

# 8V/5V Low Dropout Dual Regulator with ENABLE

# Description

The CS-8164 is a low dropout, dual 8V/5V linear regulator. The secondary 5V/100mA output is used for powering systems with standby memory. Quiescent current drain is less than 2mA when supplying 10mA loads from the standby regulator.

In automotive applications, the CS-8164 and all regulated circuits are protected from reverse battery installations, as well as high voltage transients. During line transients, such as a 60V load dump, the 750mA output will automat-

ically shutdown to protect both internal circuits and the load, while the secondary regulator continues to power any standby load.

The on board ENABLE function controls the regulator's primary output. When ENABLE is in the low state, the regulator is placed in STANDBY mode where it draws 2mA (typ) quiescent current.

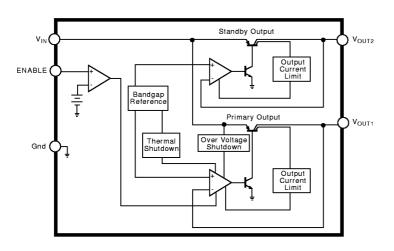
The CS-8164 is packaged in a 5-lead TO-220, with copper tab for connection to a heat sink, if necessary.

#### **Absolute Maximum Ratings**

DC Input Voltage	0.5V to 26V
Transient Peak Voltage (46V LoadDump)	60V
Internal Power Dissipation	Internally Limited
Operating Temperature Range	40°C to +125°C
Junction Temperature Range	
Storage Temperature Range	65°C to +150°C
Reverse Polarity V <sub>OUT1</sub> Input Voltage, DC	18V
Reverse Polarity Input Voltage, Transient	50V
Lead Temperature Soldering	

Wave Solder (through hole styles only).......10 sec. max, 260°C peak

#### **Block Diagram**

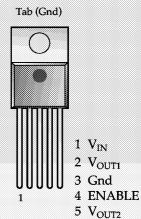


# **Features**

- Two Regulated Outputs
  Primary Output
  8V ±5%; 750mA
  Secondary Output
  5V ±2%; 100mA
- Low Dropout Voltage
- ON/OFF Control
  Option
- Standby Quiescent Drain (<2mA)
- Protection Features
  Reverse Battery
  60V Peak Transient
  Voltage
  -50V Reverse Transient
  Short Circuit
  Thermal Shutdown

# **Package Option**

5 Lead TO-220



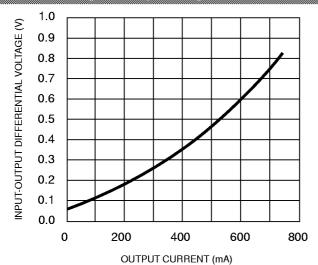


Cherry Semiconductor Corporation 2000 South County Trail East Greenwich, Rhode Island 02818-1530 Tel: (401)885-3600 Fax (401)885-5786 email: info@cherry-semi.com

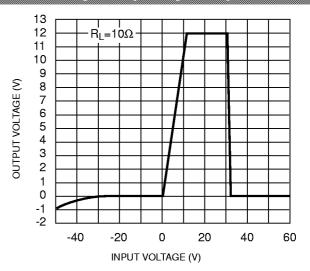
PARAMETER	TESTE CONTINUES S	MIN	TVP	MAX	U.
OUTPUT STAGE (V <sub>OUT</sub> )					
0011	12V 4V 426V I 4500m A	7.6	0.0	8.4	
Output Voltage, V <sub>OUT1</sub>	$13V \le V_{IN} \le 26V$ , $I_{OUT1} \le 500$ mA, $13V \le V_{IN} \le 16V$ , $I_{OUT1} \le 750$ mA	7.6 7.6	8.0 8.0	8.4 8.4	,
Dropout Voltage	$I_{OUT1} = 500 \text{mA}$			0.60	,
Line Regulation	$13V \le V_{IN} \le 16V$ , $I_{OUT1} = 5mA$		15	80	n
Load Regulation	$5\text{mA} \le I_{OUT1} \le 500\text{mA}$		15	80	n
Quiescent Current	$I_{OUT1} \le 10$ mA, No Load on Standby $I_{OUT1} = 500$ mA, No Load on Standby $I_{OUT1} = 750$ mA, No Load on Standby		3 40 90	7 100	n n n
Ripple Rejection	f = 120Hz		53		C
Current Limit		0.75	1.40	2.50	
Long Term Stability			50		m\
Output Impedance	500mA DC and 10mA rms, 100Hz - 10kHz		200		n
Thermal Shutdown		150	190		c
Overvoltage Shutdown		26	40		,
Standby Output (V <sub>OUT2</sub> )					
Output Voltage, (V <sub>OUT2</sub> )	$6V \le V_{IN} \le 26V$	4.75	5.00	5.25	1
Dropout Voltage	$I_{OUT2} \le 100 \text{mA}$		0.55	0.70	,
Line Deculation	$6V \le V_{IN} \le 26V$		4	50	n
Line Regulation	0 · = · IIV = <b>=</b> 0 ·				
Load Regulation	$1mA \le I_{OUT2} \le 100mA$		10	50	n
	_,		10 2	50 3	
Load Regulation	$1 \text{mA} \le I_{\text{OUT2}} \le 100 \text{mA}$ $I_{\text{OUT2}} \le 10 \text{mA}$ , $-40^{\circ}\text{C} \le T_{\text{J}} \le +125^{\circ}\text{C}$				n
Load Regulation Quiescent Current	$1\text{mA} \le I_{\text{OUT2}} \le 100\text{mA}$ $I_{\text{OUT2}} \le 10\text{mA}$ , $-40^{\circ}\text{C} \le T_{J} \le +125^{\circ}\text{C}$ $V_{\text{OUT1}}$ OFF		2		m c
Load Regulation Quiescent Current Ripple Rejection	$1\text{mA} \le I_{\text{OUT2}} \le 100\text{mA}$ $I_{\text{OUT2}} \le 10\text{mA}$ , $-40^{\circ}\text{C} \le T_{J} \le +125^{\circ}\text{C}$ $V_{\text{OUT1}}$ OFF		2 66		n c n
Load Regulation Quiescent Current Ripple Rejection Current Limit	$1\text{mA} \le I_{\text{OUT2}} \le 100\text{mA}$ $I_{\text{OUT2}} \le 10\text{mA}$ , $-40^{\circ}\text{C} \le T_{J} \le +125^{\circ}\text{C}$ $V_{\text{OUT1}}$ OFF		2 66 200		n c n mV
Load Regulation Quiescent Current Ripple Rejection Current Limit Long Term Stability	$1\text{mA} \le I_{OUT2} \le 100\text{mA}$ $I_{OUT2} \le 10\text{mA}, -40^{\circ}\text{C} \le T_{J} \le +125^{\circ}\text{C}$ $V_{OUT1} \text{ OFF}$ $f = 120\text{Hz}$ $10\text{mA DC and } 1\text{mA rms}, 100\text{Hz} - 10\text{kHz}$		2 66 200 20		n c n mV
Load Regulation Quiescent Current Ripple Rejection Current Limit Long Term Stability Output Impedance	$1\text{mA} \le I_{OUT2} \le 100\text{mA}$ $I_{OUT2} \le 10\text{mA}, -40^{\circ}\text{C} \le T_{J} \le +125^{\circ}\text{C}$ $V_{OUT1} \text{ OFF}$ $f = 120\text{Hz}$ $10\text{mA DC and } 1\text{mA rms}, 100\text{Hz} - 10\text{kHz}$		2 66 200 20		m cc mV

Package Lead Description		
PACTO GELEVADO		FUNCTION
5 Lead TO-220		
1	$V_{IN}$	Supply voltage, usually direct from battery.
2	$V_{OUT1}$	Regulated output 8V, 750mA (typ).
3	Gnd	Ground connection.
4	ENABLE	CMOS compatible input lead; switches $V_{OUT1}$ on and off. When ENABLE is high, $V_{OUT1}$ is active.
5	$V_{OUT2}$	Standby output 5V, 100mA (typ); always on.

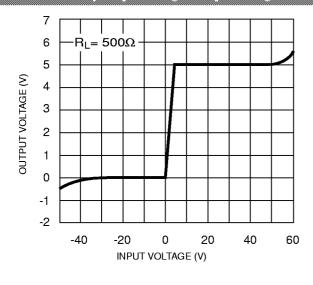
Dropout Voltage of Calcul Conces



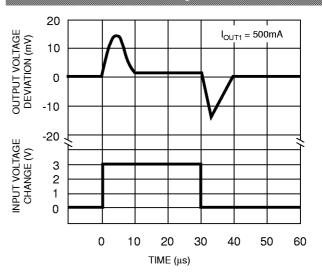
## One of the second second second



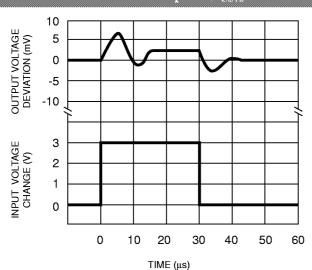
## Standby Conout Voltage vs. Input Voltage



## District control of the second of the



# Line Transien Response (V<sub>eter</sub>)



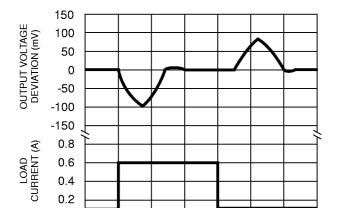
0.4

0.2 0

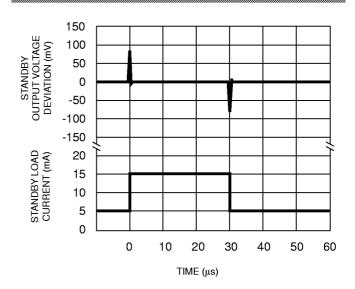
0

# **Typical Performance Characteristics**

# 



Lose Transfert Response V



Quiescen Concai ve Calpu Concai

20

TIME (µs)

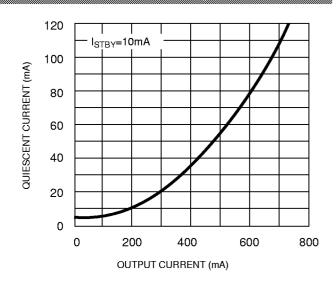
30

40

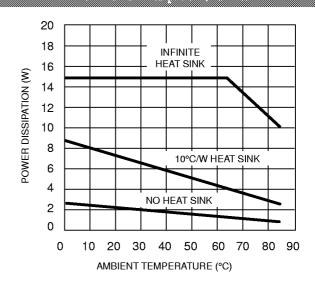
50

60

10



## Maximum Power Dissipation (C9-228)



#### **Definition of Terms**

#### **Dropout Voltage**

The input-output voltage differential at which the circuit ceases to regulate against further reduction in input voltage. Measured when the output voltage has dropped 100mV from the nominal value obtained at 14V input, dropout voltage is dependent upon load current and junction temperature.

#### Input Voltage

The DC voltage applied to the input terminals with respect to ground.

#### Input Output Differential

The voltage difference between the unregulated input voltage and the regulated output voltage for which the regulator will operate.

#### Line Regulation

The change in output voltage for a change in the input voltage. The measurement is made under conditions of low dissipation or by using pulse techniques such that the average chip temperature is not significantly affected.

#### Load Regulation

The change in output voltage for a change in load current at constant chip temperature.

#### **Long Term Stability**

Output voltage stability under accelerated life-test conditions after 1000 hours with maximum rated voltage and junction temperature.

#### **Output Noise Voltage**

The rms AC voltage at the output, with constant load and no input ripple, measured over a specified frequency range.

#### **Quiescent Current**

The part of the positive input current that does not contribute to the positive load current. i.e., the regulator ground lead current.

#### Ripple Rejection

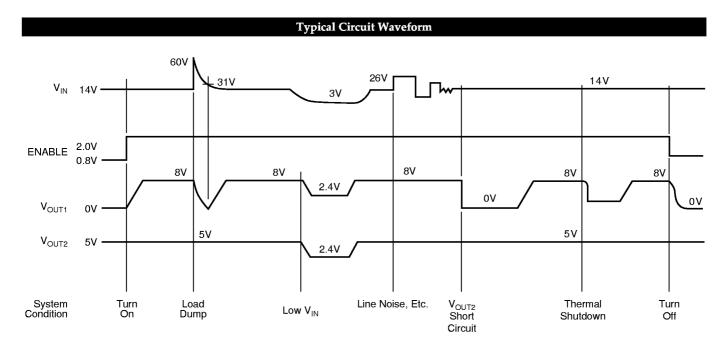
The ratio of the peak-to-peak input ripple voltage to the peak-to-peak output ripple voltage.

#### Temperature Stability of VOUT

The percentage change in output voltage for a thermal variation from room temperature to either temperature extreme.

#### **Current Limit**

Peak current that can be delivered to the output.



#### **Circuit Description**

#### Standby Output

The CS-8164 is equipped with two outputs. The second output is intended for use in systems requiring standby memory circuits. While the high current primary output can be controlled with the ENABLE lead described below, the standby output remains on under all conditions as long as sufficient input voltage is applied to the IC. Thus, memory and other circuits powered by this output remain unaffected by positive line transients, thermal shutdown, etc.

The standby regulator circuit is designed so that the quiescent current to the IC is very low (<2mA) when the other regulator output is off.

In applications where the standby output is not needed, it may be disabled by connecting a resistor from the standby output to the supply voltage. This eliminates the need for a capacitor on the output to prevent unwanted oscillations. The value of the resistor depends upon the minimum input voltage expected for a given system. Since the standby output is shunted with an internal 6.0V Zener, the current through the external resistor should be sufficient

NOTES:

supply filter.

\*\* C<sub>2</sub>, C<sub>3</sub> required for stability.

#### Circuit Description: continued

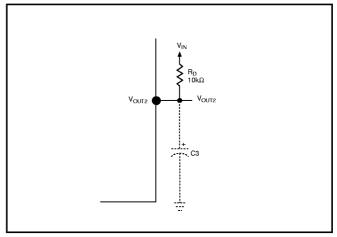
to bias V<sub>OUT2</sub> up to this point. Approximately 60µA will suffice, resulting in a  $10k\Omega$  external resistor for most applications.

#### 

Unlike the standby regulated output, which must remain on whenever possible, the high current regulated output is fault protected against overvoltage and also incorporates thermal shutdown. If the input voltage rises above approximately 30V (e.g., load dump), this output will automatically shutdown. This protects the internal circuitry and enables the IC to survive higher voltage transients than would otherwise be expected. Thermal shutdown is effective against die overheating since the high current output is the dominant source of power dissipation in the IC.

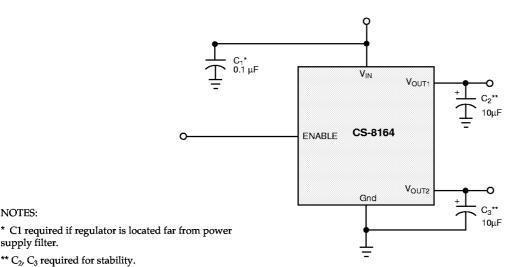
#### 06,79,71,100

The enable function controls  $V_{OUT1}$  When ENABLE is high (5V), V<sub>OUT1</sub> is on. When ENABLE is low, V<sub>OUT1</sub> is off.



Disabling V<sub>OUT2</sub> when it is not needed. C3 is no longer needed.

# **Test & Application Circuit**



#### **Application Notes**

#### Stability Considerations

The output or compensation capacitor helps determine three main characteristics of a linear regulator: start-up delay, load transient response and loop stability.

The capacitor value and type should be based on cost, availability, size and temperature constraints. A tantalum or aluminum electrolytic capacitor is best, since a film or ceramic capacitor with almost zero ESR can cause instability. The aluminum electrolytic capacitor is the least expensive solution, but, if the circuit operates at low temperatures (-25°C to -40°C), both the value and ESR of the capacitor will vary considerably. The capacitor manufacturers data sheet usually provides this information.

The value for each output capacitor shown in the test and applications circuit should work for most applications, however it is not necessarily the optimized solution.

To determine acceptable values for  $C_2$  and  $C_3$  a particular application, start with a tantalum capacitor of the recommended value and work towards a less expensive alternative part for each output.

**Step 1:** Place the completed circuit with the tantalum capacitors of the recommended values in an environmental chamber at the lowest specified operating temperature and monitor the outputs with an oscilloscope. A decade box connected in series with the capacitor C<sub>2</sub> will simulate the higher ESR of an aluminum capacitor. Leave the decade box outside the chamber, the small resistance added by the longer leads is negligible.

Step 2: With the input voltage at its maximum value, increase the load current slowly from zero to full load on the output under observation. look for oscillations on the output. If no oscillations are observed, the capacitor is large enough to ensure a stable design under steady state conditions.

#### **Application Notes: continued**

**Step 3:** Increase the ESR of the capacitor from zero using the decade box and vary the load current until oscillations appear. Record the values of load current and ESR that cause the greatest oscillation. This represents the worst case load conditions for the output at low temperature.

**Step 4:** Maintain the worst case load conditions set in step 3 and vary the input voltage until the oscillations increase. This point represents the worst case input voltage conditions

**Step 5:** If the capacitor is adequate, repeat steps 3 and 4 with the next smaller valued capacitor. A smaller capacitor will usually cost less and occupy less board space. If the output oscillates within the range of expected operating conditions, repeat steps 3 and 4 with the next larger standard capacitor value.

**Step 6:** Test the load transient response by switching in various loads at several frequencies to simulate its real working environment. Vary the ESR to reduce ringing.

**Step 7:** Remove the unit from the environmental chamber and heat the IC with a heat gun. Vary the load current as instructed in step 5 to test for any oscillations.

Once the minimum capacitor value with the maximum ESR is found for each output, a safety factor should be added to allow for the tolerance of the capacitor and any variations in regulator performance. Most good quality aluminum electrolytic capacitors have a tolerance of +/-20% so the minimum value found should be increased by at least 50% to allow for this tolerance plus the variation which will occur at low temperatures. The ESR of the capacitors should be less than 50% of the maximum allowable ESR found in step 3 above.

Repeat steps 1 through 7 with the capacitor on the other output, C<sub>3</sub>.

#### Calculating Power Disapation in a Dual Calput Linear Regulator

The maximum power dissipation for a dual output regulator (Figure 1) is:

$$\begin{split} P_{D(max)} &= \{V_{IN(max)} - V_{OUTI(min)}\}I_{OUT1(max)} + \\ &\{V_{IN(max)} - V_{OUT2(min)}\}I_{OUT2(max)} + V_{IN(max)}I_{Q} \end{split} \tag{1}$$

where:

 $V_{IN(max)}$  is the maximum input voltage,

 $V_{OUT1(min)}$  is the minimum output voltage from  $V_{OUT1}$ ,

 $V_{OUT2(min)}$  is the minimum output voltage from  $V_{OUT2}$ ,

 $I_{OUT1(max)}$  is the maximum output current for the application

 $I_{\text{OUT2(max)}}$  is the maximum output current for the application, and

 $I_Q$  is the quiescent current the regulator consumes at  $I_{\text{OUT}(\text{max})}$ 

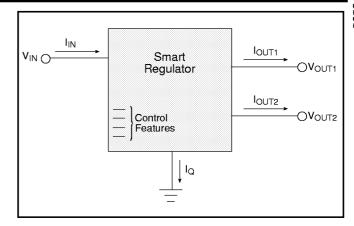


Figure 1: Dual output regulator with key performance parameters labeled.

Once the value of  $P_{D(max)}$  is known, the maximum permissible value of  $R_{\Theta JA}$  can be calculated:

$$R_{\Theta JA} = \frac{150^{\circ} \text{C - T}_{A}}{P_{D}}$$
 (2)

The value of  $R_{\odot JA}$  can then be compared with those in the package section of the data sheet. Those packages with  $R_{\odot JA}$ 's less than the calculated value in equation 2 will keep the die temperature below 150°C.

In some cases, none of the packages will be sufficient to dissipate the heat generated by the IC, and an external heatsink will be required.

#### Heat Sinks

A heat sink effectively increases the surface area of the package to improve the flow of heat away from the IC and into the surrounding air.

Each material in the heat flow path between the IC and the outside environment will have a thermal resistance. Like series electrical resistances, these resistances are summed to determine the value of  $R_{\Theta IA}$ :

$$R_{\Theta JA} = R_{\Theta JC} + R_{\Theta CS} + R_{\Theta SA}$$
 (3)

where:

 $R_{\Theta JC}$  = the junction-to-case thermal resistance,

 $R_{\Theta CS}$  = the case-to-heatsink thermal resistance, and

 $R_{\Theta SA}$  = the heatsink-to-ambient thermal resistance.

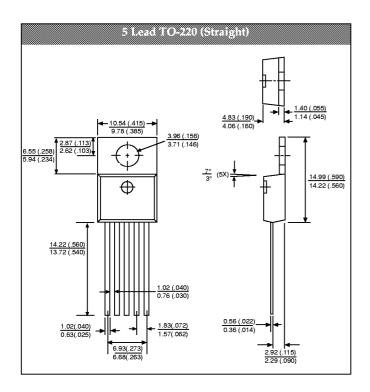
 $R_{\text{OJC}}$  appears in the package section of the data sheet. Like  $R_{\text{OJA}}$ , it too is a function of package type.  $R_{\text{OCS}}$  and  $R_{\text{OSA}}$  are functions of the package type, heatsink and the interface between them. These values appear in heat sink data sheets of heat sink manufacturers.

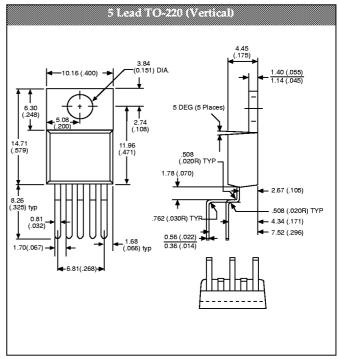
## **Package Specification**

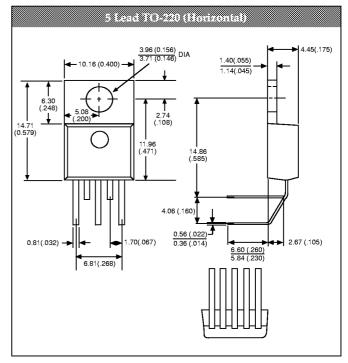
#### 

#### PACER ACED HERRINA A DINA CA

Thermal Data		Data 5 Lead TO-220	
$R_{\Theta JC}$	typ	2.0	°C/W
$R_{\Theta JA}$	typ	50	°C/W







# 

Part Number	Description
CS-8164T5	5 Lead TO-220 Straight
CS-8164TV5	5 Lead TO-220 Vertical
CS-8164TH5	5 Lead TO-220 Horizontal

Cherry Semiconductor Corporation reserves the right to make changes to the specifications without notice. Please contact Cherry Semiconductor Corporation for the latest available information.