
Low Noise Pseudomorphic HEMT in a Surface Mount Plastic Package

Technical Data

ATF-33143

Features

- Low Noise Figure
- Excellent Uniformity in Product Specifications
- 1600 micron Gate Width
- Low Cost Surface Mount Small Plastic Package SOT-343 (4 lead SC-70)
- Tape-and-Reel Packaging Option Available

Specifications

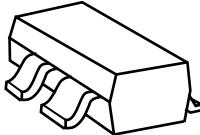
1.9 GHz; 4V, 80 mA (Typ.)

- 0.5 dB Noise Figure
- 15 dB Associated Gain
- 22 dBm Output Power at 1 dB Gain Compression
- 33.5 dBm Output 3rd Order Intercept

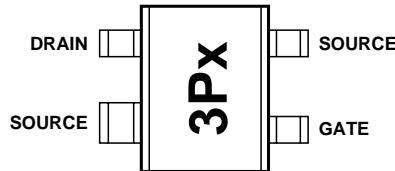
Applications

- Tower Mounted Amplifier, Low Noise Amplifier and Driver Amplifier for GSM/TDMA/CDMA Base Stations
- LNA for Wireless LAN, WLL/RLL and MMDS Applications
- General Purpose Discrete PHEMT for other Ultra Low Noise Applications

Surface Mount Package SOT-343



Pin Connections and Package Marking



Note: Top View. Package marking provides orientation and identification.

“3P” = Device code

“x” = Date code character. A new character is assigned for each month, year.

Description

Agilent's ATF-33143 is a high dynamic range, low noise PHEMT housed in a 4-lead SC-70 (SOT-343) surface mount plastic package.

Based on its featured performance, ATF-33143 is ideal for the first or second stage of base station LNA due to the excellent combination of low noise figure and enhanced linearity^[1]. The device is also suitable for applications in Wireless LAN, WLL/RLL, MMDS, and other systems requiring super low noise figure with good intercept in the 450 MHz to 10 GHz frequency range.

Note:

1. From the same PHEMT FET family, the smaller geometry ATF-34143 may also be considered for the higher gain performance, particularly in the higher frequency band (1.8 GHz and up).

ATF-33143 DC Electrical Specifications

$T_A = 25^\circ\text{C}$, RF parameters measured in a test circuit for a typical device

Symbol	Parameters and Test Conditions			Units	Min.	Typ. ^[2]	Max.
$I_{dss}^{[1]}$	Saturated Drain Current	$V_{DS} = 1.5\text{ V}$, $V_{GS} = 0\text{ V}$		mA	175	237	305
$V_P^{[1]}$	Pinchoff Voltage	$V_{DS} = 1.5\text{ V}$, $I_{DS} = 10\%$ of I_{dss}		V	-0.65	-0.5	-0.35
I_d	Quiescent Bias Current	$V_{GS} = -0.5\text{ V}$, $V_{DS} = 4\text{ V}$		mA	—	80	—
$g_m^{[1]}$	Transconductance	$V_{DS} = 1.5\text{ V}$, $g_m = I_{dss}/V_P$		mmho	360	440	—
I_{GDO}	Gate to Drain Leakage Current	$V_{GD} = 5\text{ V}$		µA			1000
I_{gss}	Gate Leakage Current	$V_{GD} = V_{GS} = -4\text{ V}$		µA	—	42	600
NF	Noise Figure	$f = 2\text{ GHz}$	$V_{DS} = 4\text{ V}$, $I_{DS} = 80\text{ mA}$ $V_{DS} = 4\text{ V}$, $I_{DS} = 60\text{ mA}$	dB		0.5	0.8
		$f = 900\text{ MHz}$	$V_{DS} = 4\text{ V}$, $I_{DS} = 80\text{ mA}$ $V_{DS} = 4\text{ V}$, $I_{DS} = 60\text{ mA}$	dB		0.4	—
G_a	Associated Gain ^[3]	$f = 2\text{ GHz}$	$V_{DS} = 4\text{ V}$, $I_{DS} = 80\text{ mA}$ $V_{DS} = 4\text{ V}$, $I_{DS} = 60\text{ mA}$	dB	13.5	15	16.5
		$f = 900\text{ MHz}$	$V_{DS} = 4\text{ V}$, $I_{DS} = 80\text{ mA}$ $V_{DS} = 4\text{ V}$, $I_{DS} = 60\text{ mA}$	dB		21	—
OIP3	Output 3 rd Order Intercept Point ^[3]	$f = 2\text{ GHz}$ 5 dBm Pout/Tone	$V_{DS} = 4\text{ V}$, $I_{DS} = 80\text{ mA}$ $V_{DS} = 4\text{ V}$, $I_{DS} = 60\text{ mA}$	dBm	30	33.5	—
		$f = 900\text{ MHz}$ 5 dBm Pout/Tone	$V_{DS} = 4\text{ V}$, $I_{DS} = 80\text{ mA}$ $V_{DS} = 4\text{ V}$, $I_{DS} = 60\text{ mA}$	dBm		32.5	—
P_{1dB}	1 dB Compressed Compressed Power ^[3]	$f = 2\text{ GHz}$	$V_{DS} = 4\text{ V}$, $I_{DS} = 80\text{ mA}$ $V_{DS} = 4\text{ V}$, $I_{DS} = 60\text{ mA}$	dBm		22	—
		$f = 900\text{ MHz}$	$V_{DS} = 4\text{ V}$, $I_{DS} = 80\text{ mA}$ $V_{DS} = 4\text{ V}$, $I_{DS} = 60\text{ mA}$	dBm		21	—

Notes:

- Guaranteed at wafer probe level.
- Typical value determined from a sample size of 450 parts from 9 wafers.
- Measurements obtained using production test board described in Figure 5.

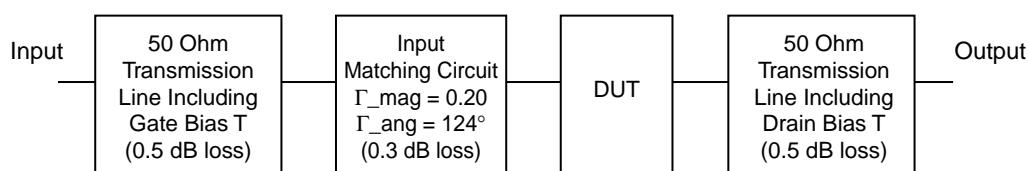


Figure 5. Block diagram of 2 GHz production test board used for Noise Figure, Associated Gain, P_{1dB} , and OIP3 measurements. This circuit represents a trade-off between an optimal noise match and a realizable match based on production test requirements. Circuit losses have been de-embedded from actual measurements.

ATF-33143 Typical Performance Curves

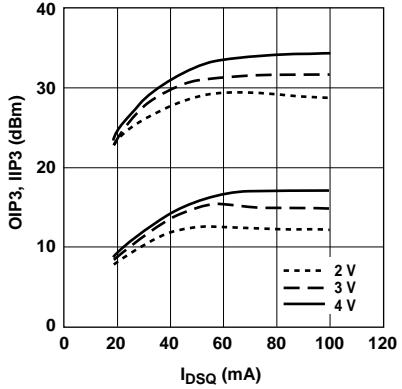


Figure 6. OIP3, IIP3 vs. Bias^[1] at 2 GHz.

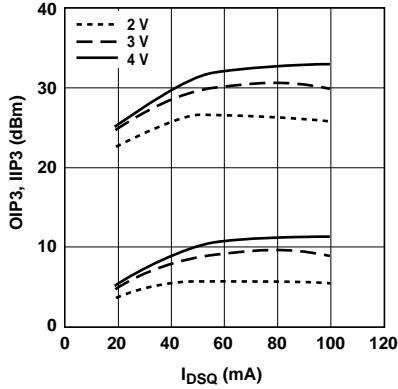


Figure 7. OIP3, IIP3 vs. Bias^[1] at 900 MHz.

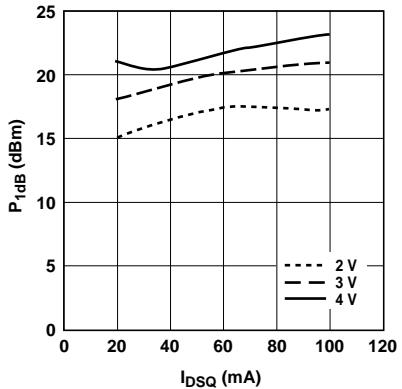


Figure 8. P_{1dB} vs. Bias^[1,2] at 2 GHz.

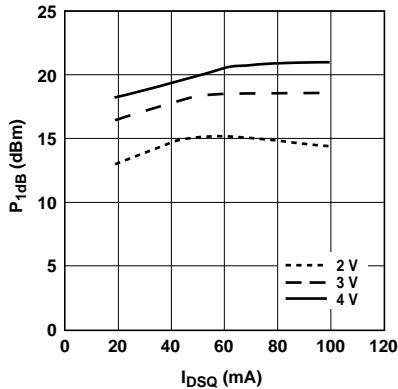


Figure 9. P_{1dB} vs. Bias^[1,2] Tuned for NF @ 4 V, 80 mA at 900 MHz.

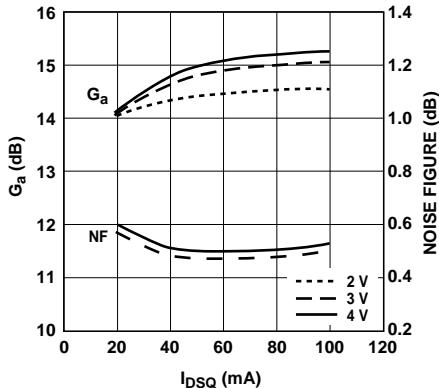


Figure 10. NF and G_a vs. Bias^[1] at 2 GHz.

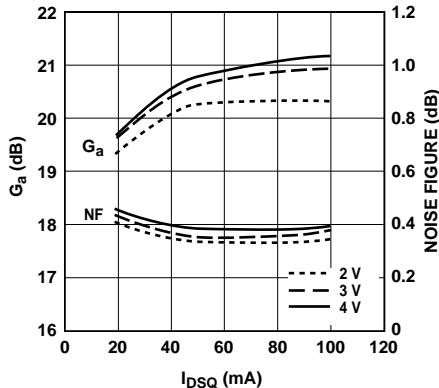


Figure 11. NF and G_a vs. Bias^[1] at 900 MHz.

Notes:

- Measurements made on a fixed tuned production test board that was tuned for optimal gain match with reasonable noise figure at 4V 80 mA bias. This circuit represents a trade-off between optimal noise match, maximum gain match and a realizable match based on production test board requirements. Circuit losses have been de-embedded from actual measurements.
- Quiescent drain current, I_{DSQ}, is set with zero RF drive applied. As P_{1dB} is approached, the drain current may increase or decrease depending on frequency and dc bias point. At lower values of I_{DSQ} the device is running closer to class B as power output approaches P_{1dB}. This results in higher P_{1dB} and higher PAE (power added efficiency) when compared to a device that is driven by a constant current source as is typically done with active biasing.

ATF-33143 Typical Performance Curves, continued

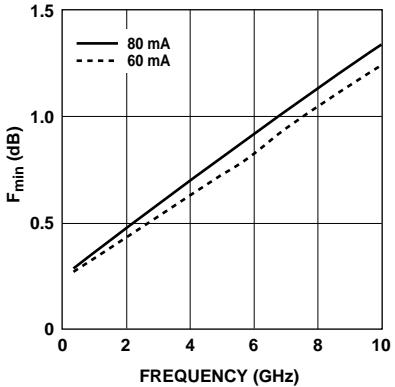


Figure 12. F_{\min} vs. Frequency and Current at 4V.

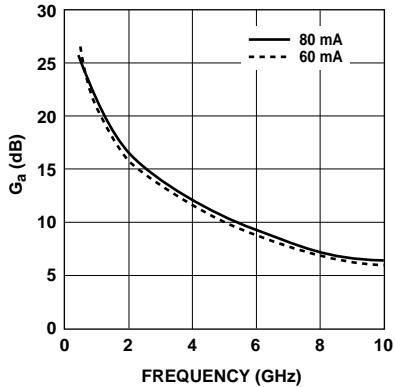


Figure 13. Associated Gain vs. Frequency and Current at 4V.

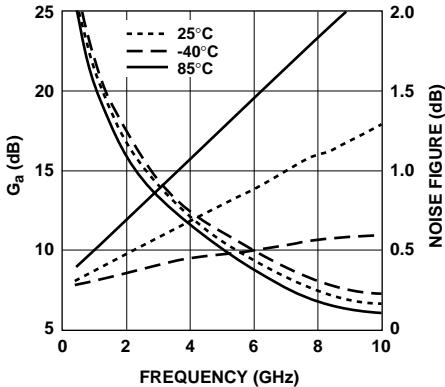


Figure 14. F_{\min} and G_a vs. Frequency and Temp at $V_{DS} = 4V$, $I_{DS} = 80$ mA.

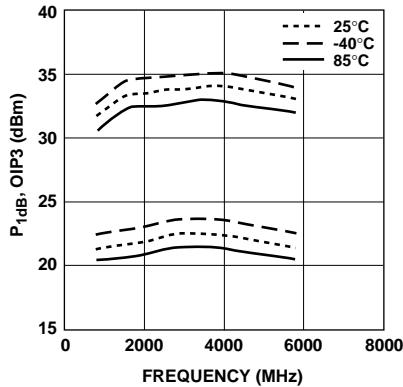


Figure 15. P_{1dB} , $OIP3$ vs. Frequency and Temp at $V_{DS} = 4V$, $I_{DS} = 80$ mA.

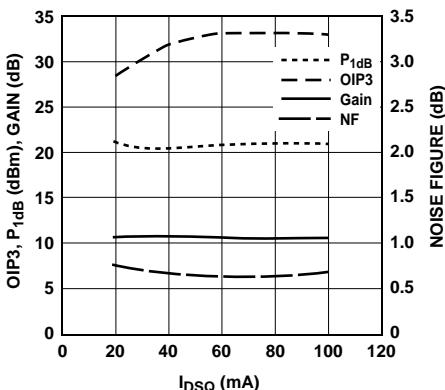


Figure 16. $OIP3$, P_{1dB} , NF and $Gain$ vs. Bias^[1,2] at 3.9 GHz.

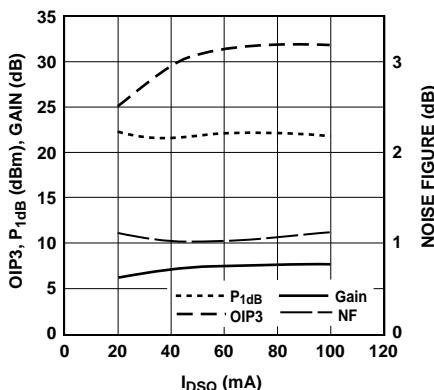


Figure 17. $OIP3$, P_{1dB} , NF and $Gain$ vs. Bias^[1,2] at 5.8 GHz.

Notes:

- Measurements made on a fixed tuned test fixture that was tuned for noise figure at 4V 80 mA bias. This circuit represents a trade-off between optimal noise match, maximum gain match and a realizable match based on production test requirements. Circuit losses have been de-embedded from actual measurements.
- Quiescent drain current, I_{Dsq} , is set with zero RF drive applied. As P_{1dB} is approached, the drain current may increase or decrease depending on frequency and dc bias point. At lower values of I_{Dsq} the device is running closer to class B as power output approaches P_{1dB} . This results in higher P_{1dB} and higher PAE (power added efficiency) when compared to a device that is driven by a constant current source as is typically done with active biasing.

ATF-33143 Typical Performance Curves, continued

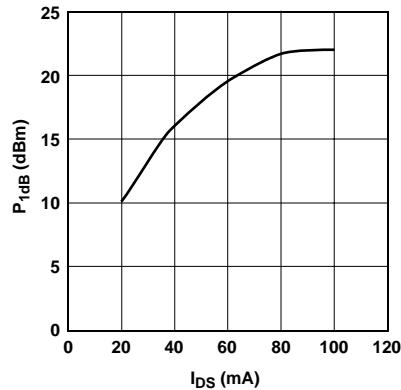


Figure 18. P_{1dB} vs. I_{DS} Active Bias^[1]
Tuned for NF @ 4V, 80 mA at 2 GHz.

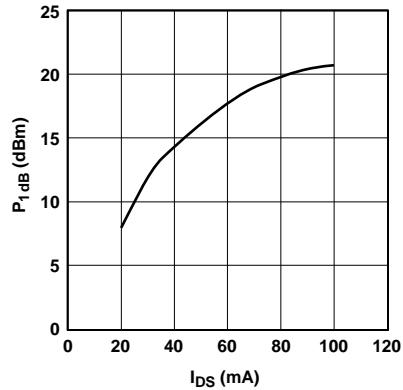


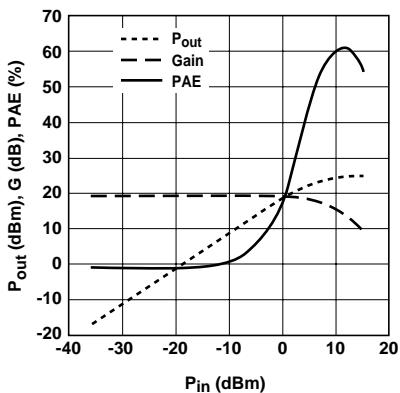
Figure 19. P_{1dB} vs. I_{DS} Active Bias^[1]
Tuned for NF @ 4V, 80 mA at 900 MHz.

Note:

1. Measurements made on a fixed tuned test board that was tuned for optimal gain match with reasonable noise figure at 4V 80 mA bias. This circuit represents a trade-off between an optimal noise match, maximum gain match and a realizable match based on production test board requirements. Circuit losses have been de-embedded from actual measurements.

ATF-33143 Power Parameters Tuned for Max P_{1dB}, V_{DS} = 4 V, I_{DSQ} = 80 mA

Freq (GHz)	P _{1dB} (dBm)	I _d (mA)	G _{1dB} (dB)	PAE _{1dB} (%)	P _{3dB} (dBm)	I _d (mA)	PAE _{3dB} (%)	Γ Out_mag (Mag.)	Γ Out_ang (°)
0.9	20.7	89	23.2	33	23.2	102	51	0.39	160
1.5	21.2	91	20.7	36	23.8	116	51	0.43	165
1.8	21.1	80	19.2	40	23.0	94	52	0.43	170
2.0	21.6	81	18.1	44	23.2	89	57	0.42	174
4.0	23.0	97	11.9	48	24.6	135	48	0.40	-150
6.0	24.0	130	5.9	36	25.2	136	36	0.37	-124



**Figure 20. Swept Power Tuned for Max P_{1dB}
V_{DS} = 4 V, I_{DSQ} = 80 mA, 2 GHz.**

Notes:

1. Measurements made on ATN LP1 power load pull system.
2. Quiescent drain current, I_{DSQ}, is set with zero RF drive applied. As P_{1dB} is approached, the drain current may increase or decrease depending on frequency and dc bias point. At lower values of I_{DSQ} the device is running closer to class B as power output approaches P_{1dB}. This results in higher P_{1dB} and higher PAE (power added efficiency) when compared to a device that is driven by a constant current source as is typically done with active biasing.
3. PAE (%) = ((P_{out} - P_{in}) / P_{dc}) X 100
4. Gamma out is the reflection coefficient of the matching circuit presented to the output of the device.

Noise Parameter Applications Information

F_{\min} values at 2 GHz and higher are based on measurements while the F_{\min} s below 2 GHz have been extrapolated. The F_{\min} values are based on a set of 16 noise figure measurements made at 16 different impedances using an ATN NP5 test system. From these measurements, a true F_{\min} is calculated. F_{\min} represents the true minimum noise figure of the device when the device is presented with an impedance matching network that transforms the source impedance, typically 50Ω , to an impedance represented by the reflection coefficient Γ_o . The designer must design a matching network that will present Γ_o to the device with minimal associated circuit losses. The noise figure of the completed amplifier is equal to the noise figure of the device plus the losses of the matching network preceding the device. The noise figure of the device is equal to F_{\min} only when the device is

presented with Γ_o . If the reflection coefficient of the matching network is other than Γ_o , then the noise figure of the device will be greater than F_{\min} based on the following equation.

$$NF = F_{\min} + \frac{4 R_n}{Z_0} \frac{|\Gamma_s - \Gamma_o|^2}{(1 + |\Gamma_o|^2)(1 - |\Gamma_s|^2)}$$

Where R_n/Z_0 is the normalized noise resistance, Γ_o is the optimum reflection coefficient required to produce F_{\min} and Γ_s is the reflection coefficient of the source impedance actually presented to the device. The losses of the matching networks are non-zero and they will also add to the noise figure of the device creating a higher amplifier noise figure. The losses of the matching networks are related to the Q of the components and associated printed circuit board loss. Γ_o is typically fairly low at higher frequencies and increases as frequency is lowered. Larger gate width devices will typically have a lower Γ_o as compared to narrower gate width devices.

Typically for FETs, the higher Γ_o usually infers that an impedance much higher than 50Ω is required for the device to produce F_{\min} . At VHF frequencies and even lower L Band frequencies, the required impedance can be in the vicinity of several thousand ohms.

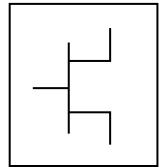
Matching to such a high impedance requires very hi-Q components in order to minimize circuit losses. As an example at 900 MHz, when airwound coils ($Q > 100$) are used for matching networks, the loss can still be up to 0.25 dB which will add directly to the noise figure of the device. Using multilayer molded inductors with Qs in the 30 to 50 range results in additional loss over the airwound coil. Losses as high as 0.5 dB or greater add to the typical 0.15 dB F_{\min} of the device creating an amplifier noise figure of nearly 0.65 dB. A discussion concerning calculated and measured circuit losses and their effect on amplifier noise figure is covered in Agilent Application 1085.

Reliability Data

Channel Temperature (°C)	Nominal Failures per million (FPM) for different durations					90% confidence Failures per million (FPM) for different durations				
	(FITs) 1000 hours	1 year	5 year	10 year	30 year	(FITs) 1000 hours	1 year	5 year	10 year	30 year
100	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
125	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	11
140	<0.1	<0.1	<0.1	<0.1	160	<0.1	<0.1	6	160	9.3K
150	<0.1	<0.1	2	140	26K	<0.1	0.3	780	8800	131K
160	<0.1	<0.1	920	21K	370K	<0.1	67	24K	120K	520K
180 NOT recommended	<0.1	4400	450K	830K	1000K	21	53K	590K	850K	1000K

Predicted failures with temperature extrapolated from failure distribution and activation energy data of higher temperature operational life STRIFE of PHEMT process

ATF-33143 Die Model



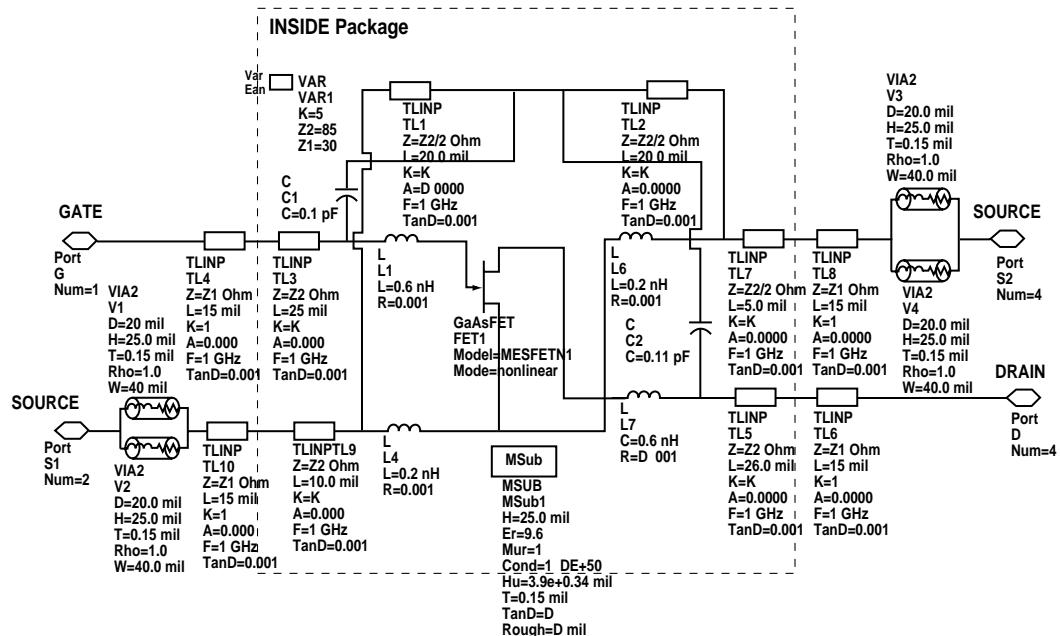
Statz Model
MESFETM1

NFET=yes	Cgs=1.6 pF	Rc=62.5	Taumd1=no
PFET=no	Gdcap=3	Gsfwd=1	Fnc=1E6
Vto=-0.95	Cgd=0.32 pF	Gsrev=0	R=0.17
Beta=0.48	Rgd=	Gdfwd=1	C=0.2
Lambda=0.09	Tqm=	Gdrev=0	P=0.65
Alpha=4	Vmax=	Vjr=1	wVgfwd=
B=0.8	Fc=	Is=1 nA	wBvgs=
Tnom=27	Rd=.125	Ir=1 nA	wBvgd=
Idstc=	Rg=1	Imax=0.1	wBvds=
Vbi=0.7	Rs=0.0625	Xti=	wldsmax=
Tau=	Ld=0.00375 nH	N=	wPmax=
Betate=	Lg=0.00375 nH	Eg=	AI IPParams=
Delta1=0.2	Ls=0.00125 nH	Vbr=	
Delta2=	Cds=0.08 pF	Vtotc=	
Gscap=3	Crf=0.1	Rin=	

This model can be used as a design tool. It has been tested on MDS for various specifications. However, for more precise and accurate design, please refer to

the measured data in this data sheet. For future improvements Agilent reserves the right to change these models without prior notice.

ATF-33143 Model

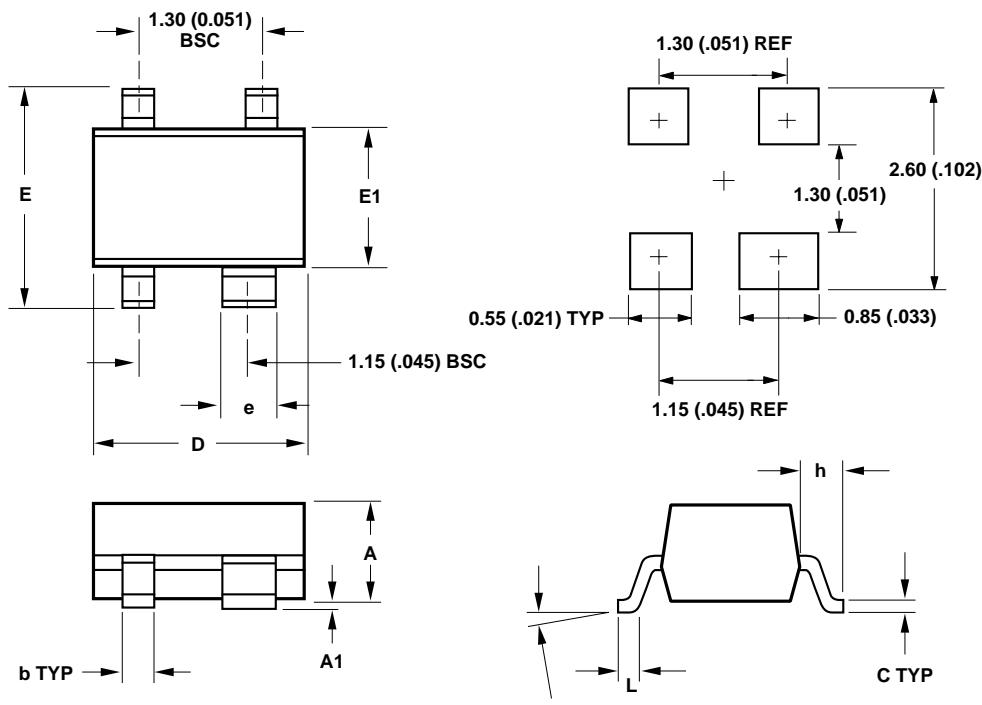


Part Number Ordering Information

Part Number	No. of Devices	Container
ATF-33143-TR1	3000	7" Reel
ATF-33143-TR2	10000	13" Reel
ATF-33143-BLK	100	antistatic bag

Package Dimensions

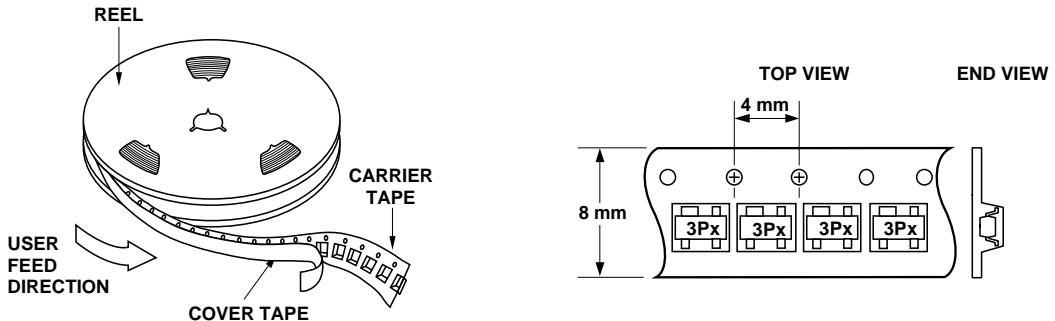
Outline 43 (SOT-343/SC-70 4 lead)



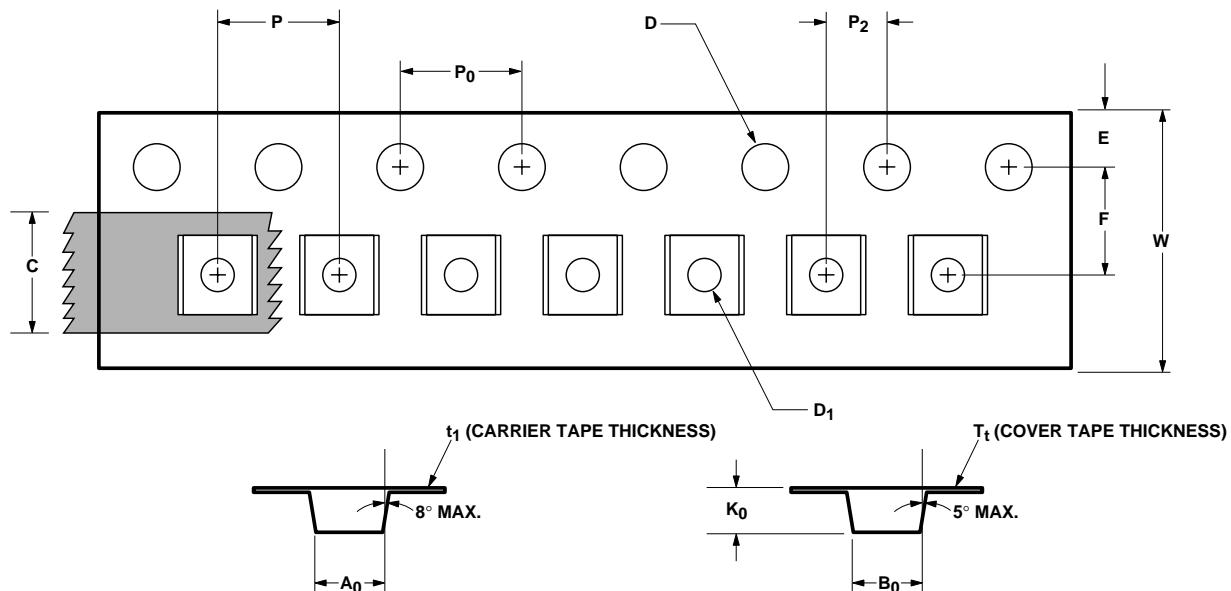
SYMBOL	DIMENSIONS	
	MIN.	MAX.
A	0.80 (0.031)	1.00 (0.039)
A1	0 (0)	0.10 (0.004)
b	0.25 (0.010)	0.35 (0.014)
C	0.10 (0.004)	0.20 (0.008)
D	1.90 (0.075)	2.10 (0.083)
E	2.00 (0.079)	2.20 (0.087)
e	0.55 (0.022)	0.65 (0.025)
h	0.450 TYP (0.018)	
E1	1.15 (0.045)	1.35 (0.053)
L	0.10 (0.004)	0.35 (0.014)
θ	0	10

DIMENSIONS ARE IN MILLIMETERS (INCHES)

Device Orientation



Tape Dimensions For Outline 4T



DESCRIPTION		SYMBOL	SIZE (mm)	SIZE (INCHES)
CAVITY	LENGTH	A ₀	2.24 ± 0.10	0.088 ± 0.004
	WIDTH	B ₀	2.34 ± 0.10	0.092 ± 0.004
	DEPTH	K ₀	1.22 ± 0.10	0.048 ± 0.004
	PITCH	P	4.00 ± 0.10	0.157 ± 0.004
	BOTTOM HOLE DIAMETER	D ₁	$1.00 + 0.25$	$0.039 + 0.010$
PERFORATION	DIAMETER	D	1.55 ± 0.05	0.061 ± 0.002
	PITCH	P ₀	4.00 ± 0.10	0.157 ± 0.004
	POSITION	E	1.75 ± 0.10	0.069 ± 0.004
CARRIER TAPE	WIDTH	W	8.00 ± 0.30	0.315 ± 0.012
	THICKNESS	t ₁	0.255 ± 0.013	0.010 ± 0.0005
COVER TAPE	WIDTH	C	5.4 ± 0.10	0.205 ± 0.004
	TAPE THICKNESS	t _t	0.062 ± 0.001	0.0025 ± 0.00004
DISTANCE	CAVITY TO PERFORATION (WIDTH DIRECTION)	F	3.50 ± 0.05	0.138 ± 0.002
	CAVITY TO PERFORATION (LENGTH DIRECTION)	P ₂	2.00 ± 0.05	0.079 ± 0.002



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Data subject to change.

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