

6427525 N E C ELECTRONICS INC

05E 23020 D

**BIPOLAR ANALOG INTEGRATED CIRCUIT** **$\mu$ PC1322CA***T-77-05-09***ELECTRONIC TUNING AM RADIO RECEIVER****DESCRIPTION**

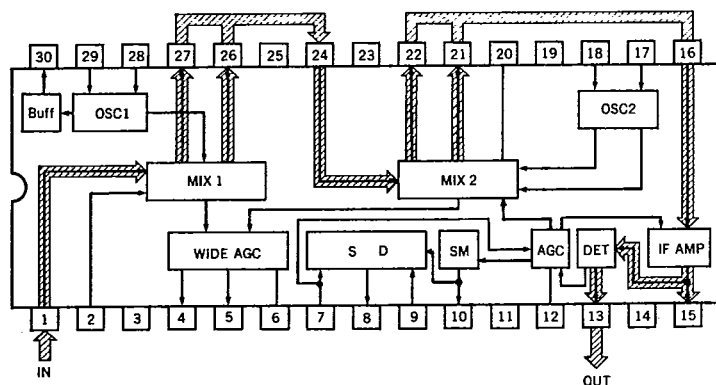
The  $\mu$ PC1322CA is a silicon monolithic integrated circuit designed for automotive AM radio receivers. The  $\mu$ PC1322CA consists of 1st mixer, 1st oscillator, oscillator buffer amplifier, 2nd mixer, 2nd oscillator, IF amplifier, detector, AGC circuit and IF output circuit for station detection. The IF output (SD OUT) is connected IF counter circuit of digital tuning microprocessor.

The  $\mu$ PC1322CA's 1st mixer and 1st oscillator convert station signal to 10.7 MHz. And 2nd mixer and 2nd oscillator convert 10.7 MHz signal to 450 kHz. Audio signal is detected from the 450 kHz signal after amplified by IF amplifier.

That is, the  $\mu$ PC1322CA uses up-conversion method, therefore a tracking adjustment free AM radio receiver can be made easily with employing the  $\mu$ PC1322CA.

**FEATURES**

- Tracking adjustment free
- MW/LW turnover switch is not necessary
- Excellent tweet characteristic
- Excellent sensitivity
- Good matching with AM stereo demodulator

**BLOCK DIAGRAM**

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 $\mu$ PC1322CA  
05E 23021 D

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ABSOLUTE MAXIMUM RATINGS ( $T_a = 25^\circ\text{C}$ )

DC Supply Voltage	$V_{CC}$	10	V
Package Dissipation	$P_D$	600	mW
Operating Temperature	$T_{opt}$	-30 to +75	$^\circ\text{C}$
Storage Temperature	$T_{stg}$	-40 to +125	$^\circ\text{C}$

RECOMMENDED OPERATING CONDITIONS ( $T_a = 25^\circ\text{C}$ )

DC Supply Voltage Range	$V_{CC}$	7.5 to 9	V
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ELECTRICAL CHARACTERISTICS ( $T_a = 25^\circ\text{C}$ ,  $V_{CC} = 8\text{ V}$ ,  $f = 1\text{ MHz}$ ,  $f_{mod} = 400\text{ Hz}$ ,  $mod = 30\%$ )

CHARACTERISTIC	SYMBOL	MIN.	TYP.	MAX.	UNIT	TEST CONDITION
Circuit Current	$I_{CC}$	34	45	58	mA	NO SIGNAL (IC only)
Signal to Noise Ratio	S/N	51	61		dB	$v_i = 74\text{ dB}\mu\text{V}$
Detector Output Volt	$v_o$	150	190	220	mV <sub>r.m.s.</sub>	$v_i = 74\text{ dB}\mu\text{V}$
Harmonic Distortion	THD <sub>1</sub>		0.2	1.0	%	$v_i = 74\text{ dB}\mu\text{V}$
	THD <sub>2</sub>		0.5	1.5	%	$v_i = 74\text{ dB}\mu\text{V}$ , $m = 80\%$
	THD <sub>3</sub>		0.4	1.5	%	$v_i = 130\text{ dB}\mu\text{V}$ , $m = 80\%$
Signal Meter Output	$V_{S1}$		0	0.1	V	NO SIGNAL
	$V_{S2}$	1.2	2.4	3.0	V	$v_i = 30\text{ dB}\mu\text{V}$
	$V_{S3}$	3.0	4.0	5.3	V	$v_i = 74\text{ dB}\mu\text{V}$
OSC. Buff. Output	$V_{osc\text{ Buff}}$	106	114	110	dB $\mu\text{V}$	

## TUNER PERFORMANCE CHARACTERISTICS

( $T_a = 25^\circ\text{C}$ ,  $V_{CC} = 8\text{ V}$ ,  $f = 1\text{ MHz}$ ,  $f_{mod} = 400\text{ Hz}$ ,  $mod = 30\%$ )

CHARACTERISTIC	TEST CONDITION	VALUE	UNIT
Maximum Sensitivity	$v_o = 30\text{ mV}_{r.m.s.}$	11	dB $\mu\text{V}$
Usable Sensitivity	S/N = 20 dB	27	dB $\mu\text{V}$
Detector Output Voltage	$v_i = 74\text{ dB}\mu\text{V}$	180	mV <sub>r.m.s.</sub>
Total Harmonic Distortion	$v_i = 74\text{ dB}\mu\text{V}$	0.2	%
	$v_i = 74\text{ dB}\mu\text{V}$ , $mod = 80\%$	0.5	%
	$v_i = 130\text{ dB}\mu\text{V}$ , $mod = 80\%$	0.4	%
Signal to Noise Ratio	$v_i = 74\text{ dB}\mu\text{V}$	61	dB
Tweet	$v_i = 74\text{ dB}\mu\text{V}$ , 2 IF = 900 kHz	61	dB
Signal Meter Output	NO SIGNAL	0	V
	$v_i = 30\text{ dB}\mu\text{V}$	2.4	V
	$v_i = 74\text{ dB}\mu\text{V}$	4.0	V
SD Sensitivity	8 pin Voltage L to H	21	dB $\mu\text{V}$

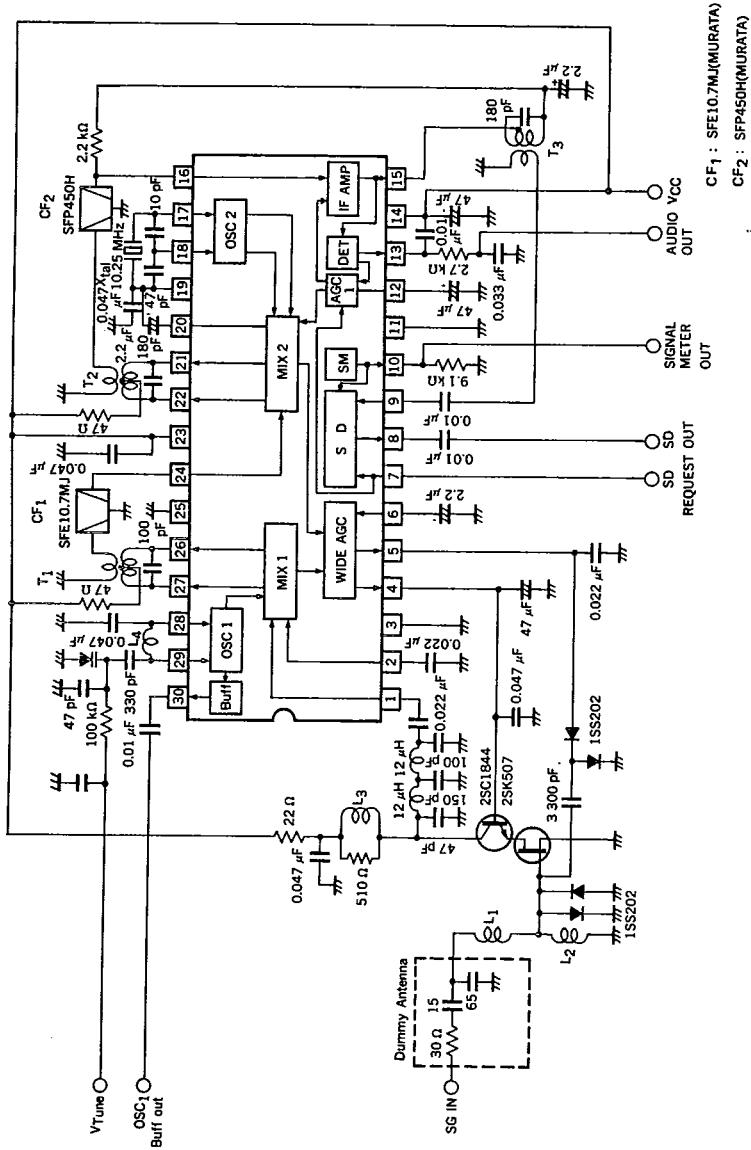
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TEST CIRCUIT

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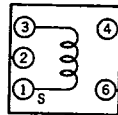


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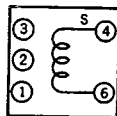
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COIL DATA (TOKO INC.)

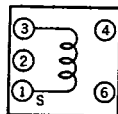
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L<sub>1</sub> X119FNS-16314Z

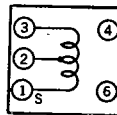
1-3 : 15 T  
 $L = 4.7 \mu\text{H}$   
 $Q_d > 60$

L<sub>2</sub> 7PD-1043

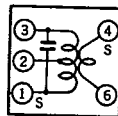
4-6 : 1440 T  
 $L = 100 \text{ mH}$   
 $Q > 45$

L<sub>3</sub> 247BR-0147Z

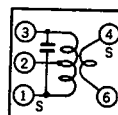
1-3 : 274 T  
 $L = 2 \text{ mH}$   
 $Q > 50$

L<sub>4</sub> 260LC-1694Y

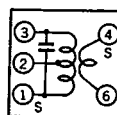
1-3 : 8 T 1-2 : 4 T  
 2-3 : 4 T  
 $L = 1.8 \mu\text{H}$   
 $Q_d > 70$

T<sub>1</sub> 260LC-1635N

1-3 : 14 T 1-2 : 7 T  
 2-3 : 7 T 4-6 : 2 T  
 $C = 47 \text{ pF}$   
 $Q = 68 \pm 20 \% f_o = 10.7 \text{ MHz}$

T<sub>2</sub> S7YC-1633N

1-3 : 150 T 1-2 : 75 T  
 2-3 : 75 T 4-6 : 20 T  
 $C = 180 \text{ pF}$   
 $Q = 42 \pm 20 \% f_o = 450 \text{ kHz}$

T<sub>3</sub> CX7YCS-8986N

1-3 : 148 T 1-2 : 43 T  
 2-3 : 105 T 4-6 : 30 T  
 $C = 180 \text{ pF}$   
 $Q = 40 \pm 20 \% f_o = 450 \text{ kHz}$

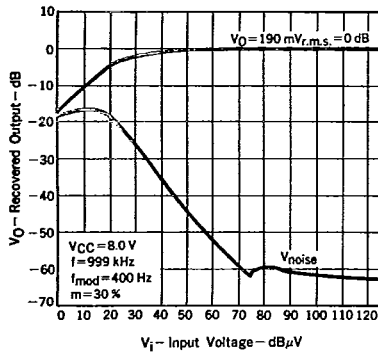
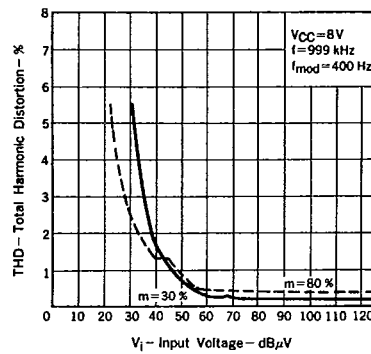
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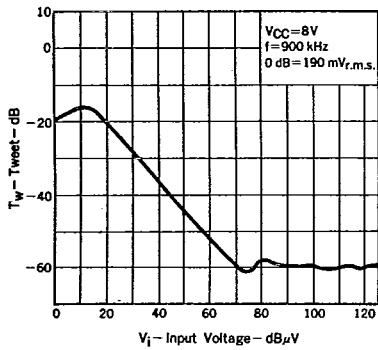
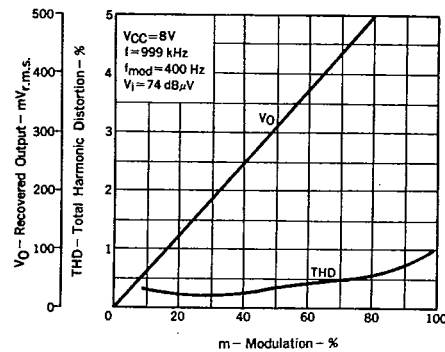
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TYPICAL CHARACTERISTICS ( $T_a = 25^\circ\text{C}$ )

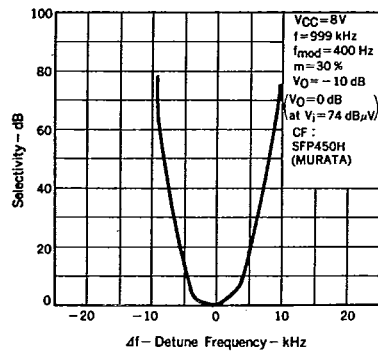
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RECOVERED OUTPUT vs.  
INPUT VOLTAGETOTAL HARMONIC DISTORTION vs.  
INPUT VOLTAGE

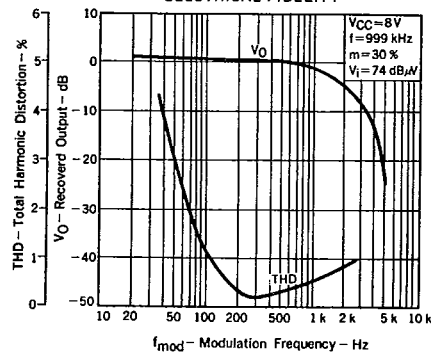
TWEET CHARACTERISTIC

RECOVERED OUTPUT AND TOTAL  
HARMONIC DISTORTION vs. MODULATION

ONE-SIGNAL SELECTIVITY



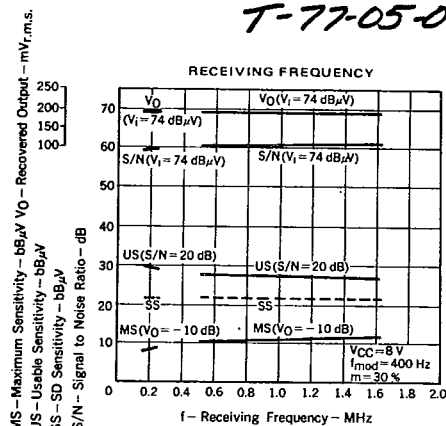
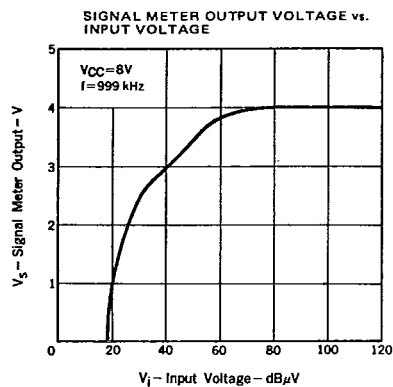
ELECTRICAL FIDELITY



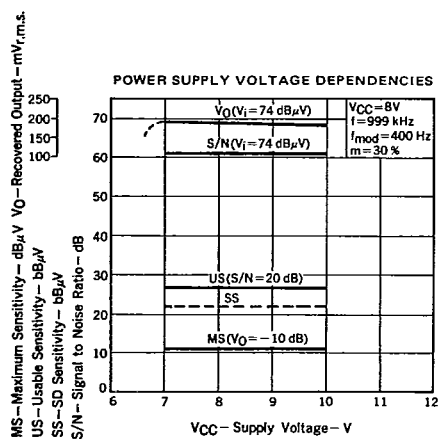
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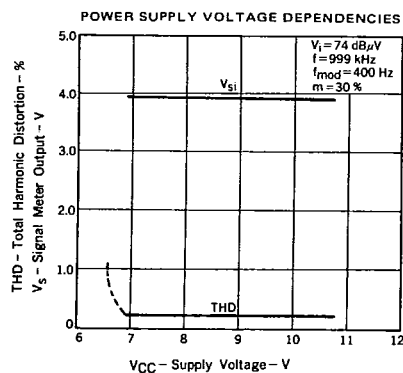
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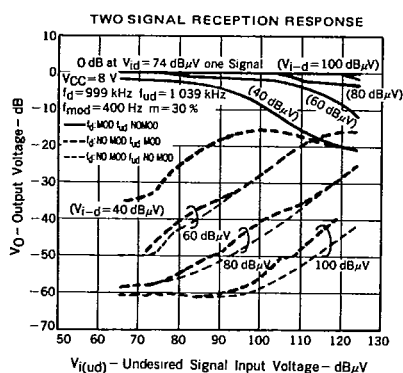
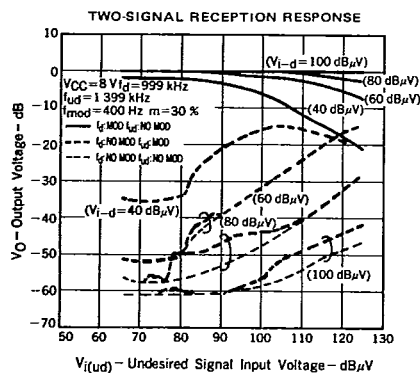
MS - Maximum Sensitivity - dB $\mu$ V  $V_0$  - Recovered Output - mV.m.s.  
 US - Usable Sensitivity - dB $\mu$ V  
 SS - SD Sensitivity - dB $\mu$ V  
 S/N - Signal to Noise Ratio - dB



MS - Maximum Sensitivity - dB $\mu$ V  $V_0$  - Recovered Output - mV.m.s.  
 US - Usable Sensitivity - dB $\mu$ V  
 SS - SD Sensitivity - dB $\mu$ V  
 S/N - Signal to Noise Ratio - dB



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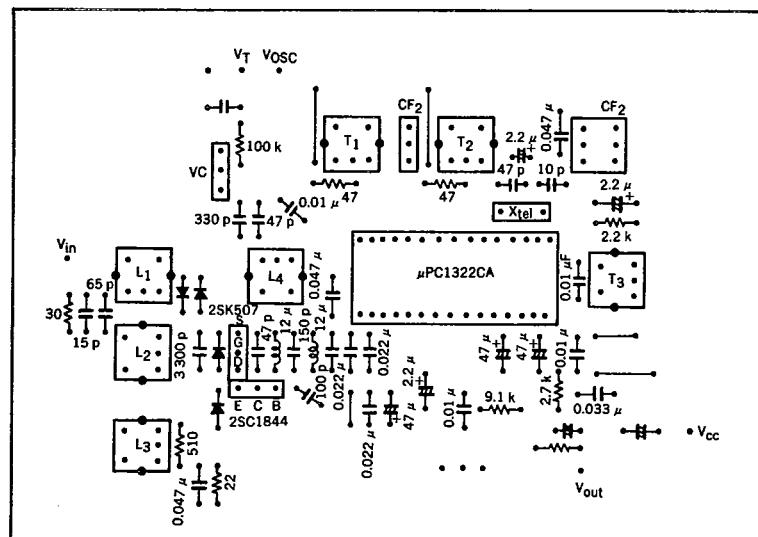
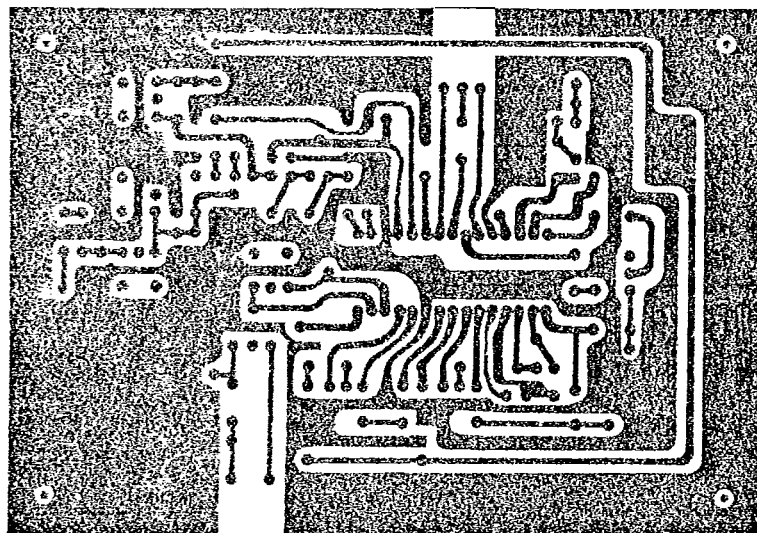
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**TYPICAL PCB (COPER SIDE)**

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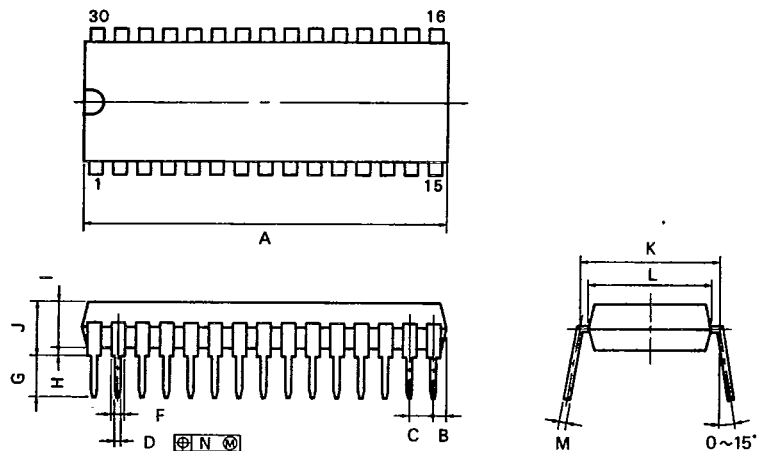
Unit C : F  
R :  $\Omega$

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30PIN PLASTIC SHRINK DIP (400 mil)



S30C-70-4008

## NOTES

- Each lead centerline is located within 0.17 mm (0.007 inch) of its true position (T.P.) at maximum material condition.
- Item "K" to center of leads when formed parallel.

ITEM	MILLIMETERS	INCHES
A	28.46 MAX.	1.121 MAX.
B	1.78 MAX.	0.070 MAX.
C	1.778 (T.P.)	0.070 (T.P.)
D	0.50 $\pm 0.10$	0.020 $\pm 0.004$
F	0.85 MIN.	0.033 MIN.
G	3.2 $\pm 0.3$	0.126 $\pm 0.012$
H	0.51 MIN.	0.020 MIN.
I	4.31 MAX.	0.170 MAX.
J	5.08 MAX.	0.200 MAX.
K	10.16 (T.P.)	0.400 (T.P.)
L	8.6	0.339
M	0.25 $\pm 0.08$	0.010 $\pm 0.003$
N	0.17	0.007

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**μPC1322CA**

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*T-77-05-09***1. GENERAL**

μPC1322CA is a monolithic integrated circuit developed as an AM tuner for car radios or car stereos. Double super-heterodyne method with  $IF_1 = 10.7$  MHz and  $IF_2 = 450$  kHz is employed. Consequently, this IC has free from tracking adjustment and flat sensitivity in the reception band.

It contains two sets of MIX and OSC circuits and an IF amplifier, detector circuit, AGC circuit, and station detector circuit. An electronic tuning receiver can be incorporated with this IC, external RF amplifier and controller such as μPD1713 or μPD1719.

The AGC circuit has wide-band characteristic to provide excellent 2-signal interference characteristics.

The operation and internal circuits of this IC are explained here.

**2. FEATURES**

- Three varactor diodes with wide variable capacitance range and identical characteristics are not required to enable electronic tuning; Only one varactor diode with a narrow capacity range is necessary.
- Tracking adjustment free.
- Flat sensitivity in the received frequency band.
- Deterioration of cross modulation and blocking with high power input to varactor diode does not occur.
- Excellent image rejection.
- No coil and switching circuit for long waves.
- Use of the antenna AGC circuit enables employment of high  $I_{FS}$  J-FET without deteriorating the cross modulation characteristics, thus enhancing the usable sensitivity.
- Good tweet characteristics.
- Good S/N ratio.
- The  $IF_2$  ceramic filter determines selectivity and easily meet AM stereo applications.

$\mu$ PC1322CA

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## 3. ELECTRICAL CHARACTERISTICS

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Table 1 shows the main electrical characteristics as measured by the standard application circuit.

Table 1 Electrical Characteristics ( $T_a = +25^\circ\text{C}$ ,  $V_{CC} = 8\text{ V}$ ,  $f = 1\text{ MHz}$ ,  $f_{\text{mod}} = 400\text{ Hz}$ ,  $m = 30\%$ )

CHARACTERISTIC	SYMBOL	MEASURED VALUE	UNIT	CONDITIONS
Max. sensitivity	MS	11	dB $\mu$ V	$V_{\text{in}}$ at $V_O = 10\text{ dB}$
Usable sensitivity	US	27	dB $\mu$ V	Input level when $S/N = 20\text{ dB}$
Signal-to-noise ratio	S/N	61	dB	$V_i = 74\text{ dB}\mu\text{V}$
Detection output	VOAF	190	mV <sub>r.m.s.</sub>	$V_i = 74\text{ dB}\mu\text{V}$
Total harmonic distortion	THD	0.2	%	$V_i = 74\text{ dB}\mu\text{V}$
Over load distortion	THD	0.4	%	$V_i = 130\text{ dB}\mu\text{V}$
Image rejection	IMR	—	dB	$f = 1.4\text{ MHz}$ , $V_O = 40\text{ mV}_{r.m.s.}$ , $f + 2\text{ IF}$
IF rejection	IFR	—	dB	$f = 0.6\text{ MHz}$ , $V_O = 40\text{ mV}_{r.m.s.}$ , $\text{IF} = 450\text{ kHz}$
Selectivity	ACA	60	dB	$f = \pm 9\text{ kHz}$
Tweet	T <sub>W</sub>	-61	dB	$V_i = 74\text{ dB}\mu\text{V}$ , $2\text{ IF}$
Local oscillation buffer output	V <sub>OSC-out</sub>	114	dB $\mu$ V	
SD sensitivity	SS	2.1	dB $\mu$ V	Input with 8 pin goes DC High
SD buffer output	SD <sub>out</sub>	1.8	V <sub>p-p</sub>	$V_i = 70\text{ dB}\mu\text{V}$
Signal meter output voltage	V <sub>S1</sub>	0	V	$V_i = 0\text{ dB}\mu\text{V}$
	V <sub>S2</sub>	2.4	V	$V_i = 30\text{ dB}\mu\text{V}$
	V <sub>S3</sub>	4.0	V	$V_i = 74\text{ dB}\mu\text{V}$

$\mu$ PC1322CA

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## 4. BLOCK DIAGRAM AND PACKAGE DIMENSION

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Figure 1 shows a block diagram. Figure 2 shows package dimension.

Figure 1 Block Diagram

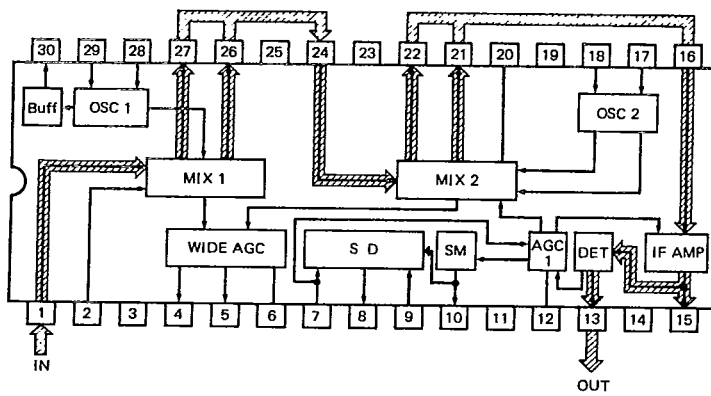
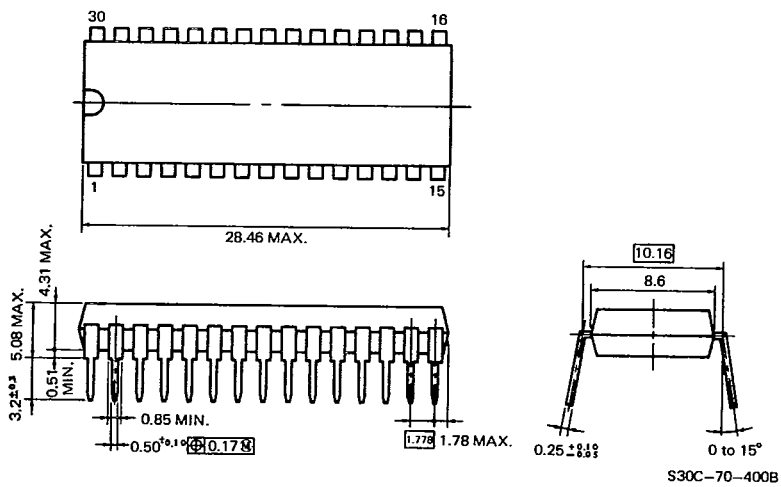


Figure 2 30-pin Plastic Shrink DIP (400 mil) Package Dimensions (Unit : mm)



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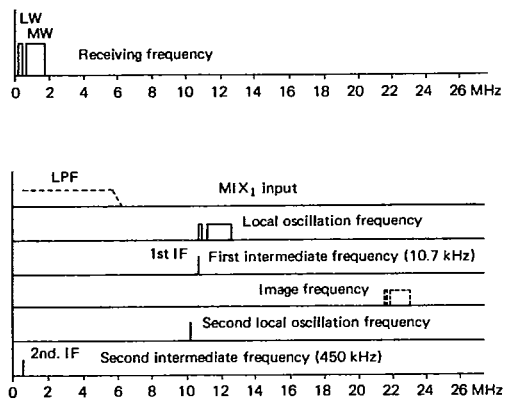
## 5. GENERAL OPERATION OF THIS IC

Figure 3 shows the standard application circuit, and Table 3 shows the coil specifications.

The input signal from the antenna is amplified by the non-tuning RF amplifier circuit, passes through the low pass filter (LPF) of approximately 6 MHz, and is input to the first mixer.

To set the first intermediate frequency (IF<sub>1</sub>) at 10.7 MHz, the first local oscillation frequency is determined as "Desired frequency + 10.7 MHz" for tuning, and the signal converted into 10.7 MHz passes through the 10.7 MHz filter and is input to the second mixer. To pass the 450 kHz filter for selectivity, the second local oscillation frequency is set as 10.25 MHz, converted into the second intermediate frequency of 450 kHz, and 450 kHz signal amplified, and then detected as the audio signal.

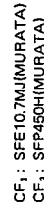
Table 2 shows the relationship of these frequencies.

Table 2 Frequency Relationship of  $\mu$ PC1322CA

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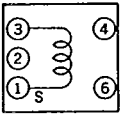
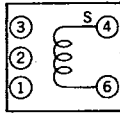
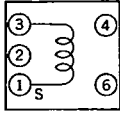
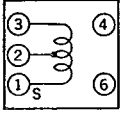
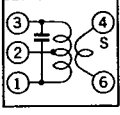
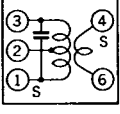
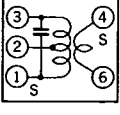
$\mu$ PC1322CA

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Table 3 Coil Specifications (Toko Corporation)

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ITEM No.	CONNECTION DIAGRAM	TYPE No.	SPECIFICATIONS
L <sub>1</sub>		X119FNS - 16314Z	①—③ 15T L = 4.7 $\mu$ F Q <sub>u</sub> > 60
L <sub>2</sub>		7PD - 1043	④—⑥ 1440T L = 100 mH Q > 45
L <sub>3</sub>		247BR - 0147Z	①—③ 274T L = 2 mH Q > 50
L <sub>4</sub>		260LC - 1694Y	①—③ ①—② ②—③ 8T 4T 4T L = 1.8 $\mu$ H Q <sub>u</sub> > 70
T <sub>1</sub>		260LC - 1635N	①—③ ①—② ②—③ ④—⑥ 14T 7T 7T 2T C = 47 pF Q = 68 $\pm$ 20 % f <sub>0</sub> = 10.7 MHz
T <sub>2</sub>		S7YC - 1633N	①—③ ①—② ②—③ ④—⑥ 150T 75T 75T 20T C = 180 pF Q = 42 $\pm$ 20 % f <sub>0</sub> = 450 kHz
T <sub>3</sub>		CX7YCS - 8986N	①—③ ①—② ②—③ ④—⑥ 148T 43T 105T 30T C = 180 pF Q = 40 $\pm$ 20 % f <sub>0</sub> = 450 kHz

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$\mu$ PC1322CA

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## 6. OPERATION EXPLANATION OF EACH STAGE

## 6.1 RF Amplifier Circuit Stage

Figure 4 RF Amplifier Circuit Stage

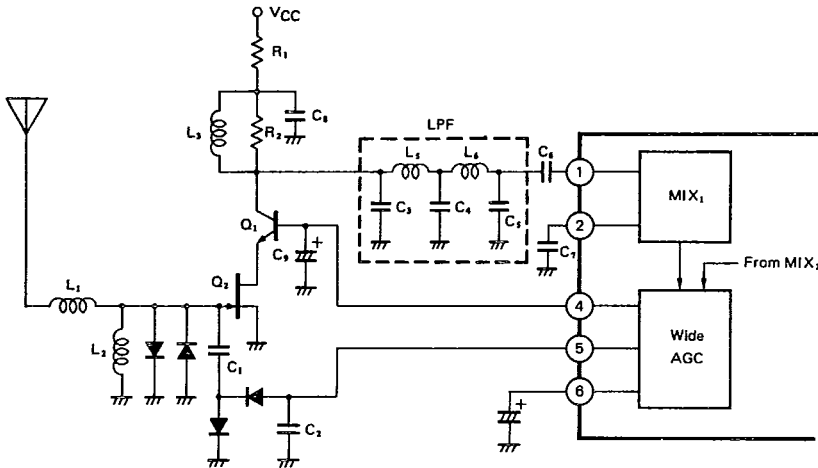


Figure 4 shows the RF amplifier circuit stage.

The car radio antenna is capacity-dependent in the AM band, so that the antenna capacity varies depending on the antenna length, diameter, and cable length. A J-FET is used for its high antenna load impedance and good linearity.

The load of  $Q_2$  is  $R_2$ , and  $L_3$  is used for bias voltage between the  $Q_2$  source and drain. This IC has the high IF<sub>1</sub> (10.7 MHz). The image frequency (higher than 21.4 MHz) is removed by the low-pass-filter consisting of  $L_5$ ,  $L_6$ ,  $C_3$ ,  $C_4$ , and  $C_5$ .

This IC has flat sensitivity in the received band because eliminating the tuning circuit that a conventional IC has.

Wide AGC consists of WAGC<sub>1</sub> shorting the input signal by  $C_1$  and WAGC<sub>2</sub> lowering the voltage between FET source and drain by  $Q_1$ .

Low noise, high  $|y_{fs}|$ , low capacitance FET for  $Q_2$  and Low noise Transistor for  $Q_1$  are required for good sensitivity.

The bias of cascade transistor  $Q_1$  shall be set  $V_C > V_B$ .

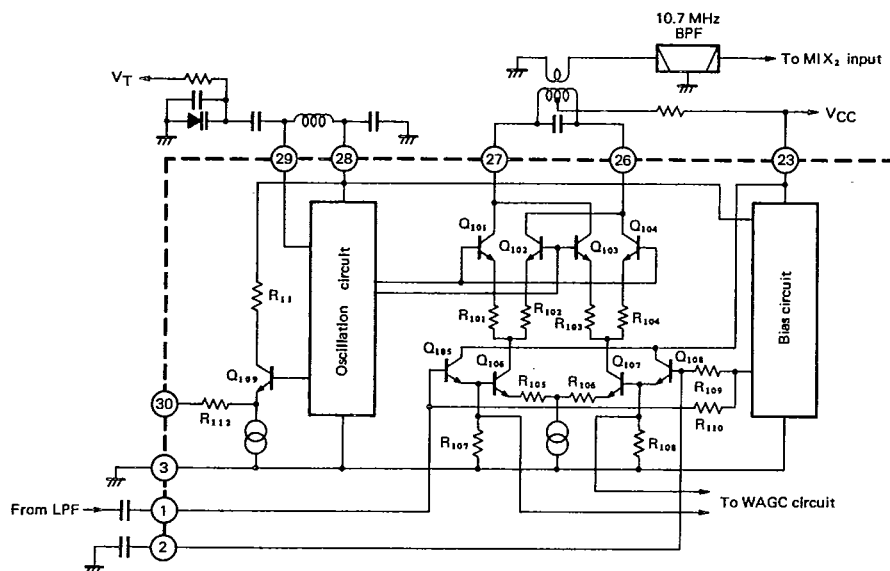
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## 6.2 First Frequency Mixer Stage

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Figure 5 First Frequency Mixer Stage



The first mixer circuit is a double-balanced mixer that consists of transistors  $Q_{101}$  through  $Q_{108}$  (Figure 5). The oscillation output injected to the bases of transistors  $Q_{101}$  through  $Q_{104}$ , and the RF signal input to the base of  $Q_{105}$  are mixed. If mixed frequency matches the resonance frequency of IFT, the output signal is generated from pins 26 and 27.  $R_{110}$  related to the input impedance to pin 1 is 1.2 k $\Omega$ .

The RF signals input to the base of  $Q_{105}$  are sensed by  $R_{107}$  and  $R_{108}$ , which connects to the wide-band AGC circuit.

The local oscillation output is amplified by the buffer amplifier  $Q_{109}$  and output to pin 30. This output is approximately 114 dB $\mu$ V, and can be directly input to the CMOS LSI for the PLL synthesizer.

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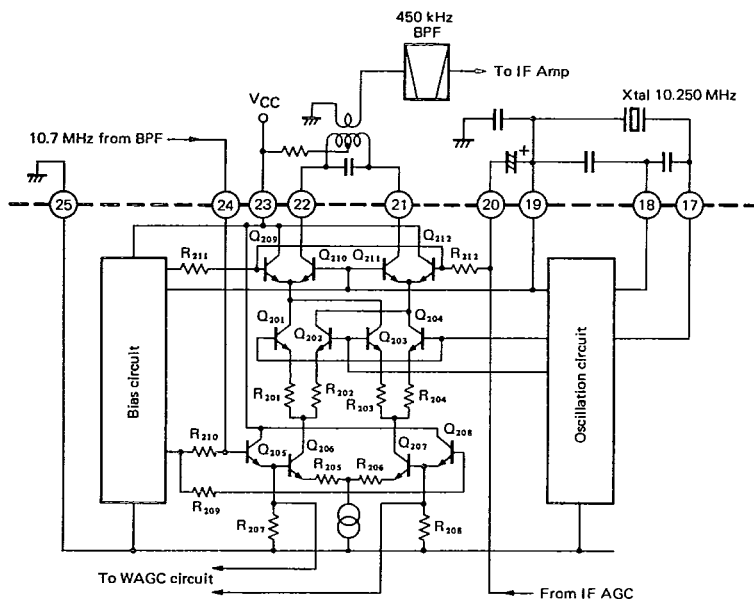
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## 6.3 Second Frequency Mixer Stage

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Figure 6 Second Frequency Mixer Stage



The second mixer stage is a double-balanced mixer with almost the same construction as the first mixer. (See Figure 6.) Difference of the first mixer is differential circuits ( $Q_{209}$  through  $Q_{212}$ ). The base potentials of  $Q_{212}$  and  $Q_{209}$  change the currents of  $Q_{210}$  and  $Q_{211}$ , and it perform the AGC operation.  $R_{210}$  related to the input impedance of this MIX is  $300\ \Omega$ .

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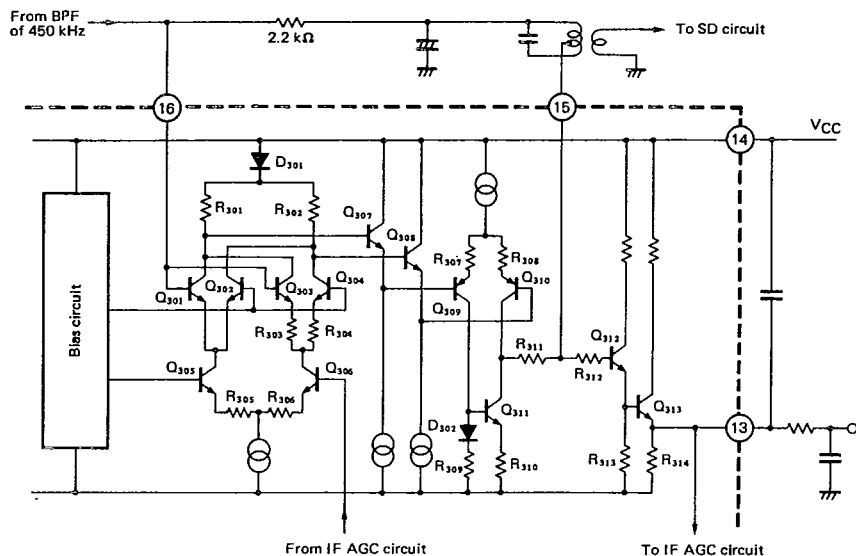
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## 6.4 Intermediate Frequency Amplifier and Detector Stage

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Figure 7 Intermediate Frequency Amplifier and Detector Stage



The intermediate amplifier stage consists of the two amplifiers, emitter follower circuits. (See Figure 7.) The first amplifier is the differential amplifier consisting of Q301, Q302, Q303, and Q304. The base potential of Q306 changes the current of this differential amplifier and perform the AGC operation. The IF<sub>2</sub> signal amplified by the first amplifier and passed through the emitter follower circuit of Q307 and Q308, is amplified by the second amplifier consisting of Q309 and Q310.

The detector stage consists of Q312 and Q313 and the audio signal outputs from pin 13.

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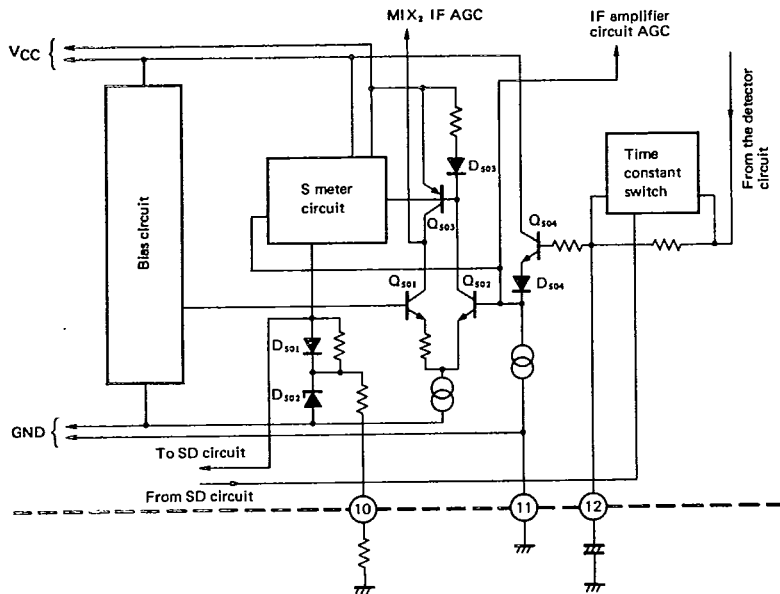
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### 6.5 AGC Circuit Stage

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$\mu$ PC1322CA has two independent AGC circuits: the IF AGC corresponding to the IF stage, and the wide AGC corresponding to the RF stage.

Figure 8 IF AGC Stage



The IF AGC, as explained in Section 6.3 and 6.4, is controlled by pin 12 voltage which is smoothed detector output (pin 13) voltage by capacitor. The signal meter output is provided to output the current in proportion to the operating voltage of AGC circuit.

Figure 9 shows the relationship between the IF AGC operating voltage and input voltage characteristics, and Figure 10 shows the relationship between the signal meter voltage and input voltage characteristics.

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Figure 9 Relation between IF AGC Operating Voltage and Input Voltage Characteristics

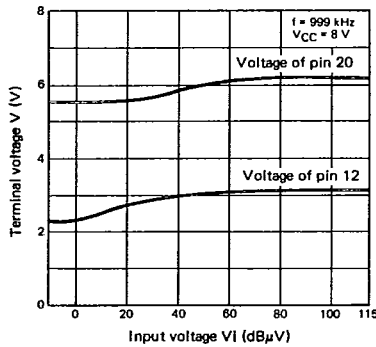


Figure 10 Relation between Signal Meter Output Voltage and Input Voltage Characteristics

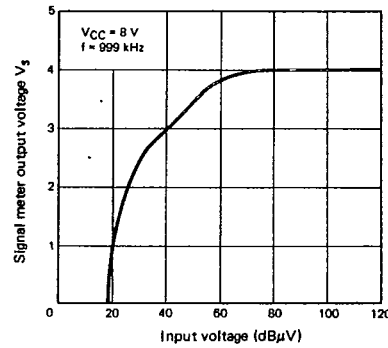
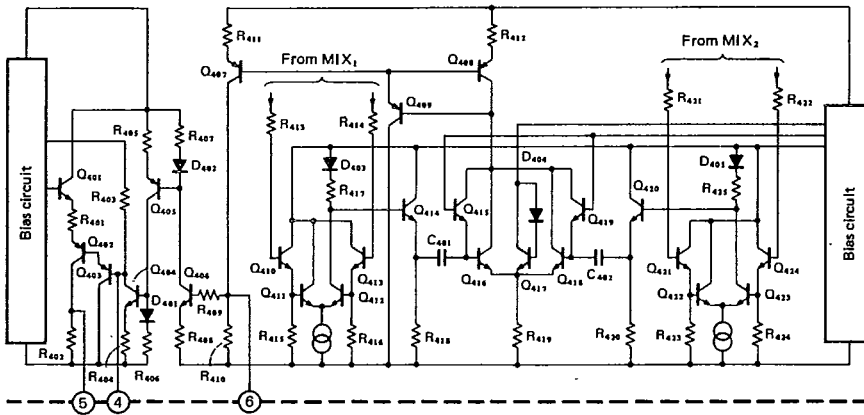


Figure 11 Wide AGC Stage



The wide AGC circuit is shown in Figure 11. The wide AGC input signals are MIX<sub>1</sub> and MIX<sub>2</sub>, these signals amplify with the amplifier circuits of Q<sub>410</sub> through Q<sub>414</sub> and Q<sub>420</sub> through Q<sub>424</sub>, adds with the detector of Q<sub>415</sub> through Q<sub>419</sub>, and converts them into the DC signals with Q<sub>406</sub> through Q<sub>408</sub>. The wide AGC enables Q<sub>401</sub> through Q<sub>405</sub> to generate both signals WAGC<sub>1</sub> of antenna short-circuit type and WAGC<sub>2</sub> of cascade connection type explained in Section 6.1.

Figure 12 shows the operations of pins 4, 5, and 6 for the input signals. Figure 13 shows the operations of pins 4 and 5 for the frequencies.

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Figure 12 WAGC Terminal Voltage vs. Input Voltage

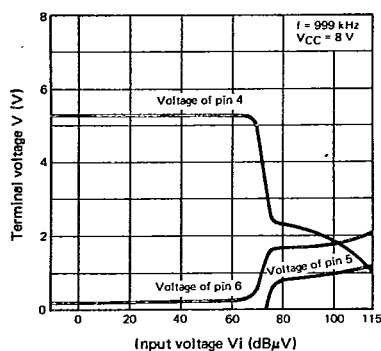
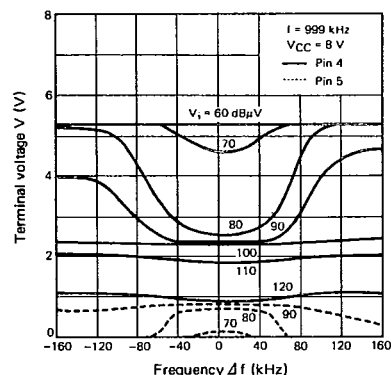


Figure 13 WAGC Terminal Voltage vs. Input Voltage



Since WAGC adds the first MIX input and second MIX input as shown above, it has the frequency characteristics in the IF<sub>1</sub> filter band between  $V_i = 70$  dBμV and 100 dBμV for the desired receiving frequency. That is, AGC operates faster near the desired frequency and slower as the frequency drifts away from the desired frequency.

Figure 14 Cross Modulation Characteristics (400 kHz)

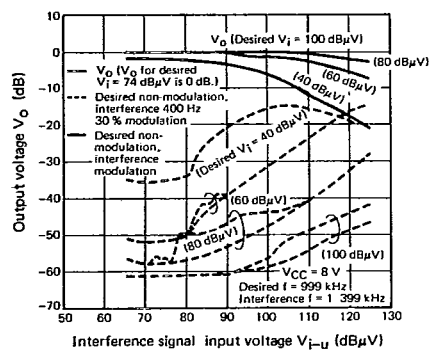
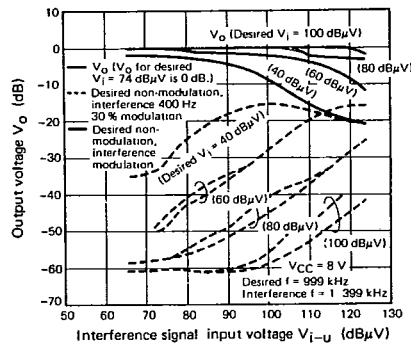


Figure 15 Cross Modulation Characteristics (40 kHz)



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Figure 14 shows how the desired station signal is interfered by signal strength (antenna input)  $V_{i(d)}$  of this interference station if the broadcasting station of antenna input  $V_{i(d)}$  is received with frequency 999 kHz and the interference station is located at 1 399 kHz, 400 kHz away from this receiving frequency.

Figure 15 shows the 2-signal characteristics if the desired station is 40 kHz away from the interference station. If a desired signal is received from the broadcasting station with the high signal strength of 60 dB $\mu$ V or more, the desired signal sensitivity is suppressed slightly if there is a broadcasting station generating the interference signal with the signal strength of 120 dB $\mu$ V. However, if a desired signal is received from the broadcasting station with the signal strength with 40 dB $\mu$ V, the desired signal sensitivity is suppressed by the interference signal.

In the above figure, the upper side of the dotted line indicates how much the crossmodulated signal is output when the desired signal is not modulated and the interference signal is modulated by 400 Hz/30 % to vary its signal strength. It also indicates how much the cross modulated signal is output if the signal strength of the desired signal is changed at this time.

If the desired signal is received from the broadcasting station with high signal strength of 80 dB $\mu$ V or more, there is no problem for hearing because the ratio of the desired signal output to the cross modulated signal output is 30 dB or more if there is the interference signal with signal strength 120 dB $\mu$ V. However, if the desired signal from the broadcasting station with the signal strength of 60 dB $\mu$ V is received, this ratio becomes 30 dB or less when there is the interference signal with the signal strength of 100 dB $\mu$ V. Since this is the same level as the noise output at non-modulation of the interference signal described below, it can be heard only as noise and does not cause cross modulation. That is, only the signal-to-noise ratio is lowered to cause no problem for hearing the car radio, which always varies the signal strength. When there is the interference signal with the signal strength of 80 dB $\mu$ V or more at 400 kHz away or with the signal strength of 75 dB $\mu$ V or more at 40 kHz away from the broadcasting station and the desired signal with the signal strength of 40 dB $\mu$ V, the ratio of the desired signal output to the cross modulated signal output becomes 30 dB or less. However, there is no problem for hearing because it is only noise.

The lower side of the dotted line indicates how much noise is generated if the interference signal strength is changed when both the desired signal and the interference signal are not modulated. It also indicates how much the noise is output when the desired signal strength is changed in this case.

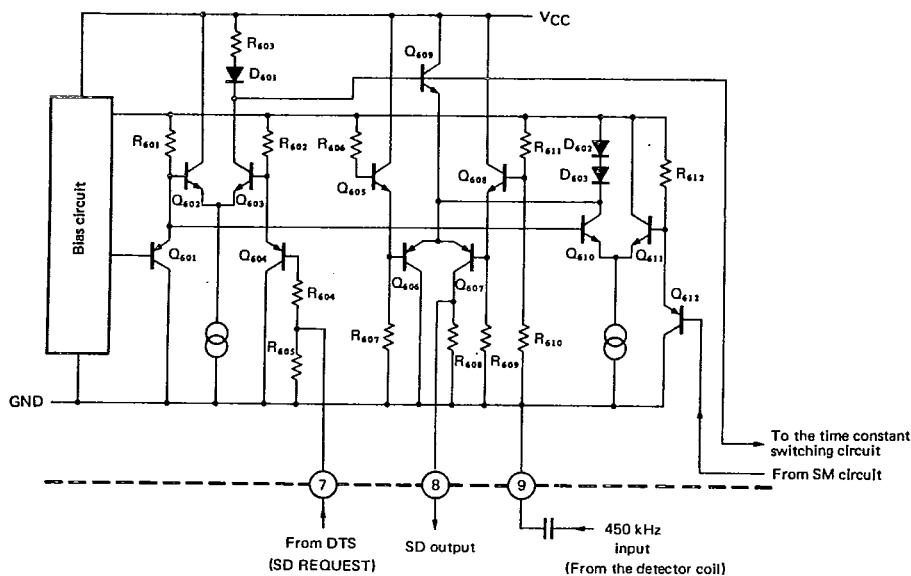
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## 6.6 Station Detector Circuit Stage

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Figure 16 Station Detector Circuit Stage



The station detector (SD) circuit is provided to stop the scan/seek operation if a broadcasting station is detected during automatic scanning or seek tuning. The SD circuit in this IC outputs the intermediate frequency signal ( $f \approx 450$  kHz). The output intermediate frequency signal is counted by the controller (such as  $\mu$ PD1713G) built into the counter circuit to lock the PLL of the controller. The station detector circuit (Figure 16) is operated by the DC voltage, which is output from the controller during automatic scanning or seek operation, from pin 7.

This DC voltage causes Q603 and then Q609 to be turned ON, and the time constant for IF AGC to be switched. If the signal meter voltage is low, the current of Q609 flows into collector Q610. If the signal meter voltage reaches a certain value, the current from Q609 drives differential amplifiers Q606 and Q607 to amplify the IF signal input from pin 9 and output it to pin 8.

If PLL is locked by the controller, pin 7 inputs 0 V to turn OFF Q603 and then Q609 to stop the output to pin 8.

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## 6.7 Other

Table 3 shows the DC voltage of each pin of this IC.

Table 3 DC Voltage of Each Pin (Standard application circuit,  $V_{CC} = 8.0$  V, Unit : V)

Pin No.	$V_{in} = 0$	$V_{in} = 74 \text{ dB}\mu\text{V}$	Pin No.	$V_{in} = 0$	$V_{in} = 74 \text{ dB}\mu\text{V}$
1	3.6	3.6	16	3.6	3.6
2	3.6	3.6	17	5.3	5.3
3	GND	GND	18	4.7	4.7
4	5.7	2.8	19	6.0	6.0
5	0	0	20	5.5	6.0
6	0.2	1.6	21	7.7	7.9
7	0	0(*5.0)	22	7.7	7.9
8	0	0(*1.0)	23	8.0( $V_{CC}$ )	8.0( $V_{CC}$ )
9	5.3	5.3	24	3.6	3.6
10	0	4.0	25	GND	GND
11	GND	GND	26	7.7	7.7
12	2.3	3.1	27	7.7	7.7
13	2.3	3.1	28	6.0	6.0
14	8.0( $V_{CC}$ )	8.0( $V_{CC}$ )	29	6.0	6.0
15	3.6	3.6	30	3.3	3.3

(\*) Indicates the value when 5 V is impressed to pin 7.

Figure 17 shows the application circuit which combines DTS IC  $\mu$ PD1713AG-018 with this IC.



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