output Current ..... 5 mA
Digital Inputs . . . . . . . . . . . . . . . . . -0.3 V to DRVDD 0.3 V
Analog Inputs ..... -0.3 V to AVDD 0.3 V
O perating T emperature ..... $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$
M aximum Junction T emperature ..... $150^{\circ} \mathrm{C}$
Storage T emperature

$\qquad$
$65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$
Lead Temperature (Soldering 10 sec ) ..... $300^{\circ} \mathrm{C}$
*Stresses greater than those listed under Absolute M aximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## EXPLANATION OF TEST LEVELS

I - D evices are $100 \%$ production tested at $25^{\circ} \mathrm{C}$ and guaranteed by design and characterization testing for industrial operating temperature range $\left(-40^{\circ} \mathrm{C}\right.$ to $\left.+85^{\circ} \mathrm{C}\right)$.
II - Parameter is guaranteed by design and/or characterization testing.
III - Parameter is a typical value only.
THERMAL CHARACTERISTICS

## Thermal Resistance

```
48-L ead L QF P
    0JA}=5\mp@subsup{7}{}{\circ}\textrm{C}/\textrm{W
    0\mp@code{ C }=2\mp@subsup{8}{}{\circ}\textrm{C}/\textrm{W}
```


## ORDERING GUIDE

| Model | Temperature Range | Package Description | Package Option |
| :--- | :--- | :--- | :--- |
| AD 9875BST | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | $48-$ L ead LQFP | ST-48 |
| AD 9875-EB | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | Evaluation B oard |  |
| AD 9875BST RL | $-40^{\circ} \mathrm{C}$ to $+85^{\circ} \mathrm{C}$ | BST Reel |  |

## CAUTION

ESD (electrostatic discharge) sensitive device. Electrostatic charges as high as 4000 V readily accumulate on the human body and test equipment and can discharge without detection. Although the AD9875 features proprietary ESD protection circuitry, permanent damage may occur on devices subjected to high-energy electrostatic discharges. Therefore, proper ESD precautions are recommended to avoid performance degradation or loss of functionality.

## PIN FUNCTION DESCRIPTIONS

| Pin | Name | Function |
| :---: | :---: | :---: |
| 1 | OSCIN | C rystal Oscillator Inverter Input |
| 2 | SENABLE | Serial Bus Enable Input |
| 3 | SCLK | Serial Bus Clock Input |
| 4 | SDATA | Serial Bus D ata I/O |
| 5, 38, 47 | AVDD | Analog 3.3 V Power Supply |
| 6, 9, 39, 42, 43, 46 | AVSS | Analog Ground |
| 7 | Tx+ | T ransmit D AC + Output |
| 8 | Tx- | T ransmit DAC-O utput |
| 10 | FSADJ | DAC Full-Scale Output Current Adjust with External Resistor |
| 11 | REFIO | DAC Bandgap D ecoupling N ode |
| 12 | PWR DN | Power-D own Input |
| 13 | DVSS | Digital Ground |
| 14 | DVDD | Digital 3.3 V Power Supply |
| 15 | FB | Regulator F eedback Input |
| 16 | GATE | Regulator Output to FET G ate |
| 17 | GAIN | T ransmit D ata Port (Tx[5:0]) M ode Select Input |
| 18 | Tx QUIET | T ransmit Quiet Input |
| 19-24 | Tx[5:0] | T ransmit D ata Input |
| 25 | Tx SYNC | T ransmit Synchronization Strobe Input |
| 26 | CLK-A | L $\times$ foscin Clock Output |
| 27 | CLK-B | $\mathrm{M} / \mathrm{N} \times \mathrm{foscin}$ Clock Output |
| 28 | Rx SYNC | Receive D ata Synchronization Strobe Output |
| 29-34 | Rx[5:0] | Receive D ata Output |
| 35 | DRVDD | Digital I/O 3.3 V Power Supply |
| 36 | DRVSS | Digital I/O Ground |
| 37 | RESET | Reset Input |
| 40 | REFB | ADC R eference D ecoupling N ode |
| 41 | REFT | ADC R eference D ecoupling N ode |
| 44 | Rx+ | Receive Path + Input |
| 45 | Rx- | Receive Path - Input |
| 48 | XTAL | Crystal Oscillator Inverter Output |

## PIN CONFIGURATION



## DEFINITIONS OF SPECIFICATIONS <br> CLOCK JITTER

The clock jitter is a measure of the intrinsic jitter of the PLL generated clocks. It is a measure of the jitter from one rising and of the clock with respect to another edge of the clock nine cycles later.

## DIFFERENTIAL NONLINEARITY ERROR (DNL, NO MISSING CODES)

An ideal converter exhibits code transitions that are exactly 1 LSB apart. DNL is the deviation from this ideal value. Guaranteed no missing codes to 10-bit resolution indicates that all 1024 codes respectively, must be present over all operating ranges.

## INTEGRAL NONLINEARITY ERROR (INL)

Linearity error refers to the deviation of each individual code from a line drawn from "negative full scale" through "positive full scale." The point used as "negative full scale" occurs 1/2 LSB before the first code transition. "positive full scale" is defined as a level 1 1/2 LSB beyond the last code transition. The deviation is measured from the middle of each particular code to the true straight line.

## PHASE NOISE

Single-sideband phase noise power density is specified relative to the carrier ( $\mathrm{dBc} / \mathrm{Hz}$ ) at a given frequency offset ( 1 kHz ) from the carrier. Phase noise can be measured directly on a generated single tone with a spectrum analyzer that supports noise marker measurements. It detects the relative power between the carrier and the offset ( 1 kHz ) sideband noise and takes the resolution bandwidth (rbw) into account by subtracting $10 \log (r b w)$. It also adds a correction factor that compensates for the implementation of the resolution bandwidth, log display and detector characteristic.

## OUTPUT COMPLIANCE RANGE

The range of allowable voltage at the output of a current-output DAC. Operation beyond the maximum compliance limits may cause either output stage saturation, resulting in nonlinear performance or breakdown.

## SPURIOUS-FREE DYNAMIC RANGE (SFDR)

The difference, in dB , between the rms amplitude of the DACs output signal (or ADC's input signal) and the peak spurious signal over the specified bandwidth ( N yquist bandwidth unless otherwise noted).

## PIPELINE DELAY (LATENCY)

The number of clock cycles between conversion initiation and the associated output data being made available.

## OFFSET ERROR

First transition should occur for an analog value $1 / 2 \mathrm{LSB}$ above negative full scale. Offset error is defined as the deviation of the actual transition from that point.

## GAIN ERROR

The first code transition should occur at an analog value $1 / 2 \mathrm{LSB}$ above negative full scale. The last transition should occur for an analog value 1 1/2 LSB below the nominal full scale. G ain error is the deviation of the actual difference between first and last code transitions and the ideal difference between first and last code transitions.

## INPUT REFERRED NOISE

The RM S output noise is measured using histogram techniques. The ADC output codes' standard deviation is calculated in LSB, and converted to an equivalent voltage. This results in a noise figure that can be directly referred to the Rx input of the AD 9875.

## SIGNAL-TO-NOISE AND DISTORTION RATIO (SINAD)

SINAD is the ratio of the RM S value of the measured input signal to the RMS sum of all other spectral components below the $N$ yquist frequency, including harmonics but excluding dc . The value for SINAD is expressed in decibels.

## EFFECTIVE NUMBER OF BITS (ENOB)

For a sine wave, SIN AD can be expressed in terms of the number of bits. $U$ sing the following formula,

$$
N=(S I N A D-1.76) d B / 6.02
$$

it is possible to get a measure of performance expressed as $N$, the effective number of bits.

## SIGNAL-TO-NOISE RATIO (SNR)

SNR is the ratio of the rms value of the measured input signal to the rms sum of all other spectral components below the $N$ yquist frequency, excluding harmonics and dc. The value for SNR is expressed in decibels.

## TOTAL HARMONIC DISTORTION (THD)

THD is the ratio of the rms sum of the first six harmonic components to the rms value of the measured input signal and is expressed as a percentage or in decibels.

## POWER SUPPLY REJECTION

Power Supply Rejection specifies the converters maximum full-scale change when the supplies are varied from nominal to minimum and maximum specified voltages.


TPC 1. $4 \times$ Low-Pass Interpolation Filter


TPC 2. $2 \times$ Low-Pass Interpolation Filter


TPC 3. $4 \times$ Bandpass Interpolation Filter, $f_{S} / 2$ Modulation, Adjacent Image Preserved


TPC 4. $2 \times$ Bandpass Interpolation Filter, $f_{S} / 2$ Modulation, Adjacent Image Preserved


TPC 5. $4 \times$ Bandpass Interpolation Filter, $f_{S} / 4$ Modulation, Lower Image Preserved


TPC 6. $4 \times$ Bandpass Interpolation Filter, $f_{S} / 4$ Modulation, Upper Image Preserved

## Typical AC Characteristics Curves for TxDAC ( Rsfr $\left.=4.02 \kappa \Omega, R_{\text {ooc }}=100 \Omega\right)$



TPC 7. Single Tone Spectral Plot @ $f_{\text {DATA }}=32$ MSPS, $f_{\text {OUT }}=5 \mathrm{MHz}, 4 \times L P F$


TPC 8. Single Tone Spectral Plot @ $f_{D A T A}=50 \mathrm{MSPS}$, $f_{\text {OUT }}=11 \mathrm{MHz}, 2 \times L P F$


TPC 9. "In Band" SFDR vs. $f_{\text {OUT }} @ f_{D A T A}=32$ MSPS and 50 MSPS


TPC 10. "Out of Band" SFDR vs. $f_{\text {OUT }} @ f_{\text {DATA }}=32$ MSPS and 50 MSPS


TPC 11. Dual Tone Spectral Plot @ $f_{\text {DATA }}=32$ MSPS, $f_{\text {OUT }}=6.9 \mathrm{MHz}$ and $7.1 \mathrm{MHz}, 4 \times L P F$


TPC 12. Dual Tone Spectral Plot @ $f_{\text {DATA }}=50$ MSPS, $f_{\text {OUT }}=6.9 \mathrm{MHz}$ and $7.1 \mathrm{MHz}, 2 \times L P F$

Typical AC Characteristics Curves for TXDAC (Rsst $\left.=4.02 \mathrm{k} \Omega, \mathrm{R}_{\mathrm{OLC}}=10.0 \Omega\right)$


TPC 13. Phase Noise Plot @ $f_{\text {DATA }}=32 \mathrm{MSPS}$, $f_{\text {OUT }}=10 \mathrm{MHz}, 4 \times$ LPF


TPC 14. Phase Noise Plot @ $f_{\text {DATA }}=50 \mathrm{MSPS}$, $f_{\text {OUT }}=10 \mathrm{MHz}, 2 \times L P F$


TPC 15. "In Band" Multitone Spectral Plot $@ f_{\text {DATA }}=50 \mathrm{MSPS}, f_{\text {OUT }}=k \times 195 \mathrm{kHz}, 2 \times$ LPF


TPC 16. "Wide-Band" Multitone Spectral Plot $@ f_{D A T A}=50 \mathrm{MSPS}, f_{O U T}=k \times 195 \mathrm{kHz}, 2 \times \operatorname{LPF}$

## Typical AC Characterization Curves for Rx Path



TPC 17. Rx vs. Tuning Target, $f_{A D C}=32 \mathrm{MHz}, L P F$ with Wideband Rx LPF = 1


TPC 18. PGA Gain Error vs. Gain


TPC 19. $f_{C}$ vs. Tuning Target, $f_{A D C}=32 \mathrm{MHz}, L P F$ with Wideband $R x L P F=0$


TPC 20. PGA Gain Step Size vs. Gain

## Typical AC Characterization Curves for Rx Path (fox (foc $=32 \mathrm{Mzz})$



TPC 21. Rx LPF Frequency Response, Low $f_{C}$ Nominal Tuning Targets


TPC 22. Rx LPF Frequency Response, High $f_{C}$ Nominal Tuning Targets


TPC 23. Rx LPF Frequency Response, Low $f_{C}, 0 \times 60$ and $0 \times 96$ Tuning Targets


TPC 24. Rx LPF Group Delay, Low $f_{C}$ Nominal Tuning Targets


TPC 25. Rx LPF Group Delay, High $f_{C}$, Nominal Tuning Targets


TPC 26. Rx LPF Group Delay, Low $f_{C}, 0 \times 60$ and $0 \times 96$ Tuning Targets

## Typical AC Characterization Curves for Rx Path (foc $\left.{ }_{\text {(foc }}=32 \mathrm{MHz}\right)$



TPC 27. Rx LPF Frequency Response, High $f_{C}, 0 \times 60$ and $0 \times 96$ Tuning Targets


TPC 28. Rx HPF Frequency Response, $f_{A D C}=32 \mathrm{MHz}$


TPC 29. Rx Path Setting, 1/2 Scale Rising Step with Gain Change


TPC 30. Rx LPF Group Delay, High $f_{C}, 0 \times 60$ and $0 \times 96$ Tuning Targets


TPC 31. Rx Input Referred Noise vs. Gain @ $f_{A D C}=32$ MSPS, $f_{I N}=1 \mathrm{MHz}$


TPC 32. Rx Path Setting, 1/2 Scale Falling Step with Gain Change

Typical AC Characterization Curves for Rx Path (Gain= $\left.=6 \mathrm{~dB}, \mathrm{f}_{\mathrm{f}}=5 \mathrm{MHz}\right)$


TPC 33. Rx Path ENOB vs. $f_{A D C}$


TPC 36. Rx Path ENOB vs. $f_{I N}$


TPC 39. Rx Path ENOB vs. Gain


TPC 34. Rx Path SNR vs. $f_{A D C}$


TPX 37. Rx Path SNR vs. $f_{I N}$


TPC 40. Rx Path SNR vs. Gain


TPC 35. Rx Path THD vs. $f_{A D C}$


TPC 38. Rx Path THD vs. $f_{I N}$


TPC 41. Rx Path THD vs. Gain

## TRANSMIT PATH

The AD 9875 transmit path consists of a Digital Interface Port, a Programmable Interpolation Filter, and a T ransmit DAC. All clock signals required by these blocks are generated from the $\mathrm{f}_{\text {OSCIN }}$ signal by the PLL-A clock generator. The block diagram below shows the interconnection between the major functional components of the transmit path.


Figure 1. Transmit Path Block Diagram

## DIGITAL INTERFACE PORT

The transmit Digital Interface Port has several modes of operation. In its default configuration, the Tx Port accepts six bit nibbles through the Tx[5:0] and TxSYNC pins and demultiplexes the data into 12 -bit words before passing it to the Interpolation Filter. The input data is sampled on the rising edge of $f_{C L K-A}$.
Additional programming options for the T x Port allow; sampling the input data on the falling edge of $f_{C L K-A}$, inversion or disabling of $\mathrm{f}_{\text {CLK-A }}$, reversing the order of the nibbles, and inputting nibble widths of 5 bits/5 bits. Also, the Tx Port interface can be controlled by the GAIN pin to provide direct access to the Rx Path Gain Adjust register. All of these modes are fully described in the Register Programming D efinitions section of this data sheet.
T he data format is two's complement, as shown below:

```
011 . . 11: M aximum
000 . . 01: M idscale + 1 LSB
000 . . 00: M idscale
111 . .11: M idscale - 1 LSB
111 . . 10: M idscale - 2 LSB
100 . . 00: M inimum
```

The data can be translated to straight binary data format by simply inverting the most significant bit.
The timing of the interface is fully described in the T ransmit T iming section of this data sheet.

## PLL-A CLOCK DISTRIBUTION

Figure 1 shows the clock signals used in the transmit path. The DAC sampling clock, $f_{D A C}$, is generated by DPLL-A. $f_{D A C}$ has a frequency equal to $L \times f_{\text {OSCIN }}$, where $f_{\text {OSCIN }}$ is the internal signal generated either by the crystal oscillator when a crystal is connected between the OSCIN and XTAL pins, or by the clock that is fed into the OSCIN pin, and $L$ is the multiplier programmed through the serial port. $L$ can have the values of $1,2,4$, or 8.

The transmit path expects a new half-word of data at the rate of $f_{\text {CLK-A }}$. When the $T x$ multiplexer is enabled, the frequency of the Tx port is:

$$
f_{C L K-A}=2 \times f_{D A C} / K=2 \times L \times f_{O S C I N} / K
$$

where $K$ is the interpolation factor that can be programmed to be 1,2 , or 4 .

When the Tx multiplexer is disabled, the frequency of the Tx port is:

$$
f_{C L K-A}=f_{D A C} / K=L \times f_{O S C I N} / K
$$

## INTERPOLATION FILTER

The interpolation filter can be programmed to run at $2 \times$ and $4 \times$ upsampling ratios in each of three different modes. The transfer functions of these six configurations are shown in T PC s 1-6. The X -axis of each of these figures corresponds to the frequency normalized to $f_{\text {DAC }}$. These transfer functions show both the discrete time transfer function of the interpolation filters alone and with the $\operatorname{SIN}(x) / x$ transfer function of the DAC. The Interpolation Filter can also be programmed into a pass-through mode if no interpolation filtering is desired.
The contents of the interpolation filters are not cleared by hardware or software resets. It is recommended to "flush" the transmit data path with zeros before transmitting data.
Table I contains the following parameters as a function of the mode that it is programmed:
Latency - the number of clock cycles from the time a digital impulse is written to the DAC until the peak value is output at the $T x \pm$ pins.
Flush - the number of clock cycles from the time a digital impulse is written to the DAC until the output at the $T x \pm$ pins settles to zero.
$f_{\text {Lower }}(0.1 \mathrm{~dB}, 3 \mathrm{~dB})$ - This indicates the lower 0.1 dB or 3 dB cutoff frequency of the interpolation filter as a fraction of $f_{D A C}$, the DAC sampling frequency.
$f_{\text {upper }}(0.1 \mathrm{~dB}, 3 \mathrm{~dB}$ ) - This indicates the upper 0.1 dB or 3 dB cutoff frequency of the interpolation filter as a fraction of $f_{D A C}$, the DAC sampling frequency.

Table I. Interpolation Filter Parameters vs. Mode

| Register 7[7:4] | $0 \times 0$ | $0 \times 1$ | $0 \times 4$ | $0 \times 5$ | $0 \times 8$ | $0 \times \mathbf{C}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M ode | $4 \times$ LPF | $2 \times$ LPF | $4 \times$ BPF | $2 \times \mathrm{BPF}$ | $4 \times$ BPF | $4 \times$ BPF |
|  |  |  | Adj. | Adj. | Lower | U pper |
| L atency, $\mathrm{f}_{\mathrm{DAC}}$ Clock Cycles | 86 | 30 | 86 | 30 | 86 | 86 |
| Flush, $\mathrm{f}_{\mathrm{DAC}}$ Clock Cycles | 128 | 48 | 128 | 48 | 142 | 142 |
| $\mathrm{f}_{\text {Lower, }} 0.1 \mathrm{~dB}$ | 0 | 0 | 0.398 | 0.276 | $\begin{aligned} & 0.148 / \\ & 0.774 \end{aligned}$ | $\begin{aligned} & 0.274 / \\ & 0.648 \end{aligned}$ |
| $\mathrm{f}_{\text {UPPER, }} 0.1 \mathrm{~dB}$ | 0.102 | 0.204 | 0.602 | 0.724 | $\begin{aligned} & 0.226 / \\ & 0.852 \end{aligned}$ | $\begin{array}{\|l\|l} 0.352 / \\ 0.762 \end{array}$ |
| flower, 3 dB | 0 | 0 | 0.381 | 0.262 | $\begin{aligned} & 0.131 / \\ & 0.757 \end{aligned}$ | $\left\lvert\, \begin{array}{l\|l\|} 0.257 / \\ 0.631 \end{array}\right.$ |
| $f_{\text {UPPER, }} 3 \mathrm{~dB}$ | 0.119 | 0.238 | 0.619 | 0.738 | $\begin{array}{\|l\|} \hline 0.243 / \\ 0.869 \end{array}$ | $\begin{aligned} & 0.369 / \\ & 0.743 \end{aligned}$ |

## AD9875

## D/A CONVERTER

The AD 9875 DAC provides differential output current on the $T x+$ and $T x-$ pins. The value of the output currents are complimentary, meaning that they will always sum to $I_{F S}$, the full-scale current of the DAC. For example, when the current from $T x+$ is at full-scale, the current from $T x$ - is zero. The two currents will typically drive a resistive load which will convert the output currents to a voltage. The T x+ and Tx-output currents are inherently ground seeking and should each be connected to matching resistors, $R_{L}$, that are tied directly to AGND.
The full-scale output current of the DAC is set by the value of the resistor placed from the FSADJ pin to AGND. The relationship between the resistor, $\mathrm{R}_{\text {SET }}$, and the full-scale output current is governed by the following equation:

$$
I_{F S}=39.4 / R_{S E T}
$$

The full-scale current can be set from 2 mA to 20 mA . Generally, there is a trade-off between D AC performance and power consumption. The best DAC performance will be realized at an $I_{F S}$ of 20 mA . H owever, the value of $\mathrm{I}_{F S}$ adds directly to the overall current consumption of the device.
The single-ended voltage output appearing at the $T x+$ and $T x-$ nodes are:

$$
\begin{aligned}
& V_{T X+}=I_{T X+} \times R_{L} \\
& V_{T x-}=I_{T x-} \times R_{L}
\end{aligned}
$$

$N$ ote that the full-scale voltage of $\mathrm{V}_{T X+}$ and $\mathrm{V}_{T x-}$ should not exceed the maximum output compliance range of 1.5 V to prevent signal compression. T o maintain optimum distortion and linearity performance, the maximum voltages at $\mathrm{V}_{T x+}$ and $\mathrm{V}_{\mathrm{Tx}}$ should not exceed 0.5 V .

The single ended full-scale voltage at either output node will be:

$$
V_{F S}=I_{F S} \times R_{L}
$$

The differential voltage, $\mathrm{V}_{\mathrm{DIFF}}$, appearing across $\mathrm{V}_{\mathrm{T}_{\mathrm{X}}+}$ and $\mathrm{V}_{\mathrm{Tx}-}$ is:

$$
\begin{gathered}
V_{\text {DIFF }}=\left(I_{T X+}-I_{T X-}\right) \times R_{L} \\
\text { and } \\
V_{D_{\text {DIFF_FS }}}=I_{F S} \times R_{L}
\end{gathered}
$$

For optimum performance, a differential output interface is recommended since any common-mode noise or distortion can be supressed.
It should be noted that the differential output impedance of the DAC is $2 \times R_{L}$ and any load connected across the two output resistors will load down the output voltage accordingly.

## RECEIVE PATH DESCRIPTION

The receive path consists of a two-stage PGA, a continuous time, 4-pole LPF, an ADC, a digital HPF and a digital data multiplexer. Also working in conjunction with the receive path is an offset correction circuit and a digital phase lock loop. E ach of these blocks will be discussed in detail in the following sections.

## PROGRAMMABLE GAIN AMPLIFIER

The PGA has a programmable gain range from -6 dB to +36 dB if the narrower (approximately 12 MHz ) LPF bandwidth is
selected, or if the LPF is bypassed. If the wider (approximately 26 M Hz ) LPF bandwidth is selected, the gain range is -6 dB to +30 dB . The PGA is comprised of two sections, a C ontinuous Time PGA (CPGA) and a Switched C apacitor PGA (SPGA). The CPGA has possible gain settings of $-6,0,6,12,18$, and 24 . TheSPGA has possible gain settings of $0,2,4,6,8,10$, and 12 dB . T able I shows how the gain is distributed for each programmed gain setting.
The CPGA input appears at the device $R x+$ and $R x$ - input pins. The input impedance of this stage is nominally $270 \Omega$ differential and is not gain dependent. It is best to ac-couple the input signal to this stage and let the inputs self bias. This will lower the offset voltage of the input signal, which is important at higher gains, as any offset will lower the output compliance range of the CPGA output. When the inputs are driven by direct coupling, the dc level should be AVDD/2. H owever, this could lead to larger dc offsets and consequently reduce the dynamic range of the Rx path.

## LOW-PASS FILTER

T he Low-Pass Filter (LPF) is a programmable, multistage, fourth order low-pass filter comprised of two real poles and a complex pole pair. The first real pole is implemented within the C PGA. The second filter stage implements a complex pair of poles. T he last real pole is implemented in a buffer stage that drives the SPGA.

There are two passband settings for the LPF. Within each passband the filters are tunable over about a $\pm 30 \%$ frequency range. $T$ he formula for the cutoff frequency is:

$$
\begin{aligned}
\mathrm{f}_{\text {CUTOFF LOW }} & =\mathrm{f}_{\mathrm{ADC}} \times 64 /(64+\text { Target }) \\
\mathrm{f}_{\text {CUTOFF HIGH }} & =\mathrm{f}_{\mathrm{ADC}} \times 158 /(64+\text { Target })
\end{aligned}
$$

Where $T$ arget is the decimal value programmed as the tuning target in Register 5.
This filter may also be bypassed by setting Bit 0 of Register 4. In this case, the bandwidth of the Rx path will decrease with increasing gain and be approximately 50 M Hz at the highest gain settings.

## ADC

The AD 9875's analog-to-digital converter implements a pipelined multistage architecture to achieve high sample rates while consuming low power. The ADC distributes the conversion over several smaller A/D subblocks, refining the conversion with progressively higher accuracy as it passes the results from stage to stage. As a consequence of the distributed conversion, ADCs require a small fraction of the $2^{\mathrm{N}}$ comparators used in a traditional n-bit flash-type A/D. A sample-and-hold function within each of the stages permits the first stage to operate on a new input sample while the remaining stages operate on preceding samples. Each stage of the pipeline, excluding the last, consists of a low resolution flash A/D connected to a switched capacitor DAC and interstage residue amplifier (M DAC). The residue amplifier amplifies the difference between the reconstructed DAC output and the flash input for the next stage in the pipeline. One bit of redundancy is used in each one of the stages to facilitate digital correction of flash errors. The last stage simply consists of a flash A/D.


Figure 2. ADC Theory of Operation
The digital data outputs of the ADC are represented in two's complement format. T hey saturate to full-scale or zero when the input signal exceeds the input voltage range.
The two's complement data format is shown below:

```
011 . . 11: M aximum
000 . . 01: M idscale + 1 L SB
000 . . 00: M idscale
111.. 11: M idscale - 1 LSB
111 . . 10: M idscale - 2 LSB
100 . . 00: M inimum
```

The $M$ aximum value will be output from the ADC when the $R x+$ input is $1 V$ or more greater than the $R x$ - input. The M inimum value will be output from the ADC when the Rx-input is 1 V or more greater than the $\mathrm{R} x+$ input. This results in a full-scale ADC voltage of 2 Vppd .
The data can be translated to straight binary data format by simply inverting the most significant bit.
The best ADC performance will be achieved when the ADC clock source is selected from $f_{\text {OSCIN }}$ and $f_{\text {OScIN }}$ is provided from a low jitter clock source. The amount of degradation from jitter on the ADC clock will depend on how quickly the input is varying at the sampling instance. T PC 36 charts this effect in the form of $E N O B$ vs. input frequency for the two clocking scenarios.
The maximum sample rate of the ADC in full-precision mode, that is outputting 10 bits, is 55 MSPS . TPC 33 shows the ADC performance in $E N O B$ vs. $f_{A D C C L K}$. The maximum sample rate of the ADC in half-precision mode, that is outputting five bits, is 64 M SPS . The timing of the interface is fully described in the Receive T iming section of this data sheet.

## DIGITAL HPF

Following the ADC there is a bypassable digital HPF. The response is a single pole IIR HPF. The transfer function is approximately:

$$
H(z)=(Z-0.99994) /(Z-0.98466)
$$

Where the sampling period is equal to the ADC clock period. This results in a 3 dB frequency approximately $1 / 400$ th of the ADC sampling rate. The transfer functions are plotted for 32 M SPS and 50 M SPS in TPC 31 and TPC 32.
The digital HPF introduces a 1 ADC clock cycle latency. If the HPF function is not desired, the HPF can be bypassed and the latency will not be incurred.

## CLOCK AND OSCILLATOR CIRCUITRY

T he AD 9875's internal oscillator generates all sampling clocks from a fundamental frequency quartz crystal. Figure 3a shows how the quartz crystal is connected between OSCIN (Pin 1) and XTAL (Pin 48) with parallel resonant load capacitors as specified by the crystal manufacturer. The internal oscillator circuitry can also be overdriven by a T TL level clock applied to OSCIN with XTAL left unconnected.
The PLL has a frequency capture range between 10 M Hz and 64 M Hz .

## VOLTAGE REGULATOR CONTROLLER

The AD 9875 contains an on-chip voltage regulator controller (VRC) for providing a linear 1.3 V supply for low voltage digital circuitry or other external use. T he VRC consists of an op amp and a resistive voltage divider. As shown in $F$ igure $3 b$, the resistive divider establishes a voltage of 1.3 V at the inverting input of the amplifier when DVDD is equal to its nominal voltage of 3.3 V. The feedback loop around the op amp will adjust the gate voltage such that the voltage at the FB pin, $\mathrm{V}_{\mathrm{FB}}$, will be equal to the voltage at the inverting input of the op amp.


Figure 3a. Connections for Fundamental Mode Crystal


Figure 3b. Connections for a 1.3 V Linear Regulator The maximum current output from the circuit is largely dependent on the M OSFET device. For the SI2301 shown, 250 mA can be delivered. The regulated output voltage should have bulk decoupling and high frequency decoupling capacitors to ground as required by the load. The regulator circuit will be stable for capacitive loads between $0.1 \mu \mathrm{~F}$ and $47 \mu \mathrm{~F}$.
It should be noted that the regulated output voltage, $\mathrm{V}_{\mathrm{FB}}$, is proportional to DVDD. Therefore, the percentage variation in DVDD will also be seen at the regulated output voltage. The load regulation is roughly equal to the on resistance of the M OSFET device chosen. For the SI2301, this is about $60 \mathrm{~m} \Omega$.

## AD9875

## AGC TIMING CONSIDERATIONS

When implementing the AGC timing loop it is important to consider the delay and settling time of the Rx path in response to a change in gain. Figure 4 shows the delay the receive signal experiences through the blocks of the Rx path. Whether the gain is programmed through the serial port or over the TX[5:0] pins, the gain takes effect immediately with the delays shown below. When gain changes do not involve the CPGA, the new gain will be evident in samples after seven ADC clock cycles. When the gain change does involve the CPGA, it takes an additional 45 ns to 70 ns due to the propagation delays of the buffer, LPF and PGA. Table III, in the Register Programming section, details the PGA programming map.


Figure 4. AGC Timing

## Transmit Port Timing

The AD 9875 transmit port consists of a 6-bit data bus T x[5:0], a clock and a Tx SYNC signal. T wo consecutive nibbles of the $\mathrm{T} x$ data are multiplexed together to form a 10-bit data word. The clock appearing on the CLK-A pin is a buffered version of the internal $T x$ data sampling clock. D ata from the $T \times$ port is read on the rising edge of this sampling clock. The Tx SYNC signal is used to indicate to which word a nibble belongs. The first nibble of every word is read while Tx SYNC is low, the second nibble of that same word is read on the following $T x$ SY NC high level. The timing is illustrated in the Figure 5.


Figure 5. Transmit Timing Diagram AD9875
The Tx port is highly configurable and offers the following options:
N egative edge sampling can be chosen by two different methods; either by setting the Tx Port $N$ egative Edge Sampling bit (Register 3, Bit 7) or the Invert CLK-A bit (Register 8, Bit 6). The main difference between the two methods is that setting Register 3, Bit 7 inverts the internal sampling clock and will affect only the transmit path, even if CLK -A is used to clock the Rx data. Inverting CLK-A would affect both the Rx and $T x$ paths if they both use CLK-A.
The first nibble of each word can be read in as the least significant nibble by setting the Tx LS N ibbleF irst bit (Register 7, Bit 2).
For the AD 9875, the most significant nibble defaults to six bits and the least significant nibble defaults to form four bits. This can be changed so that the least significant nibble and most significant nibble have five bits each. This is done by setting the Tx Port W idth F ive B its bit (Register 7, Bit 1). In all cases, the nibbles are justified toward Bit 5.

Also, the $T x$ path can be used in a reduced resolution mode by setting the Tx Port M ultiplexer B ypass bit (Register 7, Bit 0). In this mode the $T x$ data word becomes six bits and is read in a single cycle. The clocking modes are the same as described above, but the level of TxSYNC is irrelevant.
If Tx SYNC is low for more than one clock cycle, the last transmit data will read continuously until Tx SY N C is brought high for the second nibble of a new transmit word. T his feature can be used to "flush" the interpolator filters with zeros.

## PGA Gain Adjust Timing

In addition to the serial port, the $T \times[5: 1]$ pins can be used to write to the Rx Path G ain Adjust bits (Register 6, Bits 4:0). This provides a faster way to update the PGA gain. A high level on the GAIN pin with T $\times$ SYNC low programs the PGA setting on the rising edge of CLK-A. A low level on the GAIN pin enables data to be fed to the interpolator and DAC. The GAIN pin must be held high, the Tx SY N C must be held low, and the GAIN data must be stable for three clock cycles to successfully update the PGA GAIN value.
It should be noted that Tx SYNC must be held low and Tx GAIN must be held high to update the gain register. If Tx GAIN and Tx SYNC are both high, no data is written to the gain register of the $T x$ data path.


Figure 6. GAIN Programming

## Receive Port Timing

The AD 9875 receives port consists of a six bit data bus Rx[5:0], a clock and an Rx SYNC signal. T wo consecutive nibbles of the $R x$ data are multiplexed together to form a 10-bit data word. The $R x$ data is valid on the rising edge of CLK-A when the ADC Clock Source PLL-B/2 bit (Register 3, Bit 6) is set to 0 . The Rx SY NC signal is used to indicate to which word a nibble belongs. The first nibble of every word is transmitted while $R x$ SYNC is low, the second nibble of that same word is transmitted on the following Rx SYNC high level. When RxSYNC is low, the sampled nibble is read as the most significant nibble. When the Rx SYNC is high, the sampled nibble is read as the least significant nibble. The timing is illustrated in Figure 7.


Figure 7. Receive Timing Diagram
The Rx port is highly configurable and offers the following options:
N egative edge sampling can be chosen by setting the Invert CLK-A bit (Register 8, Bit 6) or the Invert CLK-B bit (Register 8, Bit 7), depending on the clock selected as the ADC sampling source. Inverting CLK-A would affect the Tx sampling edge as well as the Rx sampling edge.
The first nibble of each word can be read in as the least significant nibble by setting the Rx LS N ibble F irst bit (Register 8, Bit 2).

For the AD 9875, the most significant nibble defaults to six bits and the least significant nibble defaults to four bits. This can be changed so that the least significant nibble and most significant nibble have five bits each. This is done by setting the $R \times$ Port Width Five B its bit (Register 8, Bit 1). In all cases, the nibbles are justified toward Bit 5.
Also, the Rxpath can be used in a reduced resolution mode by setting the Rx Port M ultiplexer Bypass bit (Register 8, Bit 0). In this mode the Rx data word becomes six bits and is read in a single cycle. The clocking modes are the same as described above, but the level of Rx SYN C will stay low.
The $R x[5: 0]$ pins can be put into a high impedance state by setting the $T$ hree State $R x$ P ort bit (Register 8, Bit 3).

## SERIAL INTERFACE FOR REGISTER CONTROL

The serial port is a three wire serial communications port consisting of a clock (SCLK), chip select ( $\overline{\text { SENABLE }}$ ), and a bidirectional data (SDATA) signal. T he interface allows read/write access to all registers that configure the AD 9875 internal parameters. Single or multiple byte transfers are supported as well as M SB first or LSB first transfer formats.

## General Operation of the Serial Interface

Serial communication over the serial interface can be from 1 to 5 bytes in length. The first byte is always the instruction byte. T he instruction byte establishes whether the communication is going to be a read or write access, the number of data bytes to be transferred and the address of the first register to be accessed. The instruction byte transfer is complete immediately upon the eighth rising edge of SCLK after $\overline{\text { SENABLE }}$ is asserted. Likewise, the data registers change immediately upon writing to the eighth bit of each data byte.

## Instruction Byte

The instruction byte contains the following information as shown below:

Table II. Instruction Byte Information
MSB

| 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R/W | N1 | N0 | A4 | A3 | A2 | A1 | A0 |

## Bitl7-R/W

This bit determines whether a read or a write data transfer will occur after the instruction byte write. Logic high indicates read operation; logic zero indicates a write operation.

## Bits I6:I5-N1:N0

T hese two bits determine the number of bytes to be transferred during the data transfer cycle. The bit decodes are shown in the table below:

## Table III. Decode Bits

| N1:N0 | Description |
| :--- | :--- |
| $0: 0$ | Transfer 1 Byte |
| $0: 1$ | Transfer 2 Bytes |
| $1: 0$ | Transfer 3 Bytes |
| 1:1 | Transfer 4 Bytes |

## Bits 14:10-A4:A0

These bits determine which register is accessed during the data transfer portion of the communications cycle. F or multibyte transfers, this address is the starting byte address. The remaining register addresses are generated by the AD 9875.

## Serial Interface Port Pin Description <br> SCLK—Serial Clock

The serial clock pin is used to synchronize data transfers to and from the AD 9875 and to run the internal state machines. SCLK maximum frequency is 25 M Hz . All data transmitted to the AD 9875 is sampled on the rising edge of SCLK. All data read from the AD 9875 is validated on the rising edge of SCLK and is updated on the falling edge.

## SENABLE-Serial Interface E nable

The $\overline{\text { SENABLE }}$ pin is active low. It enables the serial communication to the device. $\overline{\text { SENABLE }}$ select should stay low during the entire communication cycle. All input on the serial port is ignored when SENABLE is inactive.

## SDATA-Serial Data I/O

The signal on this line is sampled on the first eight rising edges of SCLK after SENABLE goes active. D ata is then read from or written to the AD 9875 depending on what was read.
Figures 8 and 9 show the timing relationships between the three SPI signals.


Figure 8. Timing Diagram Register Write to AD9875/AD9876


Figure 9. Timing Diagram Register Read from AD9875/AD9876

## MSB/LSB Transfers

The AD 9875 serial port can support both most significant bit (M SB) first or least significant bit (LSB) first data formats. The bit order is controlled by the SPI LSB First bit (Register 0, Bit 6). The default is value is $0, M$ SB first. $M$ ultibyte data transfers in M SB format can be completed by writing an instruction byte that includes the register address of the last address to be accessed. The AD 9875 will automatically decrement the address for each successive byte required for the multibyte communication cycle.
When the SPI LSB First bit (Register 0, Bit 6) is set high, the serial port interprets both instruction and data bytes LSB first. M ultibyte data transfers in LSB format can be completed by writing an instruction byte that includes the register address of the first address to be accessed. The AD 9875 will automatically increment the address for each successive byte required for the multibyte communication cycle.

Figures 10a and 10b show how the serial port words are built for each of these modes.


Figure 10a. Serial Register Interface Timing MSB-First


Figure 10b. Serial Register Interface Timing LSB-First

## Notes on Serial Port Operation

The serial port is disabled and all registers are set to their default values during a hardware reset. D uring a software reset, all registers except register 0 are set to their default values. Register 0 will remain at the last value sent, with the exception that the Software R eset bit will be set to 0 .
The serial port is operated by an internal state machine and is dependent on the number of SCLK cycles since the last time SENABLE went active. On every eighth rising edge of SCLK, a byte is transferred over the SPI. D uring a multibyte write cycle, this means the registers of the AD 9875 are not simultaneously updated, but occur sequentially. For this reason, it is recommended that single byte transfers be used when changing the SPI configuration or performing a software reset.

Table IV. Register Layout

| Address (hex) | Bit 7 | Bit 6 | Bit 5 | Bit 4 | Bit 3 | Bit 2 | Bit 1 | Bit 0 | Default (hex) | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 |  | SPI LSB First | Software Reset |  |  |  |  |  | $0 \times 00$ | Read/W rite |
| 1 | Power- <br> D own <br> Regulator | PowerDown PLL-B | PowerDown PLL-A | PowerDown DAC | Power- <br> Down Interpolator | Power- <br> D own <br> Rx <br> Reference | Power- <br> D own <br> ADC and FPGA | Power- <br> Down <br> RxLPF and CPGA | $0 \times 00$ | Read/W rite PWR DN Pin Low |
| 2 | Power- <br> Down Regulator | PowerDown PLL-B | PowerDown PLL-A | PowerDown DAC | PowerDown Interpolator | Power- <br> D own <br> Rx <br> Reference | PowerDown ADC and FPGA | Power- <br> Down <br> RxLPF and CPGA | $0 \times 9 \mathrm{~F}$ | Read/W rite PWR DN Pin High |
| 3 | Tx Port N egative Edge Sampling | ADC Clock Source PLL-B/2 | $\begin{aligned} & \text { PLL-E } \\ & (\times M) \\ & <5: 4= \end{aligned}$ | M ultiplier | $\begin{aligned} & \text { PLL-B } \\ & \text { (/N)D } \\ & <3: 3> \end{aligned}$ | vider |  | M ultiplier | $0 \times 02$ | Read/W rite |
| 4 | Tx Port Tuning U pdate D isable | RxLPF Tuning In Progress (Read Only) | Rx Path DC Offset Correction | RxDigital HPF Bypass | Fast ADC <br> Sampling | Wideband RxLPF | $\begin{aligned} & \hline \text { Enable } \\ & \text { 1-Pole } \\ & \text { Rx LPF } \end{aligned}$ | RxLPF <br> Bypass | $0 \times 01$ | Read/W rite |
| 5 | Rx LPF Fc Adjust <4:0> |  |  |  |  |  |  |  | $0 \times 80$ | Read/W rite |
| 6 |  |  | PGA Gain Set by Register | Rx Path G ain Adjust <4:0> |  |  |  |  | $0 \times 00$ | Read/W rite |
| 7 | Interpolation Filter Select$<3: 0\rangle$ |  |  |  | Power-D own Interpolator at TxQUIET Pin Low | Tx Port LS Nibble F irst | Tx Port Width 5-bits | Tx Port M ultiplexer Bypass | $0 \times 00$ | Read/W rite |
| 8 | Invert CLK B | Invert CLK B | Invert CLK B | Invert CLK B | Three-State Rx Port | Rx Port LS Nibble First | Rx Port Width 5-bits | Rx Port M ultiplexer Bypass | $0 \times 00$ | Read/W rite |
| F |  |  |  |  | Die Revision N umber <3:0> |  |  |  |  | Read Only |

## REGISTER PROGRAMMING DEFINITIONS <br> REGISTER 0-RESET/SPI Configuration <br> Bit 5: Software Reset

Setting this bit high resets the chip. The PLLs will relock to the input clock and all registers (except Register $0 \times 0$, Bit 6) revert to their default values. U pon completion of the reset, Bit 5 is reset to 0 .

The content of the interpolator stages are not cleared by software or hardware resets. It is recommended to "flush" the transmit path with zeros before transmitting data.

## Bit 6: LSB/MSB First

Setting this bit high causes the serial port to send and receive data least significant bit (LSB) first. The default low state configures the serial port to send and receive data most significant bit (M SB) first.

## RE GISTERS 1 and 2-Power-Down

The combination of the PWR D N pin and Registers 1 and 2 allow for the configuration of two separate pin selectable power settings. The PWR DN pin selects between two sets of individually programmed operation modes.
When the PWR DN pin is low, the functional blocks corresponding to the bits set in register 1 will be powered down.
When the PWR DN pin is high, the functional blocks corresponding to the bits set in Register 2 will be powered down

## Bit 0: Power-Down Receive Filter and CPGA

Setting this bit high powers down and bypasses the RxLPF and coarse programmable gain amplifier.

## Bit 1: Power-Down ADC and FPGA

Setting this bit high powers down the ADC and fine programmable gain amplifier (FPGA).

## Bit 2: Power-Down Rx Reference

Setting this bit high powers down the ADC reference. This bit should be set if an external reference is applied.

## B it 3: Power-Down Interpolators

Setting this bit high powers down the transmit digital interpolators. It does not clear the content of the data path.

## Bit 4: Power-Down DAC

Setting this bit high powers down the transmit DAC.

## Bit 5, Bit 6: Power-Down PLL-A, PLL-B

Setting these bits high powers down the on-chip phase lock loops which generated CLK-A and CLK-B respectively. When powered down these clocks are high impedance.

## Bit 7: Power-Down Regulator

Setting this bit high powers down the on-chip voltage control regulator.

## REGISTER 3-CLOCK SOURCE CONFIGURATION

T he AD 9875 integrates two independently programmable PLLs referred to as PLL-A and PLL-B. The output of the PLLs are used to generate all the chips internal and external clock signals from the $\mathrm{f}_{\text {CLKIN }}$ signal. All T x path clock signals are derived from PLL-A. If $f_{C L K I N}$ is programmed as the ADC sampling clock source, the Rx port clocks are also derived from PLL-A. Otherwise, the ADC sampling clock is PLL-B/2 and the Rxpath clocks are derived from PLL-B.

## Bit 1,0: PLL-A Multiplier

Bits 1 and 0 determine the multiplication factor (L) for PLL-A and the DAC sampling clock frequency, $f_{D A C}$.

$$
f_{D A C}=L \times f_{C L K I N}
$$

Bit 1,0
$0,0: L=1$
$0,1: L=2$
1,0: L = 4
1,1: L = 8

## Bit 5 to 2: PLL-B Multiplier/Divider

Bits 5 to 2 determine the multiplication factor ( M ) and division factor ( N ) for PLL-B and the CLK-B frequency. For multiplexed $10-/ 12$-bit data, $\mathrm{f}_{\mathrm{CLK}-\mathrm{B}}=\mathrm{f}_{\mathrm{CLKIN}} \times \mathrm{M} / \mathrm{N}$. F or nonmultiplexed 6-bit data, $f_{C L K-B}=\left(f_{C L K I N} / 2\right) \times M / N$. All nine combinations of $M$ and $N$ values are valid, yielding seven unique $\mathrm{M} / \mathrm{N}$ ratios.

Bit 5,4
Bit 3,2

| $0,0: M=3$ | $0,0: N=2$ |
| :--- | :--- |
| $0,1: M=4$ | $0,1: N=4$ |
| $1,0: M=6$ | $1,0: N=1$ |

## Bit 6: ADC Clock Source PLL-B/2

Setting Bit 6 high selects PLL-B/2 as the ADC sampling Clock source. In this mode, the Rx data and $\mathrm{CLK}-\mathrm{B}$ will run at a rate of $f_{C L K-B}$. RxSYNC will run at $f_{\text {CLK-B }} / 2$.
Setting Bit 6 low selects the $\mathrm{f}_{\text {CLKIN }}$ signal as the ADC sampling clock source. This mode of operation yields the best ADC performance if an external crystal is used or a low jitter clock source drives the OSCIN pin.

## Bit 7: Tx Port Negative Edge Sampling

Setting Bit 7 high will cause the $T x$ port to sample the TxDATA and $T$ xSY N C on the falling edge of CLK-A. By default, the $T x$ Port sampling occurs on the rising edge of CLK-A. The timing is shown in Figure 5.

## REGISTER 4-RECEIVE FILTER SELECTION

The AD 9875 receive path has a continuous time 4-pole LPF and a 1-pole digital HPF. The 4-pole LPF has two selectable cutoff frequencies. Additionally, the filter can be tuned around those two cutoff frequencies. These filters can also be bypassed to different degrees as described below.
The continuous time 4-pole low-pass filter is automatically calibrated to one of two selectable cutoff frequencies.
The cutoff frequency $\mathrm{f}_{\text {CUTOFF }}$ is described as a function of the ADC sampling frequency $f_{A D C}$ and can be influenced ( $\pm 30 \%$ ) by the Rx-Filter Tuning $T$ arget word in Register 5.

$$
\begin{aligned}
\mathrm{f}_{\text {CUTOFF LOW }} & =\mathrm{f}_{\mathrm{ADC}} \times 64 /(\text { Target }+64) \\
\mathrm{f}_{\text {CUTOFF HIGH }} & =\mathrm{f}_{\mathrm{ADC}} \times 158 /(\text { Target }+64)
\end{aligned}
$$

## Bit 0: Rx LPF Bypass

Setting this bit high bypasses the 4-pole LPF. The filter is automatically powered down when this bit is set.

## Bit 1: Enable 1-Pole Rx LPF

The AD 9875 can be configured with an additional 1-pole $\sim 16 \mathrm{M} \mathrm{Hz}$ input filter for applications that require steeper filter roll-off or want to use the 1 -pole filter instead of the 4 -pole receive Low-Pass filter. The 1-pole filter is untrimmed and subject to cutoff frequency variations of $\pm 20 \%$.

## Bit 2: Wideband Rx LPF

This bit selects the nominal cutoff frequency of the 4-pole LPF. Setting this bit high selects a nominal cutoff frequency of 28.8 M Hz . When the wideband filter is selected, the Rx path gain is limited to 30 dB .

## Bit 3: Fast ADC Sampling

Setting this bit increases the quiescent current in the SVGA block. T his may provide some performance improvement when the ADC sampling frequency is greater than 50 M SPS (in 6-bit mode).

## Bit 4: Rx Digital HPF Bypass

Setting this bit high bypasses the 1-pole digital H PF that follows the ADC. The digital filter must be bypassed for ADC sampling above 50 M SPS.

## Bit 5: Rx Path DC Offset Correction

Writing a O ne to this bit triggers an immediate receive path offset correction and reads back zero after the completion of the offset correction.

## Bit 6: Rx LPF Tuning Update In Progress

This bit indicates when receive filter calibration is in progress. The duration of a receive filter calibration is about 500 ms . Writing to this bit has no effect.

## Bit 7: Rx LPF Tuning Update Disable

Setting this bit high disables the automatic background receive filter calibration. The AD 9875 automatically calibrates the receive filter on reset and every few $(\sim 2)$ seconds thereafter to compensate for process and temperature variation, power supply and long term drift. Programming a one to this bit disables this function. Programming a zero triggers an immediate first calibration and enables the periodic update.

## REGISTER 5-RECEIVE FILTER TUNING TARGET

This register sets the filter tuning target as a function of $\mathrm{f}_{\mathrm{SCLIN}}$. See Register 4 description.

## REGISTER 6-Rx PATH GAIN ADJUST

The AD 9875 uses a combination of a continuous time PGA (CPGA) and a switched capacitor PGA (SPGA) for a gain range of -6 to 36 dB with a resolution of 2 dB . T he $R x$ path gain can be programmed over the serial interface by writing to the $R x$ Path G ain Adjust register or directly using the GAIN and M SB aligned $T x[5: 1]$ bits. The register default value is $0 \times 00$ for lowest gain setting $(-6 \mathrm{~dB})$. The register always reads back the actual gain setting irrespective of which of the two programming modes were used.
T able V describes the gains and how they are achieved as a function of the Rx Path adjust bits.

## Bit 5: PGA Gain Set through Register

Setting this bit high will result in the Rx Path $G$ ain being set by writing to the PGA Gain Control register. D efault is zero which selects writing the gain through the $\mathrm{T} x[5: 1]$ pins in conjunction with the gain pin.

Table V. PGA Programming Map

| Rx Path <br> Gain [4:0] | Rx Path <br> Gain | CPGA <br> Gain | SPGA <br> Gain |
| :--- | :--- | :--- | :--- |
| $0 \times 00$ | -6 | -6 | 0 |
| $0 \times 01$ | -4 | -6 | 2 |
| $0 \times 02$ | -2 | -6 | 4 |
| $0 \times 03$ | 0 | -6 | 6 |
| $0 \times 04$ | 2 | -6 | 8 |
| $0 \times 05$ | 4 | -6 | 10 |
| $0 \times 06$ | 6 | 0 | 6 |
| $0 \times 07$ | 8 | 0 | 8 |
| $0 \times 08$ | 10 | 0 | 10 |
| $0 \times 09$ | 12 | 6 | 6 |
| $0 \times 0 \mathrm{~A}$ | 14 | 6 | 8 |
| $0 \times 0 \mathrm{~B}$ | 16 | 6 | 10 |
| $0 \times 0 \mathrm{C}$ | 18 | 12 | 6 |
| $0 \times 0 \mathrm{D}$ | 20 | 12 | 8 |
| $0 \times 0 \mathrm{E}$ | 22 | 18 | 10 |
| $0 \times 0 \mathrm{~F}$ | 24 | 18 | 6 |
| $0 \times 10$ | 26 | 18 | 8 |
| $0 \times 11$ | 28 | $18 / 24$ | 10 |
| $0 \times 12 *$ | $30 / 30$ | $18 / 24$ | $12 / 6$ |
| $0 \times 13^{*}$ | $30 / 32$ | $18 / 24$ | $12 / 8$ |
| $0 \times 14^{*}$ | $30 / 34$ | $18 / 24$ | $12 / 12$ |
| $0 \times 15^{*}$ | $30 / 36$ |  |  |

*W hen the Wideband Rx Filter bit is set high, the Rx Path Gain is limited to 30 dB . The first of the two values in the chart refers to this mode. The second number refers to the mode when the lower Rx LPF cutoff frequency is chosen, or the Rx LPF filter is bypassed.

## REGISTER 7-TRANSMIT PATH SETTINGS

The AD 9875 transmit path has a programmable interpolation filter that precedes the transmit DAC. The interpolation filter can be programmed to operate in seven different modes. Also, the digital interface can be programmed to operate in several different modes. These modes are described below.

## Bit 0: Transmit Port Demultiplexer Bypass

Setting Bit 0 high bypasses the input data demultiplexer. In this mode, consecutive nibbles on the TxD ATA(5:0) pins are treated as individual words to be sent through the $T$ x path. This creates a six bit data path. The state of T xSY NC is ignored in this mode.

## Bit 1: Transmit Port Width

If Bit 1 is set high, the $T \times$ port will operate such that the most significant nibble and the least significant nibble are each five bits wide. The default mode is six bits for the most significant nibble and four bit for the least significant nibble. The data is always aligned to the M SB pin Tx[5]. Enabling this pin on the AD 9875 allows for a five pin versus the default six pin interface.

## Bit 2: Transmit Port Least Significant Nibble First

Setting Bit 2 high reconfigures the AD 9875 for a transmit mode that expects least significant nibble before the most significant nibble.

## Bit 3: Power-Down Interpolator at TxQUIET Pin Low

Setting Bit 3 high enables the T XQUIET pin to shut off the DAC output. If the bit is set to one, then pulling the T xQUIET pin low will power down the interpolator filters. In most applications the interpolator filter will need to be flushed with zeros before or after being powered down.

## Bit 4 to Bit 7: Interpolation Filter Select

Bits 4 to 7 define the Interpolation filter characteristic and interpolation rate.

## Bits 7:4;

$0 \times 2$; Interpolation Bypass.
$0 \times 0$; see T PC $1.4 \times$ Interp, LPF .
$0 \times 1$; see T PC 2. $2 \times$ Interp, LPF .
$0 \times 4$; see T PC 3. $4 \times$ Interp, BPF, Adj image.
$0 \times 5$; see T PC 4. $2 \times$ Interp, BPF, Adj image.
$0 \times 8$; see T PC 5. $4 \times$ Interp, BPF, lower image.
$0 \times$ C ; see TPC 6. $4 \times$ Interp, BPF, upper image.
The interpolation factor has a direct influence on the CLK-A output frequency. When the transmit input data multiplexer is enabled (10-bit mode):

$$
f_{C L K-A}=2 \times f_{D A C} / K
$$

where $K$ is the interpolation factor.
When the transmit input data multiplexer is disabled ( $5-/ 6$-bit mode):

$$
f_{C L K-A}=f_{D A C} / K
$$

where $K$ is the interpolation factor.

## REGISTER 8-RECEIVER AND CLOCK OUTPUT SETTINGS <br> Bit 0: Rx Port Multiplexer Bypass

Setting this bit high bypasses the Rxport output multiplexer. This will output only the 6 M SBs of the ADC word. This mode enables ADC sampling rates above 55 M SPS.

## Bit 1: Rx Port Width Five Bits

If the bit is set high, the $R x$ port data will be output in two nibbles of five bits each (on pins $\mathrm{Rx}[5: 1]$ ). When this bit is low (default), the most significant nibble will contain six bits and the least significant nibble will have four bits. T he default mode makes the AD 9875 pin compatible with the AD 9876.

## Bit 2: Rx Port LS Nibble First

Reconfigures the AD 9875 for a receive mode that expects less significant bits before the most significant bits.

## Bit 3: Three-State Rx Port

This bit sets the receive output $\mathrm{Rx}[5: 0]$ into a high impedance three-state mode. It allows for sharing the bus with other devices.

## Bit 4, Bit 5: Disable CLK-A, Disable CLK-B

Setting Bit 4 or Bit 5 stops CLK -A or CLK-B respectively, from toggling. The output is held to a logic 0 level.

## Bit 4, Bit 5: Disable CLK-A, Disable CLK-B

Setting Bit 4 or Bit 5 fixes CLK -A or CLK-B to a low output level, respectively.

## Bit 6: CLK-A Output Invert

Setting Bit 6 high inverts the CLK -A output signal.

## Bit 7: CLK-B Output Invert

Setting this bit high inverts the CLK-B output signal. This effectively changes the timing of the $R x[5: 0]$ and $R x S Y N C$ signals from rising edge triggered to falling edge triggered with respect to the CLK-B signal.

## REGISTER F, DIE REVISION

This register stores the die revision of the chip. It is a readonly register.

## PCB DESIGN CONSIDERATIONS

Although the AD 9875 is a mixed-signal device, the part should be treated as an analog component. The digital circuitry on-chip has been specially designed to minimize the impact that the digital switching noise will have on the operation of the analog circuits. Following the power, grounding and layout recommendations in this section will help you get the best performance from the M XFE.

## Component Placement

If the three following guidelines of component placement are followed, chances for getting the best performance from the $M \times F E$ are greatly increased. F irst, manage the path of return currents flowing in the ground plane so that high frequency switching currents from the digital circuits do not flow on the ground plane under the M xFE or analog circuits. Second, keep noisy digital signal paths and sensitive receive signal paths as short as possible. Third, keep digital (noise generating) and analog (noise susceptible) circuits as far away from each other as possible.
In order to best manage the return currents, pure digital circuits that generate high switching currents should be closest to the power supply entry. T his will keep the highest frequency return current paths short, and prevent them from traveling over the sensitive M xFE and analog portions of the ground plane. Also, these circuits should be generously bypassed at each device which will further reduce the high frequency ground currents. The M xFE should be placed adjacent to the digital circuits, such that the ground return currents from the digital sections will not flow in the ground plane under the M xFE. The analog circuits should be placed furthest from the power supply.
The AD 9875 has several pins which are used to decouple sensitive internal nodes. These pins are REFIO, REFB, and REFT. The decoupling capacitors connected to these points should have low ESR and ESL. T hese capacitors should be placed as close to the M xFE as possible and be connected directly to the analog ground plane.
The resistor connected to the FSADJ pin should also be placed close to the device and connected directly to the analog ground plane.

## Power Planes and Decoupling

The AD 9875 evaluation board demonstrates a good power supply distribution and decoupling strategy. The board has four layers; two signal layers, one ground plane and one power plane. The power plane is split into a 3VDD section used for the 3 V digital logic circuits, a DVDD section used to supply the digital supply pins of the AD 9875, an AVDD section used to supply the analog supply pins of the AD 9875, and a VANLG section that supplies the higher voltage analog components on the board. The 3VDD section will typically have the highest frequency currents on the power plane and should be kept the furthest from the M xFE and analog sections of the board. The DVDD portion of the plane brings the current used to power the digital portion of the M xFE to the device. This should be treated similarly to the 3VDD power plane and be kept from going underneath the M xFE or analog components. The M xF E should largely sit on the AVDD portion of the power plane.

## AD9875

The AVDD and DVDD power planes may be fed from the same low noise voltage source; however, they should be decoupled from each other to prevent the noise generated in the DVDD portion of the M xFE from corrupting the AVDD supply. T his can be done by using ferrite beads between the voltage source and DVDD, and between the source and AVDD. Both DVDD and AVDD should have a low ESR, bulk decoupling capacitor on the $M \times F E$ side of the ferrite as well as a low ESR, ESL decoupling capacitors on each supply pin (i.e., the AD 9875 requires five power supply decoupling caps, one each on Pins 5, 38, 47, 14, and 35). The decoupling caps should be placed as close to the M xF E supply pins as possible. An example of the proper decoupling is shown in the AD 9875 evaluation board schematic.

## Ground Planes

In general, if the component placing guidelines discussed earlier can be implemented, it is best to have at least one continuous ground plane for the entire board. All ground connections should be made as short as possible. This will result in the lowest impedance return paths, and the quietest ground connections.

If the components cannot be placed in a manner that will keep the high-frequency ground currents from traversing under the MxFE and analog components, it may be necessary to put
current steering channels into the ground plane to route the high-frequency currents around these sensitive areas. T hese current steering channels should be made only when and where necessary.

## Signal Routing

The digital Rx and Tx signal paths should be kept as short as possible. Also, the impedance of these traces should have a controlled characteristic impedance of about $50 \Omega$. This will prevent poor signal integrity and the high currents that can occur during undershoot or overshoot caused by ringing. If the signal traces cannot be kept shorter than about 1.5 inches, then series-termination resistors ( $33 \Omega$ to $47 \Omega$ ) should be placed close to all signal sources. It is a good idea to series-terminate all clock signals at their source, regardless of trace length.
The receive $\mathrm{Rx} \pm$ signals are the most sensitive signals on the entire board. C areful routing of these signals is essential for good receive path performance. The $\mathrm{Rx} \pm$ signals form a differential pair and should be routed together as a pair. By keeping the traces adjacent to each other, noise coupled onto the signals will appear as common-mode and will be largely rejected by the $M \times F E$ receive input. K eeping the driving point impedance of the receive signal low and placing any low-pass filtering of the signals close to the M xFE will further reduce the possibility of noise corrupting these signals.

## OUTLINE DIMENSIONS

Dimensions shown in inches and (mm).

## 48-Lead LQFP <br> (ST-48)



CONTROLLING DIMENSIONS ARE IN MILLIMETERS.


[^0]:    M xFE is a trademark of Analog D evices, Inc
    TxDAC + is a registered trademark of Analog D evices, Inc.

[^1]:    Specifications subject to change without notice.

