



LS404

HIGH PERFORMANCE QUAD OPERATIONAL AMPLIFIER

- SINGLE OR SPLIT SUPPLY OPERATION
- LOW POWER CONSUMPTION
- SHORT CIRCUIT PROTECTION
- LOW DISTORTION, LOW NOISE
- HIGH GAIN-BANDWIDTH PRODUCT
- HIGH CHANNEL SEPARATION

DESCRIPTION

The LS404 is a high performance quad operational amplifier with frequency and phase compensation built into the chip. The internal phase compensation allows stable operation as voltage follower in spite of its high Gain-Bandwidth Product.

The circuit presents very stable electrical characteristics over the entire supply voltage range, and is particularly intended for professional and telecom applications (active filter, etc).

The patented input stage circuit allows small input signal swings below the negative supply voltage and prevents phase inversion when the inputs are over drivers.

ORDER CODE

| Part Number | Temperature Range | Package | |
|-------------|-------------------|---------|---|
| | | N | D |
| LS404C | 0°C, +70°C | • | • |
| LS404I | -40°C, +105°C | • | • |
| LS404M | -55°C, +125°C | • | • |

Example : LS204CN

N = Dual in Line Package (DIP)

D = Small Outline Package (SO) - also available in Tape & Reel (DT)

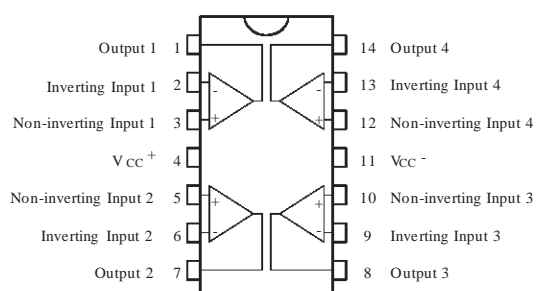


N
DIP14
(Plastic Package)



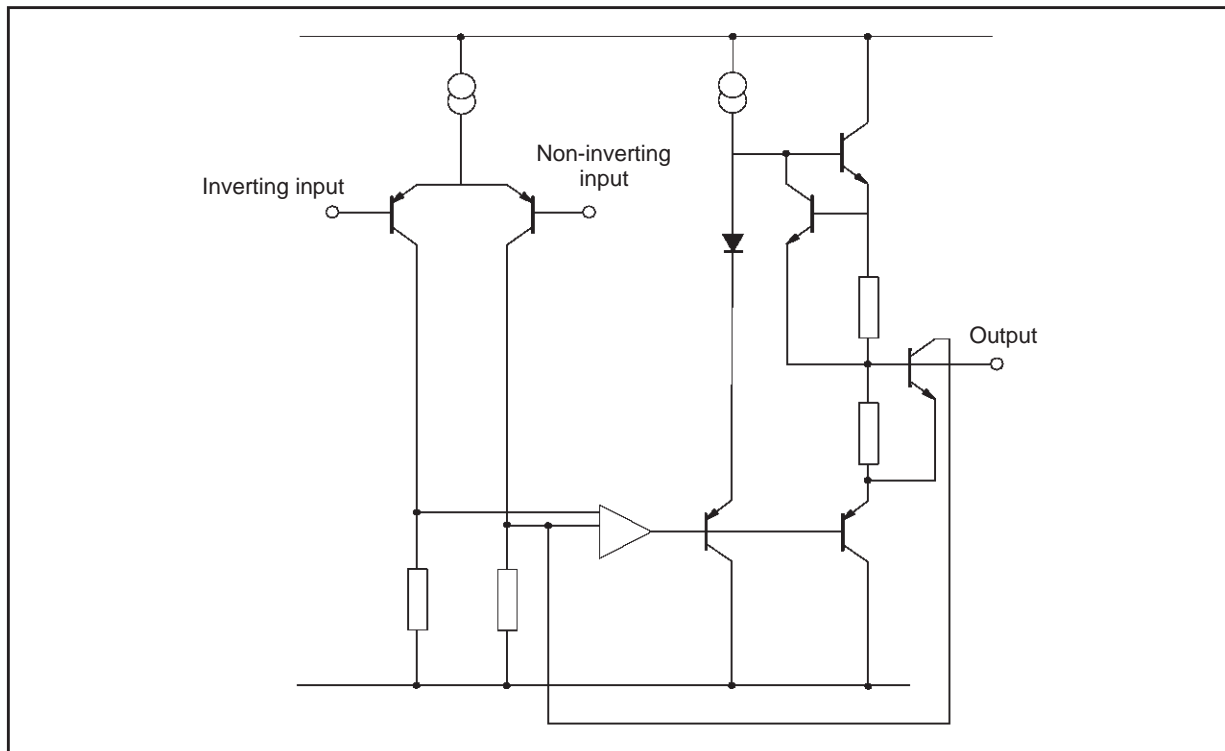
D
SO14
(Plastic Micropackage)

PIN CONNECTIONS (top view)



LS404

SCHEMATIC DIAGRAM (1/4 LS404)



ABSOLUTE MAXIMUM RATINGS

| Symbol | Parameter | Value | Unit |
|------------|---|----------------------------|--------------------|
| V_{CC} | Supply voltage | ± 18 | V |
| V_i | Input Voltage | Positive Negative | V |
| V_{id} | Differential Input Voltage | $\pm(V_{CC} - 1)$ | V |
| T_{oper} | Operating Temperature Range | LS204C LS204I LS204I | $^{\circ}\text{C}$ |
| P_{tot} | Power Dissipation at $T_{amb} = 70^{\circ}\text{C}$ | 400 | mW |
| T_{stg} | Storage Temperature Range | -65 to +150 | $^{\circ}\text{C}$ |

ELECTRICAL CHARACTERISTICS $V_{CC} = \pm 15V$, $T_{amb} = 25^{\circ}C$ (unless otherwise specified)

| Symbol | Parameter | LS404I - LS404M | | | LS404C | | | Unit |
|-----------------|---|-----------------|---------------|------|----------|----------------|------|------------------------|
| | | Min. | Typ. | Max. | Min. | Typ. | Max. | |
| I_{CC} | Supply Current | | 1.3 | 2 | | 1.5 | 3 | mA |
| I_{ib} | Input Bias Current | | 50 | 200 | | 100 | 300 | nA |
| R_i | Input Resistance ($f = 1kHz$) | | 1 | | | 1 | | M Ω |
| V_{io} | Input Offset Voltage ($R_s \leq 10k\Omega$) | | 0.7 | 2.5 | | 0.5 | 5 | mV |
| DV_{io} | Input Offset Voltage Drift ($R_s \leq 10k\Omega$) $T_{min} < T_{op} < T_{max}$ | | 5 | | | 5 | | $\mu V/^{\circ}C$ |
| I_{io} | Input Offset Current | | 10 | 40 | | 20 | 80 | nA |
| DI_{io} | Input Offset Current Drift $T_{min} < T_{op} < T_{max}$ | | 0.08 | | | 0.1 | | nA/ $^{\circ}C$ |
| I_{os} | Output Short-circuit Current | | 23 | | | 23 | | mA |
| A_{vd} | Large Signal Voltage Gain $R_L = 2k\Omega$, $V_{CC} = \pm 15V$ $V_{CC} = \pm 4V$ | 90 | 100 95 | | 86 | 100 95 | | dB |
| GBP | Gain Bandwidth Product $f = 100kHz$, $R_L = 2k$, $C_L = 100pF$ | 1.8 | 3 | | 1.5 | 2.5 | | MHz |
| e_n | Equivalent Input Noise Voltage $f = 1kHz$, $R_s = 50\Omega$ $R_s = 1k\Omega$ $R_s = 10k\Omega$ | | 8 10 18 | 15 | | 10 12 20 | | $\frac{nV}{\sqrt{Hz}}$ |
| THD | Total Harmonic Distortion Unity Gain $R_L = 2k\Omega$, $V_o = 2V_{pp}$ $f = 1kHz$ $f = 20kHz$ | | 0.01 0.03 | 0.4 | | 0.01 0.03 | | % |
| $\pm V_{opp}$ | Output Voltage Swing $R_L = 2k\Omega$, $V_{CC} = \pm 15V$ $V_{CC} = \pm 4V$ | ± 13 | ± 3 | | ± 13 | ± 3 | | V |
| V_{opp} | Large Signal Voltage Swing $f = 10kHz$, $R_L = 10k\Omega$ $R_L = 1k\Omega$ | | 22 20 | | | 22 20 | | V _{pp} |
| SR | Slew Rate ($R_L = 2k\Omega$, unity gain) | 0.8 | 1.5 | | | 1 | | V/ μs |
| SVR | Supply Voltage Rejection Ratio $V_{ic} = 1V$, $f = 100Hz$ | 90 | 94 | | 86 | 90 | | dB |
| CMR | Common Mode Rejection Ratio $V_{ic} = 10V$ | 90 | 94 | | 86 | 90 | | dB |
| V_{o1}/V_{o2} | Channel Separation ($f = 1kHz$) | 100 | 120 | | | 120 | | dB |

Figure 1 : Supply Current versus Supply Voltage

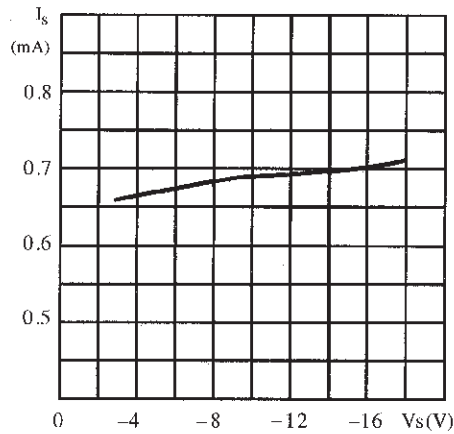


Figure 2 : Supply Current versus Ambient Temperature

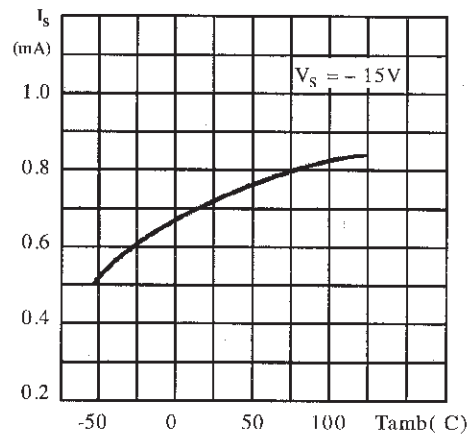


Figure 3 : Output Short Circuit Current versus Ambient Temperature

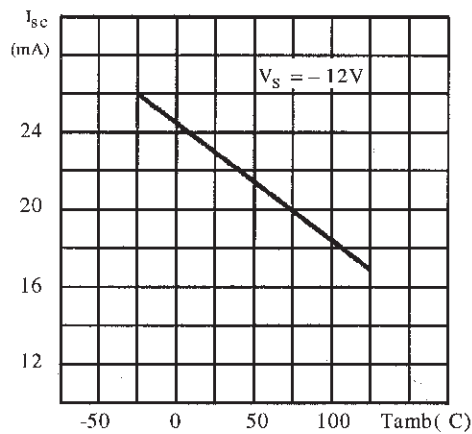


Figure 4 : Open Loop Frequency and Phase Response

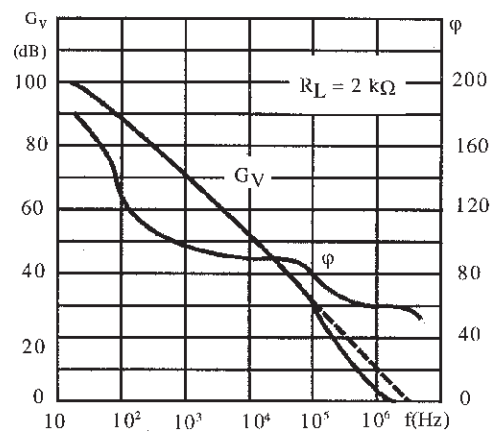


Figure 5 : Output Loop Gain versus Ambient Temperature

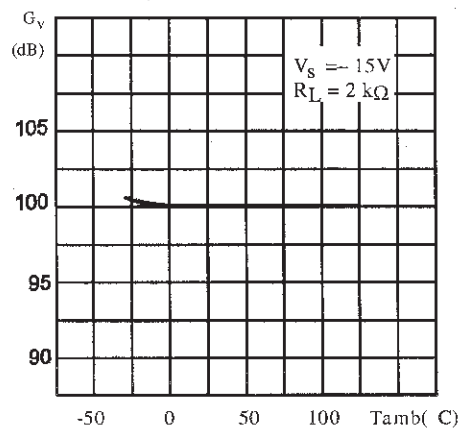


Figure 6 : Supply Voltage Rejection versus Frequency

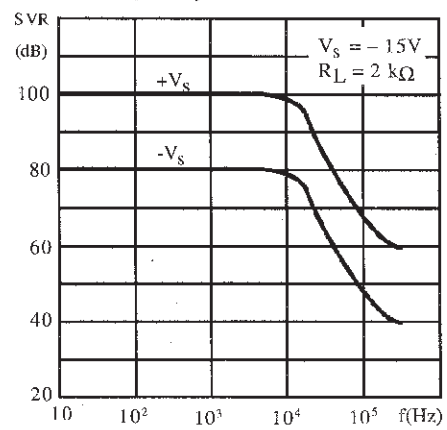


Figure 7 : Large Signal Frequency Response

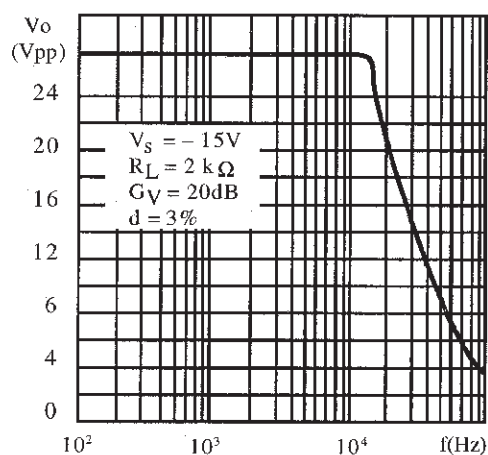


Figure 8 : Output Voltage Swing versus Load Resistance

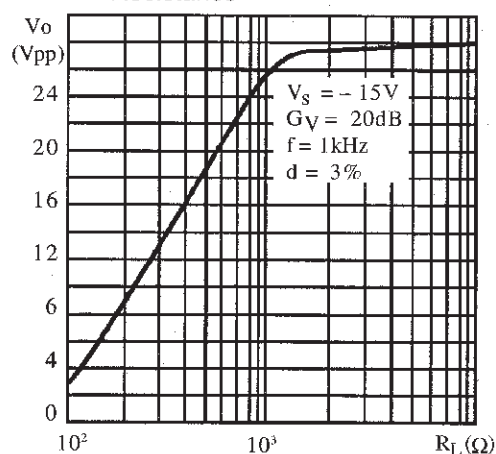


Figure 9 : Total Input Noise versus Frequency

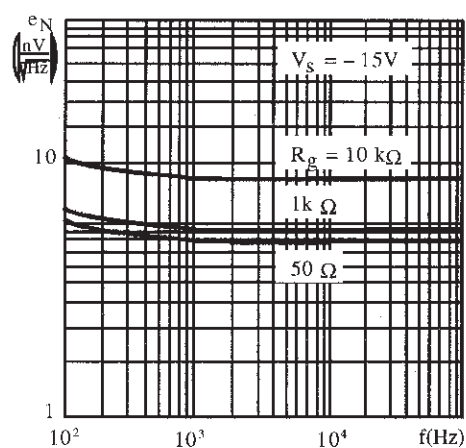


Figure 10 : Amplitude Response

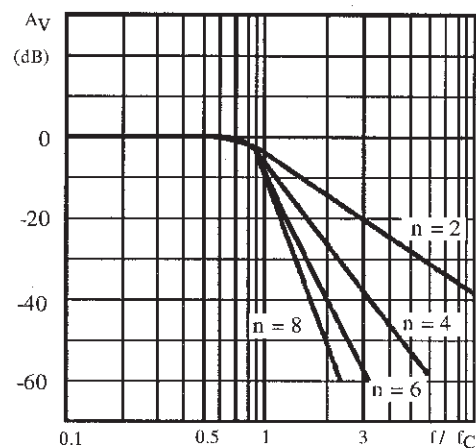
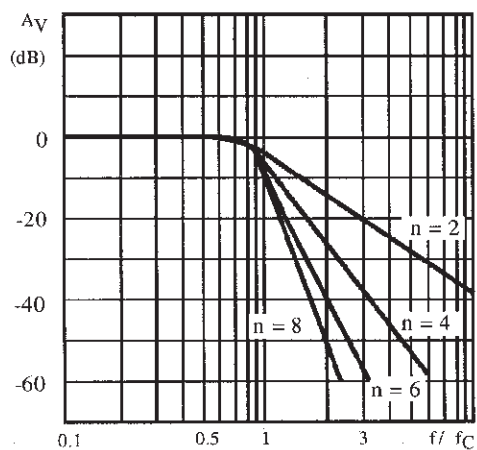
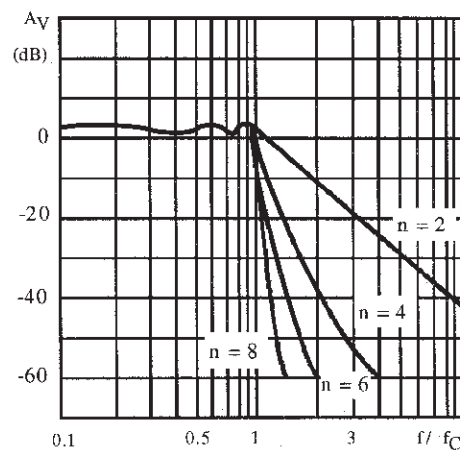


Figure 11 : Amplitude Response

Figure 12 : Amplitude Response ($\pm 1\text{dB}$ ripple)

APPLICATION INFORMATION: Active low-pass filter**BUTTERWORTH**

The Butterworth is a "maximally flat" amplitude response filter (figure 10). Butterworth filters are used for filtering signals in data acquisition systems to prevent aliasing errors in samples-data applications and for general purpose low-pass filtering.

The cut-off frequency F_c , is the frequency at which the amplitude response is down 3dB. The attenuation rate beyond the cutoff frequency is $n6$ dB per octave of frequency where n is the order (number of poles) of the filter.

Other characteristics :

- ☐ Flattest possible amplitude response
- ☐ Excellent gain accuracy at low frequency end of passband

BESSEL

The Bessel is a type of "linear phase" filter. Because of their linear phase characteristics, these filters approximate a constant time delay over a limited frequency range. Bessel filters pass transient waveforms with a minimum of distortion. They are also used to provide time delays for low pass filtering of modulated waveforms and as a "running average" type filter.

The maximum phase shift is $\frac{-n\pi}{2}$ radians where

n is the order (number of poles) of the filter. The cut-off frequency f_c , is defined as the frequency at which the phase shift is one half of this value.

The table below shows the typical overshoot and settling time response of the low pass filters to a step input.

For accurate delay, the cut-off frequency should be twice the maximum signal frequency.

The following table can be used to obtain the -3dB frequency of the filter.

| | 2 Pole | 4 Pole | 6 Pole | 8 Pole |
|----------------|------------|------------|------------|------------|
| -3dB Frequency | 0.77 f_c | 0.67 f_c | 0.57 f_c | 0.50 f_c |

Other characteristics :

- ☐ Selectivity not as great as Chebyshev or Butterworth
- ☐ Very little overshoot response to step inputs
- ☐ Fast rise time

CHEBYSHEV

Chebyshev filters have greater selectivity than either Bessel or Butterworth at the expense of ripple in the passband (figure 11).

Chebyshev filters are normally designed with peak-to-peak ripple values from 0.2dB to 2dB.

Increased ripple in the passband allows increased attenuation above the cut-off frequency.

The cut-off frequency is defined as the frequency at which the amplitude response passes through the specified maximum ripple band and enters the stop band.

Other characteristics :

- ☐ Greater selectivity
- ☐ Very non-linear phase response
- ☐ High overshoot response to step inputs

| | Number of Poles | Peak Overshoot | Settling Time (% of final value) | | |
|----------------------------|-----------------|----------------|----------------------------------|----------------|----------------|
| | | % Overshoot | ±1% | ±0.1% | ±0.01% |
| Butterworth | 2 | 4 | 1.1 F_c sec. | 1.7 F_c sec. | 1.9 F_c sec. |
| | 4 | 11 | 1.7/ f_c | 2.8/ f_c | 3.8/ f_c |
| | 6 | 14 | 2.4/ f_c | 3.9S/ f_c | 5.0S/ f_c |
| | 8 | 14 | 3.1/ f_c | 5.1/ f_c | 7.1/ f_c |
| Bessel | 2 | 0.4 | 0.8/ f_c | 1.4/ f_c | 1.7/ f_c |
| | 4 | 0.8 | 1.0/ f_c | 1.8/ f_c | 2.4/ f_c |
| | 6 | 0.6 | 1.3/ f_c | 2.1/ f_c | 2.7/ f_c |
| | 8 | 0.1 | 1.6/ f_c | 2.3/ f_c | 3.2/ f_c |
| Chebyshev (ripple ±0.25dB) | 2 | 11 | 1.1/ f_c | 1.6/ f_c | - |
| | 4 | 18 | 3.0/ f_c | 5.4/ f_c | - |
| | 6 | 21 | 5.9/ f_c | 10.4/ f_c | - |
| | 8 | 23 | 8.4/ f_c | 16.4/ f_c | - |
| Chebyshev (ripple ±1dB) | 2 | 21 | 1.6/ f_c | 2.7/ f_c | - |
| | 4 | 28 | 4.8/ f_c | 8.4/ f_c | - |
| | 6 | 32 | 8.2/ f_c | 16.3/ f_c | - |
| | 8 | 34 | 11.6/ f_c | 24.8/ f_c | - |

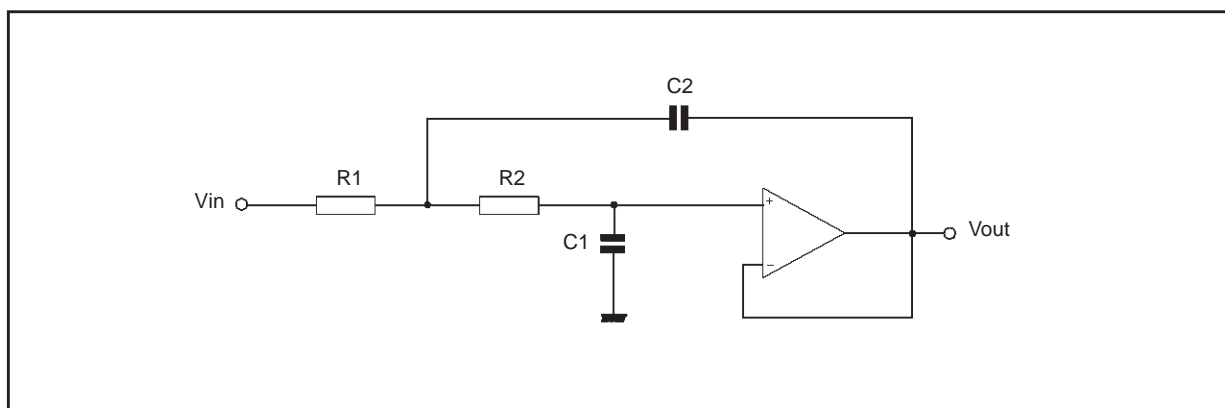
Design of 2nd order active low pass filter (Sallen and Key configuration unity gain op-amp)

Fixed $R = R_1 = R_2$, we have (see figure 13)

$$C_1 = \frac{1}{R} \frac{\xi}{\omega_c}$$

$$C_2 = \frac{1}{R} \frac{1}{\xi \omega_c}$$

Figure 13 : Filter Configuration



Three parameters are needed to characterize the frequency and phase response of a 2nd order active filter: the gain (G_v), the damping factor (ξ) or the Q factor ($Q = 2\xi^{-1}$), and the cutoff frequency (f_c).

The higher order response are obtained with a series of 2nd order sections. A simple RC section is introduced when an odd filter is required.

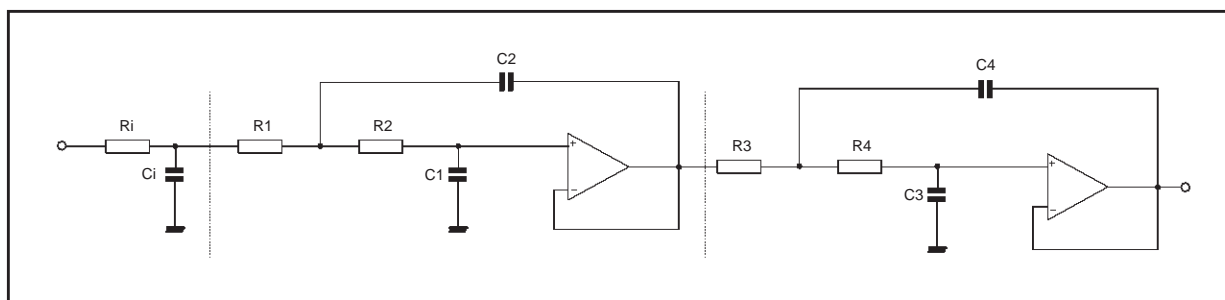
The choice of ' ξ ' (or Q factor) determines the filter response (see table 1).

Table 1

| Filter Response | ξ | Q | Cutoff Frequency f_c |
|-----------------|----------------------|----------------------|---|
| Bessel | $\frac{\sqrt{3}}{2}$ | $\frac{\sqrt{1}}{3}$ | Frequency at which Phase Shift is -90° |
| Butterworth | $\frac{\sqrt{2}}{2}$ | $\frac{\sqrt{1}}{2}$ | Frequency at which $G_v = -3\text{dB}$ |
| Chebyshev | $\frac{\sqrt{2}}{2}$ | $\frac{\sqrt{1}}{2}$ | Frequency at which the amplitude response passes through specified max. ripple band and enters the stop bank. |

EXAMPLE

Figure 14 : 5th Order Low-pass Filter (Butterworth) with Unity Gain configuration



In the circuit of figure 14, for $f_c = 3.4\text{kHz}$ and $R_i = R_1 = R_2 = R_3 = 10\text{k}\Omega$, we obtain:

$$C_i = 1.354 \frac{1}{R} \frac{1}{2\pi f_c} = 6.33\text{nF}$$

$$C_1 = 0.421 \frac{1}{R} \frac{1}{2\pi f_c} = 1.97\text{nF}$$

$$C_2 = 1.753 \frac{1}{R} \frac{1}{2\pi f_c} = 8.20\text{nF}$$

$$C_3 = 0.309 \frac{1}{R} \frac{1}{2\pi f_c} = 1.45\text{nF}$$

$$C_4 = 3.325 \frac{1}{R} \frac{1}{2\pi f_c} = 15.14\text{nF}$$

The attenuation of the filter is 30dB at 6.8kHz and better than 60dB at 15kHz.

The same method, referring to table 2 and figure 15 is used to design high-pass filter. In this case the damping factor is found by taking the reciprocal of the numbers in table 2. For $f_c = 5\text{kHz}$ and $C_i = C_1 = C_2 = C_3 = 1\text{nF}$ we obtain:

$$R_i = \frac{1}{0.354} \frac{1}{C} \frac{1}{2\pi f_c} = 25.5\text{k}\Omega$$

$$R_1 = \frac{1}{0.421} \frac{1}{C} \frac{1}{2\pi f_c} = 75.6\text{k}\Omega$$

$$R_2 = \frac{1}{1.753} \frac{1}{C} \frac{1}{2\pi f_c} = 18.2\text{k}\Omega$$

$$R_3 = \frac{1}{0.309} \frac{1}{C} \frac{1}{2\pi f_c} = 103\text{k}\Omega$$

$$R_4 = \frac{1}{3.325} \frac{1}{C} \frac{1}{2\pi f_c} = 9.6\text{k}\Omega$$

Table 2 : Damping Factor for Low-pass Butterworth Filters

| Order | C_i | C_1 | C_2 | C_3 | C_4 | C_5 | C_6 | C_7 | C_8 |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 2 | | 0.707 | 1.41 | | | | | | |
| 3 | 1.392 | 0.202 | 3.54 | | | | | | |
| 4 | | 0.92 | 1.08 | 0.38 | 2.61 | | | | |
| 5 | 1.354 | 0.421 | 1.75 | 0.309 | 3.235 | | | | |
| 6 | | 0.966 | 1.035 | 0.707 | 1.414 | 0.259 | 3.86 | | |
| 7 | 1.336 | 0.488 | 1.53 | 0.623 | 1.604 | 0.222 | 4.49 | | |
| 8 | | 0.98 | 1.02 | 0.83 | 1.20 | 0.556 | 1.80 | 0.195 | 5.125 |

Figure 15 : 5th Order High-pass Filter (Butterworth) with Unity Gain configuration

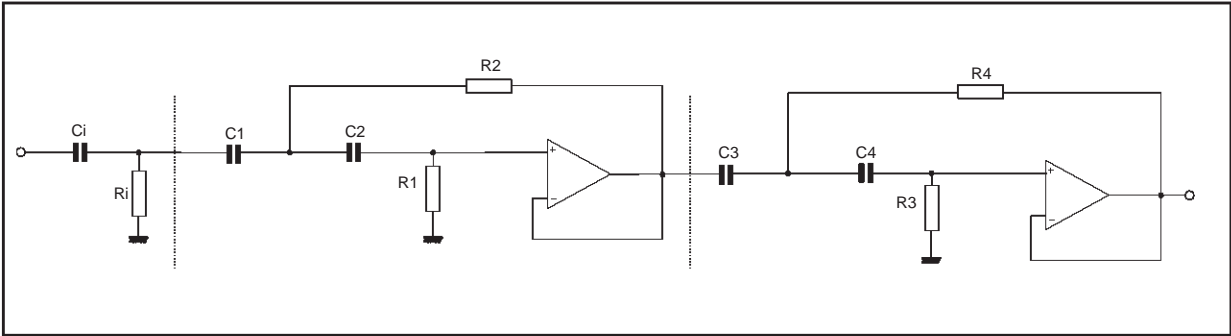
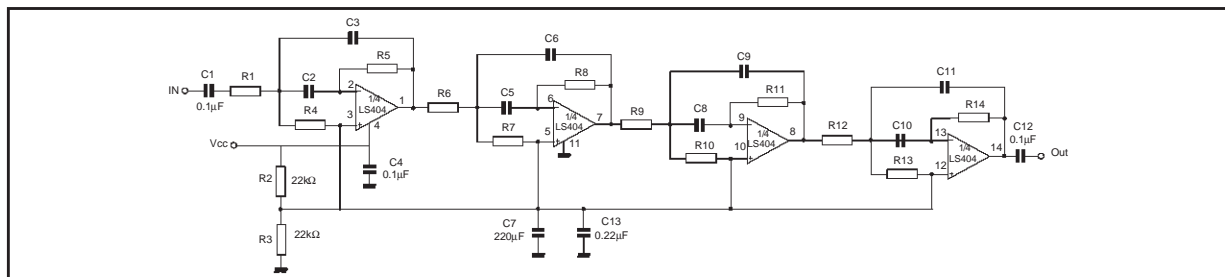
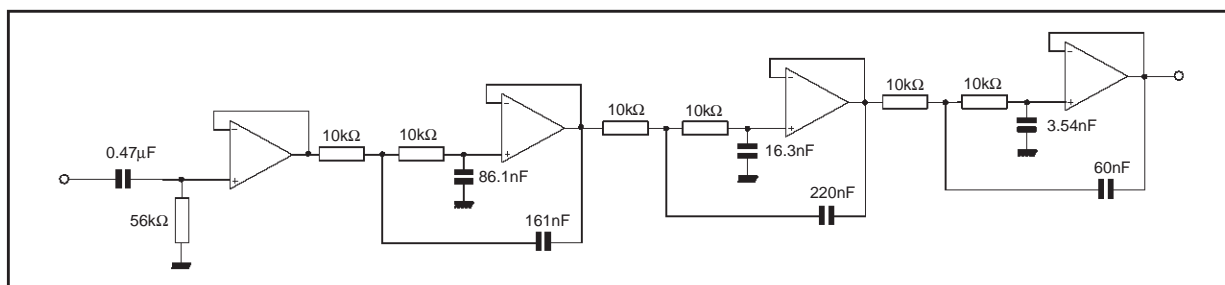
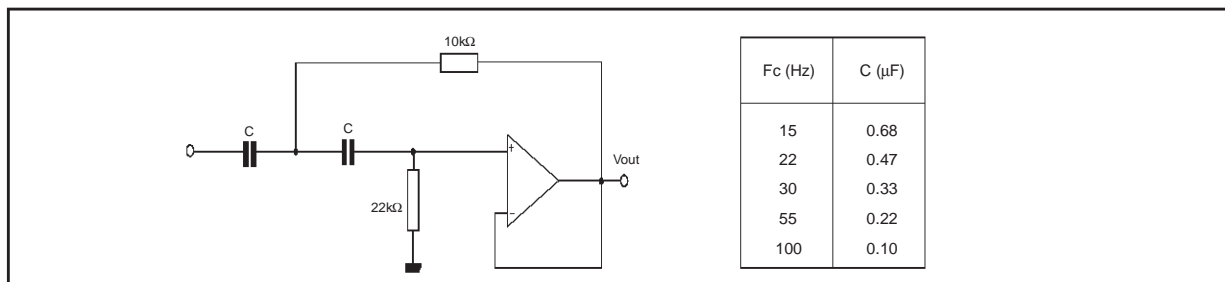
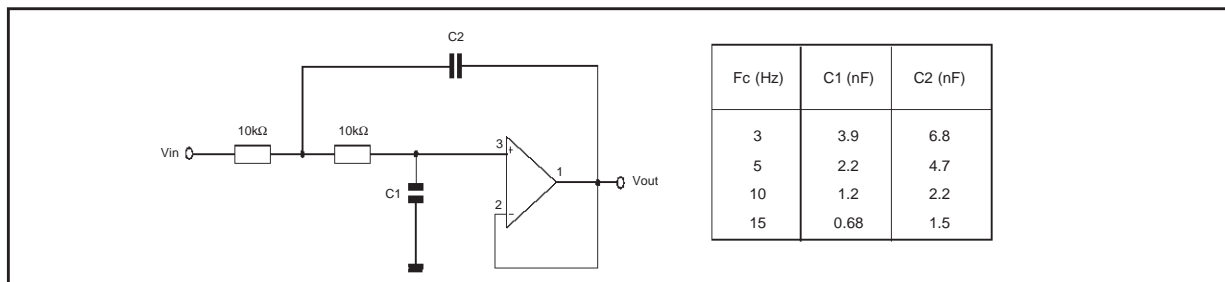


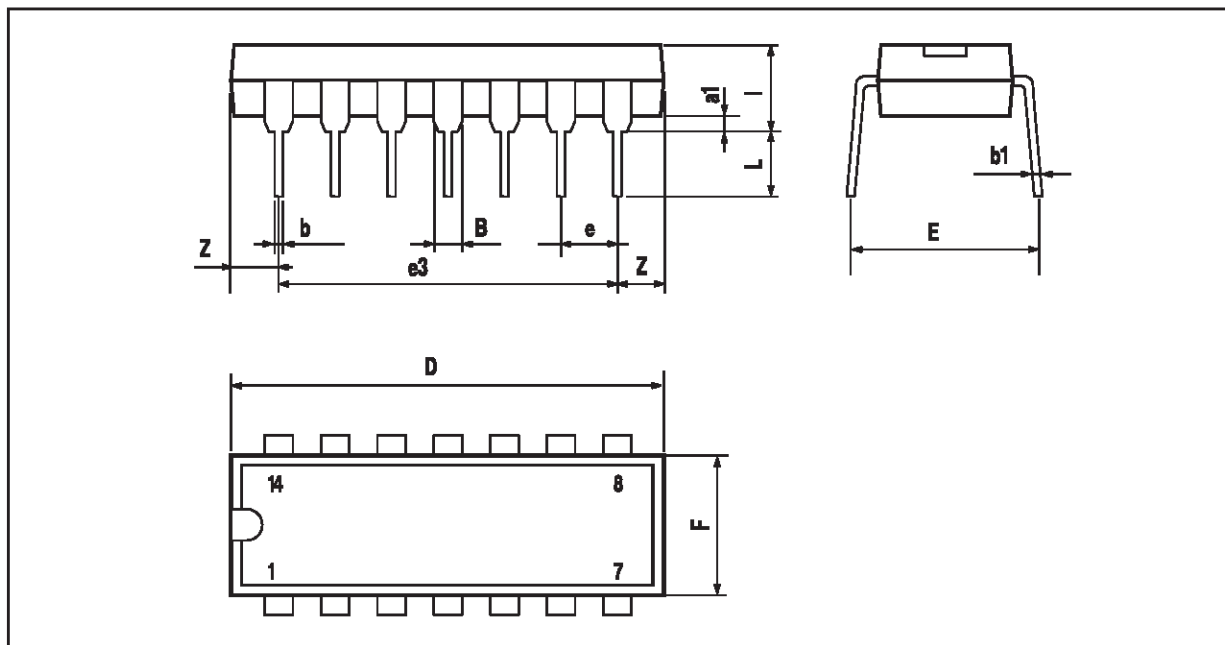
Figure 16 : Multiple Feedback 8-pole Bandpass Filter**Figure 17 : Six pole 355Hz Low-pass Filter (chebychev type)**

This is a - pole Chebyshev type with $\pm 0.25\text{dB}$ ripple in the passband. A decoupling stage is used to avoid the influence of the input impedance on the filter's characteristics. The attenuation is about 55dB at 710Hz and reaches 80dB at 1065Hz. the in band attenuation is limited in practise to the $\pm 0.25\text{dB}$ ripple and does not exceed 0.5dB at 0.9fc.

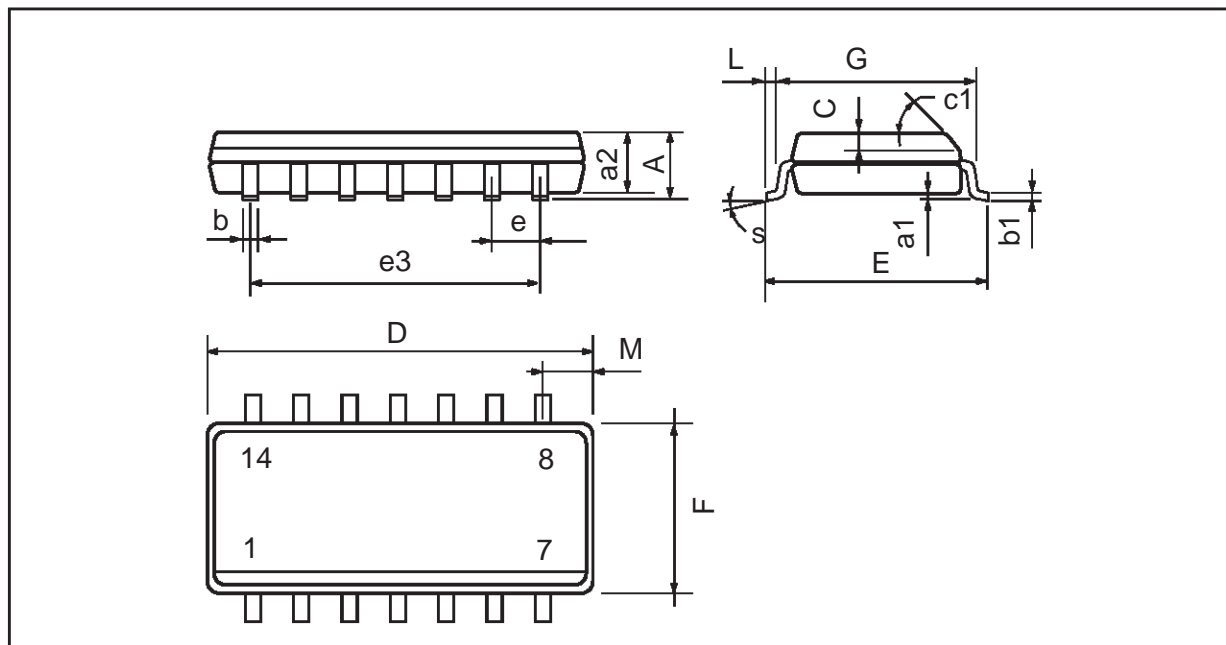
Figure 18 : Subsonic Filter ($G_v = 0\text{dB}$)**Figure 19 : High Cut filter ($G_v = 0\text{dB}$)**

LS404

PACKAGE MECHANICAL DATA 14 PINS - PLASTIC PACKAGE



| Dimensions | Millimeters | | | Inches | | |
|------------|-------------|-------|------|--------|-------|-------|
| | Min. | Typ. | Max. | Min. | Typ. | Max. |
| a1 | 0.51 | | | 0.020 | | |
| B | 1.39 | | 1.65 | 0.055 | | 0.065 |
| b | | 0.5 | | | 0.020 | |
| b1 | | 0.25 | | | 0.010 | |
| D | | | 20 | | | 0.787 |
| E | | 8.5 | | | 0.335 | |
| e | | 2.54 | | | 0.100 | |
| e3 | | 15.24 | | | 0.600 | |
| F | | | 7.1 | | | 0.280 |
| i | | | 5.1 | | | 0.201 |
| L | | 3.3 | | | 0.130 | |
| Z | 1.27 | | 2.54 | 0.050 | | 0.100 |

PACKAGE MECHANICAL DATA**14 PINS - PLASTIC MICROPACKAGE (SO)**

| Dimensions | Millimeters | | | Inches | | |
|------------|-------------|------|------|--------|-------|-------|
| | Min. | Typ. | Max. | Min. | Typ. | Max. |
| A | | | 1.75 | | | 0.069 |
| a1 | 0.1 | | 0.2 | 0.004 | | 0.008 |
| a2 | | | 1.6 | | | 0.063 |
| b | 0.35 | | 0.46 | 0.014 | | 0.018 |
| b1 | 0.19 | | 0.25 | 0.007 | | 0.010 |
| C | | 0.5 | | | 0.020 | |
| c1 | 45° (typ.) | | | | | |
| D (1) | 8.55 | | 8.75 | 0.336 | | 0.344 |
| E | 5.8 | | 6.2 | 0.228 | | 0.244 |
| e | | 1.27 | | | 0.050 | |
| e3 | | 7.62 | | | 0.300 | |
| F (1) | 3.8 | | 4.0 | 0.150 | | 0.157 |
| G | 4.6 | | 5.3 | 0.181 | | 0.208 |
| L | 0.5 | | 1.27 | 0.020 | | 0.050 |
| M | | | 0.68 | | | 0.027 |
| S | 8° (max.) | | | | | |

Note : (1) D and F do not include mold flash or protrusions - Mold flash or protrusions shall not exceed 0.15mm (.066 inc) ONLY FOR DATA BOOK.

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