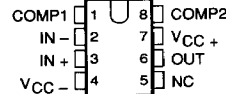


# LT1008M, LT1008C PICOAMP INPUT CURRENT, MICROVOLT OFFSET LOW-NOISE OPERATIONAL AMPLIFIERS

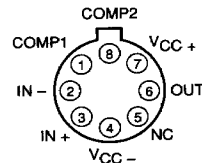
D3233, MAY 1988 – REVISED FEBRUARY 1989

- Input Bias Current . . .  $\pm 30$  pA Typ,  
 $\pm 100$  pA Max at 25°C
- Input Offset Voltage . . . 30  $\mu$ V Typ,  
120  $\mu$ V Max at 25°C
- Offset Voltage Temperature Coefficient . . .  
1.5  $\mu$ V/°C Max
- Low Peak-to-Peak Noise Voltage at  
0.1 Hz to 10 Hz . . . 0.5  $\mu$ V
- Low Supply Current . . . 380  $\mu$ A Typ,  
600  $\mu$ A Max at 25°C
- Supply Voltage Rejection Ratio . . . 114 dB  
Min at 25°C
- Common-Mode Rejection Ratio . . . 114 dB  
Min at 25°C
- High Voltage Amplification with 5-mA Load  
Current
- Applications:  
Precision Instrumentation  
Charge Integrators  
Wide-Dynamic-Range Logarithmic  
Amplifiers  
Light Meters  
Low-Frequency Active Filters  
Standard Cell Buffers  
Thermocouple Amplifiers

JG OR P PACKAGE  
(TOP VIEW)

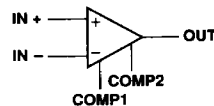


L PACKAGE  
(TOP VIEW)



NC – No internal connection  
Pin 4 (L Package) is in electrical contact  
with the case.

symbol



## description

The LT1008 is a precision operational amplifier that can be used in practically all precision applications. The LT1008 offers picoampere bias currents (maintained over the full temperature range), microvolt offset voltage, low offset voltage temperature coefficient and long-term drift, low voltage and current noise, and low power dissipation. Additionally, the LT1008's precision specifications include high common-mode and supply voltage rejection ratios. The LT1008 can deliver a 5-mA load current with high voltage amplification.

The LT1008 is externally compensated with a single capacitor to add flexibility in shaping the frequency response of the amplifier. The LT1008 is a pin-for-pin replacement for the LM108 series.

The LT1008M is characterized for operation over the full military temperature range of  $-55^{\circ}\text{C}$  to  $125^{\circ}\text{C}$ . The LT1008C is characterized for operation from  $0^{\circ}\text{C}$  to  $70^{\circ}\text{C}$ .

## AVAILABLE OPTIONS

T <sub>A</sub>	PACKAGE		
	CERAMIC DIP (JG)	METAL CAN (L)	PLASTIC DIP (P)
0°C to 70°C	LT1008CJG	LT1008CL	LT1008CP
-55°C to 125°C	LT1008MJG	LT1008ML	LT1008MP

PRODUCTION DATA documents contain information current as of publication date. Products conform to specifications per the terms of Texas Instruments standard warranty. Production processing does not necessarily include testing of all parameters.

TEXAS  
INSTRUMENTS

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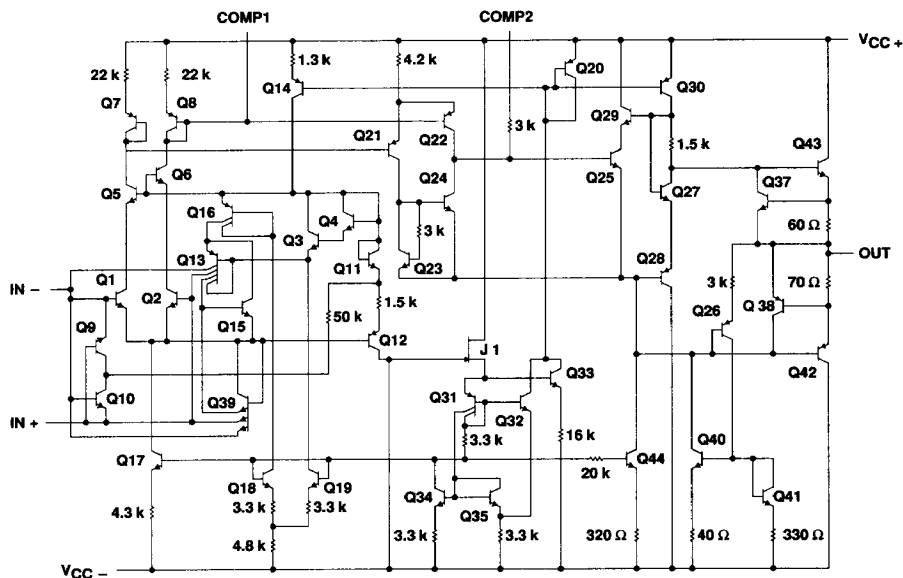
2

Operational Amplifiers



# LT1008M, LT1008C PICOAMP INPUT CURRENT, MICROVOLT OFFSET LOW-NOISE OPERATIONAL AMPLIFIERS

## schematic



All resistor values shown are nominal and in ohms.

## absolute maximum ratings over operating free-air temperature range (unless otherwise noted)

Supply voltage, $V_{CC+}$ (see Note 1)	20 V
Supply voltage, $V_{CC-}$	-20 V
Input voltage range, $V_I$	$\pm 20$ V
Differential input current (see Note 2)	$\pm 10$ mA
Duration of output short-circuit at (or below) 25°C (see Note 3)	unlimited
Operating free-air temperature, $T_A$ : LT1008M	-55°C to 125°C
LT1008C	0°C to 70°C
Storage temperature range	-65°C to 150°C
Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds: JG or L package	300°C
Lead temperature 1,6 mm (1/16 inch) from case for 10 seconds: P package	260°C

- NOTES: 1. All voltage values are with respect to the midpoint between  $V_{CC+}$  and  $V_{CC-}$ .  
2. Differential input voltages greater than 1 V will cause excessive current to flow through the input protection diodes unless current-limiting resistors are used.  
3. The output may be shorted to either supply.

## recommended operating conditions

			LT1008M			LT1008C			UNIT
			MIN	NOM	MAX	MIN	NOM	MAX	
Supply voltage, V <sub>CC</sub>			± 20			± 20			V
Common-mode input voltage, V <sub>IC</sub>		V <sub>CC</sub> ± = ± 15 V	± 13.5			- 15 ± 13.5			V
Operating free-air temperature, T <sub>A</sub>			- 55	125		0	70		°C



**LT1008M, LT1008C**  
**PICOAMP INPUT CURRENT, MICROVOLT OFFSET**  
**LOW-NOISE OPERATIONAL AMPLIFIERS**

**electrical characteristics,  $V_{CC} \pm = \pm 15V$ ,  $V_{IC} = 0$  (unless otherwise noted)**

PARAMETER	TEST CONDITIONS	$T_A^\dagger$	LT1008M			LT1008C			UNIT
			MIN	TYP	MAX	MIN	TYP	MAX	
$V_{IO}$ Input offset voltage	$V_{CC} \pm = \pm 15V$ , $V_{IC} = 0$	25°C		30	120		30	120	$\mu V$
		Full range			250			180	
	$V_{CC} \pm = \pm 15V$ , $V_{IC} = \pm 13.5V$	25°C		40	180		40	180	
		Full range			320			250	
	$V_{CC} \pm = \pm 2V$ to $\pm 20V$	25°C		40	180		40	180	
	$V_{CC} \pm = \pm 2.5V$ to $\pm 20V$	Full range			320			250	
$\alpha_{VIO}$ Average temperature coefficient of input offset voltage		Full range		0.2	1.5		0.2	1.5	$\mu V/^\circ C$
Long-term drift of input offset voltage		25°C		0.3			0.3		$\mu V/mo$
$I_{IO}$ Input offset current	$V_{CC} \pm = \pm 15V$ , $V_{IC} = 0$	25°C		30	100		30	100	$pA$
		Full range			250			180	
	$V_{CC} \pm = \pm 15V$ , $V_{IC} = \pm 13.5V$	25°C		40	150		40	150	
		Full range			350			250	
	$V_{CC} \pm = \pm 2V$ to $\pm 20V$	25°C		40	150		40	150	
	$V_{CC} \pm = \pm 2.5V$ to $\pm 20V$	Full range			350			250	
$\alpha_{IIO}$ Average temperature coefficient of input offset current		Full range		0.4	2.5		0.4	2.5	$pA/^\circ C$
$I_{IB}$ Input bias current	$V_{CC} \pm = \pm 15V$ , $V_{IC} = 0$	25°C		$\pm 30$	$\pm 100$		$\pm 30$	$\pm 100$	$pA$
		Full range			$\pm 600$			$\pm 180$	
	$V_{CC} \pm = \pm 15V$ , $V_{IC} = \pm 13.5V$	25°C		$\pm 40$	$\pm 150$		$\pm 40$	$\pm 150$	
		Full range			$\pm 800$			$\pm 250$	
	$V_{CC} \pm = \pm 2V$ to $\pm 20V$	25°C		$\pm 40$	$\pm 150$		$\pm 40$	$\pm 150$	
	$V_{CC} \pm = \pm 2.5V$ to $\pm 20V$	Full range			$\pm 800$			$\pm 250$	
$\alpha_{IIB}$ Average temperature coefficient of input bias current		Full range		0.6	6		0.4	2.5	$pA/^\circ C$
$V_{ICR}$ Common-mode input voltage range		25°C	$\pm 13.5$	$\pm 14$		$\pm 13.5$	$\pm 14$		$V$
		Full range	$\pm 13.5$			$\pm 13.5$			
$V_{OM}$ Maximum peak output voltage swing	$R_L = 10k\Omega$	25°C	$\pm 13$	$\pm 14$		$\pm 13$	$\pm 14$		$V$
		Full range	$\pm 13$			$\pm 13$			
$A_{VD}$ Large-signal differential voltage amplification	$V_O = \pm 12V$ , $R_L \geq 10k\Omega$	25°C	200	2000		200	2000		$V/mV$
		Full range	100			150			
	$V_O = \pm 10V$ , $R_L \geq 2k\Omega$	25°C	120	600		120	600		
CMRR Common-mode rejection ratio	$V_{IC} = \pm 13.5V$	25°C	114	132		114	132		dB
		Full range	108			110			
$k_{SVR}$ Supply-voltage rejection ratio ( $\Delta V_{CC\pm} / \Delta V_{IO}$ )	$V_{CC} \pm = \pm 2V$ to $\pm 20V$	25°C	114	132		114	132		dB
	$V_{CC} \pm = \pm 2.5V$ to $\pm 20V$	Full range	108			110			
$I_{CC}$ Supply current	$V_{CC} \pm = \pm 15V$ , $V_{IC} = \pm 13.5V$	25°C		380	600		380	600	$\mu A$
		Full range							
	$V_{CC} \pm = \pm 2V$ to $\pm 20V$	25°C		380	600		380	600	
	$V_{CC} \pm = \pm 15V$ , $V_{IC} = 0$	Full range			800			800	

$^\dagger$ Full range is  $-55^\circ C$  to  $125^\circ C$  for the LT1008M and  $0^\circ C$  to  $70^\circ C$  for the LT1008C.

2

Operational Amplifiers



# **LT1008M, LT1008C** **PICOAMP INPUT CURRENT, MICROVOLT OFFSET** **LOW-NOISE OPERATIONAL AMPLIFIERS**

**operating characteristics,  $V_{CC} \pm = \pm 15 \text{ V}$ ,  $T_A = 25^\circ\text{C}$  (unless otherwise noted)**

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
SR	Slew rate at unity gain	$C_f = 30 \text{ pF}$ , See Figure 29(a)	0.1	0.2		$\text{V}/\mu\text{s}$
$V_{NPP}$	Peak-to-peak equivalent input noise voltage	$f = 0.1 \text{ Hz to } 10 \text{ Hz}$		0.5		$\mu\text{V}$
$V_n$	Equivalent input noise voltage	$f = 10 \text{ Hz}$		17	30	$\text{nV}/\sqrt{\text{Hz}}$
		$f = 1 \text{ kHz}$		14	22	
$I_n$	Equivalent input noise current	$f = 10 \text{ Hz}$		20		$\text{fA}/\sqrt{\text{Hz}}$

**2**

## **TYPICAL CHARACTERISTICS**

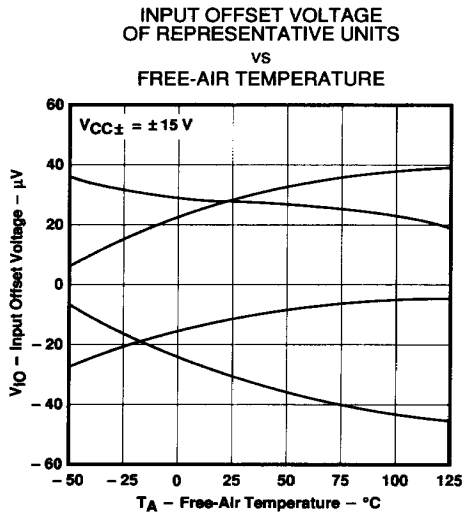
**table of graphs**

			FIGURE
$V_{IO}$	Input offset voltage	vs Temperature	1
		vs Source resistance	5
$\Delta V_{IO}$	Change in input offset voltage	vs Time – minutes	2
		vs Time – months	3
$\alpha_{VIO}$	Temperature coefficient of input offset voltage	vs Source resistance	6
$I_{IB}$	Input bias current	vs Common-mode input voltage	7
		vs Temperature	8
$A_{VD}$	Differential voltage amplification	vs Load resistance	9
		vs Frequency	10, 11, 12
CMRR	Common-mode rejection ratio	vs Frequency	13
$k_{SVR}$	Supply-voltage rejection ratio	vs Frequency	14
$I_{OS}$	Short-circuit output current	vs Time	15
$I_{CC}$	Supply current	vs Supply voltage	4
SR	Slew rate	vs Compensation capacitance	16
$V_{NPP}$	Peak-to-peak equivalent input noise voltage	vs Time	17
$V_n, I_n$	Equivalent input noise voltage and equivalent input noise current	vs Frequency	18
		vs Source resistance	19
	Phase shift	vs Frequency	11, 12
	Pulse response	Small-signal	20, 21, 22
		Large-signal	23, 24

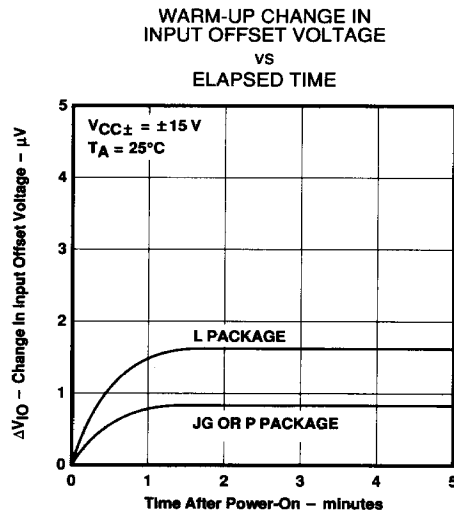


**LT1008M, LT1008C**  
**PICOAMP INPUT CURRENT, MICROVOLT OFFSET**  
**LOW-NOISE OPERATIONAL AMPLIFIERS**

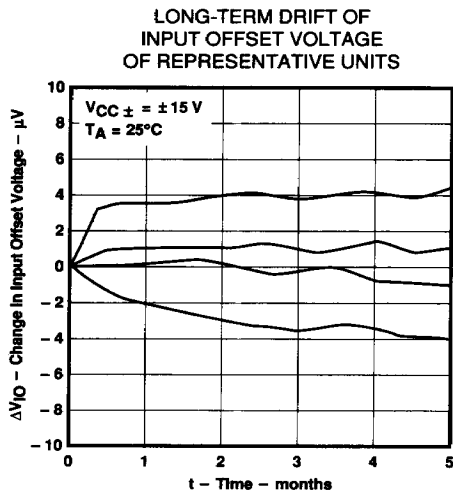
**TYPICAL CHARACTERISTICS†**



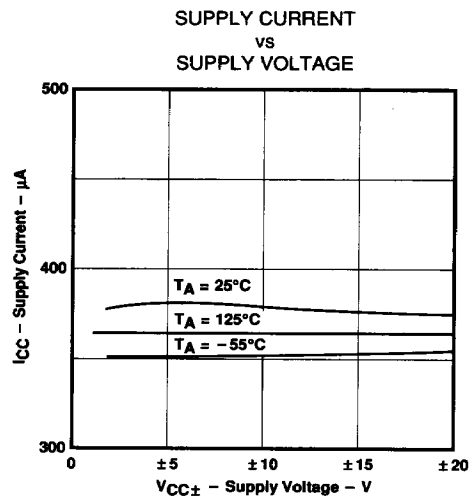
**FIGURE 1**



**FIGURE 2**



**FIGURE 3**



**FIGURE 4**

†Data for temperatures below  $0^{\circ}\text{C}$  and above  $70^{\circ}\text{C}$  are applicable to the LT1008M only.



**LT1008M, LT1008C**  
**PICOAMP INPUT CURRENT, MICROVOLT OFFSET**  
**LOW-NOISE OPERATIONAL AMPLIFIERS**

**TYPICAL CHARACTERISTICS†**

2

Operational Amplifiers

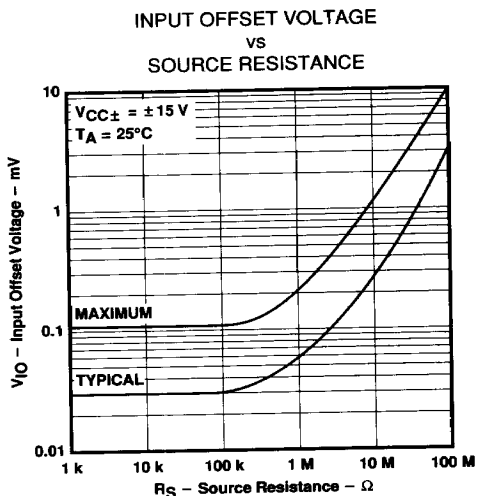


FIGURE 5

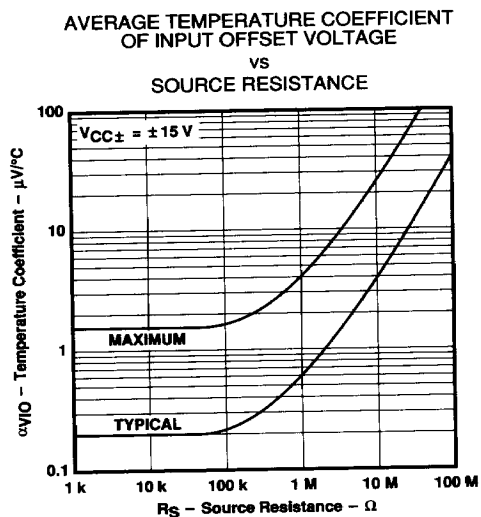


FIGURE 6

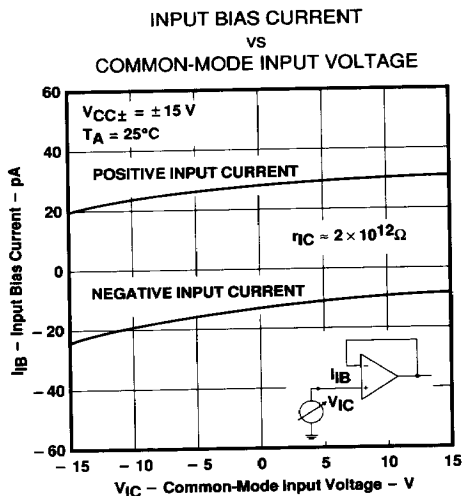


FIGURE 7

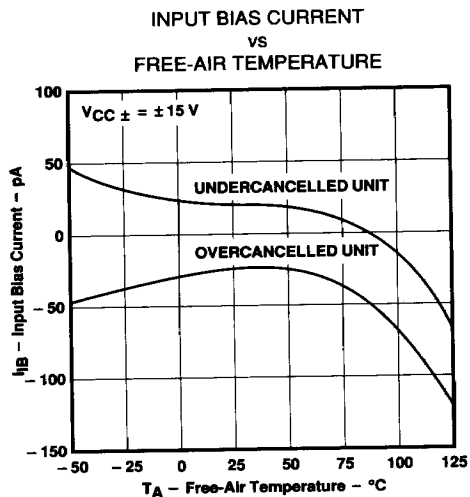


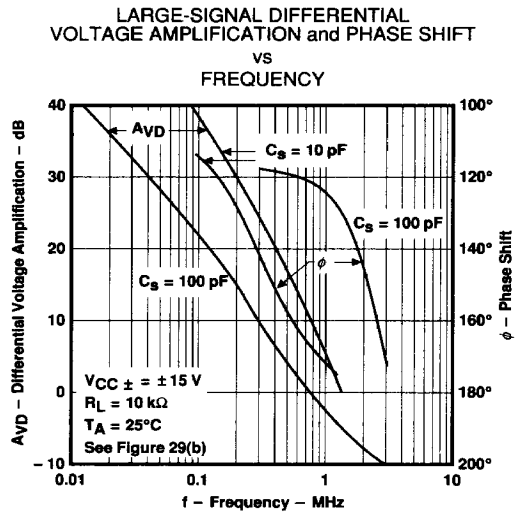
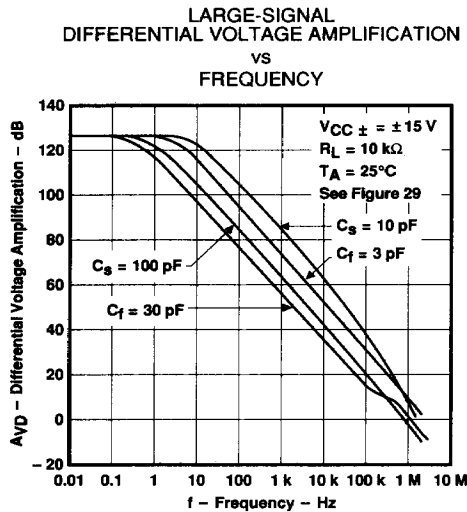
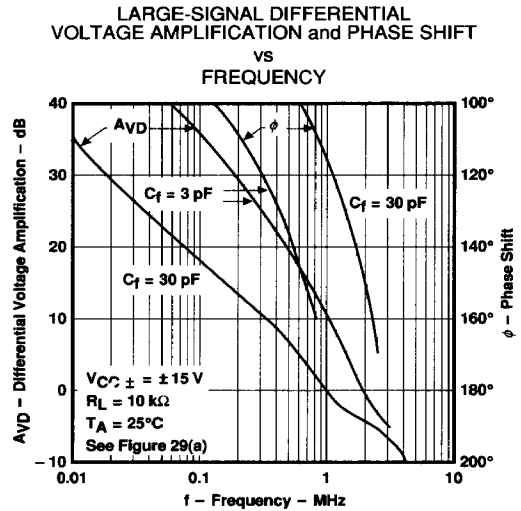
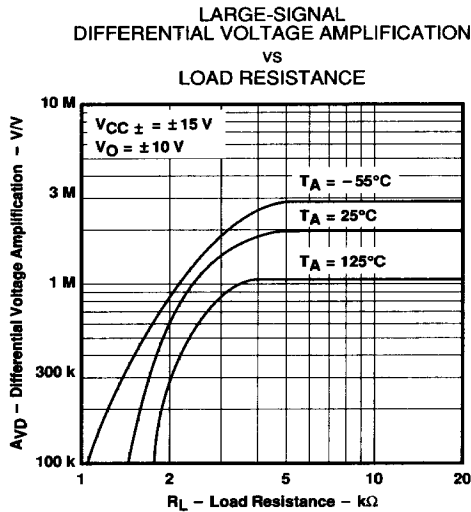
FIGURE 8

†Data for temperatures below  $0^\circ\text{C}$  and above  $70^\circ\text{C}$  are applicable to the LT1008M only.



**LT1008M, LT1008C**  
**PICOAMP INPUT CURRENT, MICROVOLT OFFSET**  
**LOW-NOISE OPERATIONAL AMPLIFIERS**

**TYPICAL CHARACTERISTICS†**



†Data for temperatures below 0°C and above 70°C are applicable to the LT1008M only.



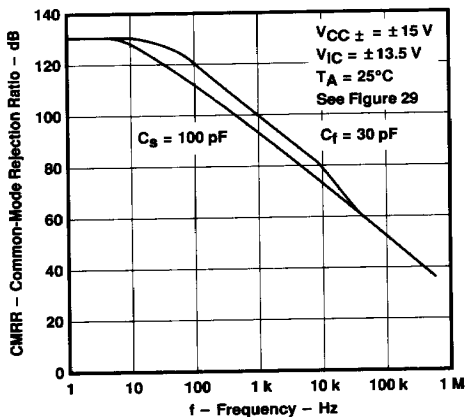
**LT1008M, LT1008C**  
**PICOAMP INPUT CURRENT, MICROVOLT OFFSET**  
**LOW-NOISE OPERATIONAL AMPLIFIERS**

**TYPICAL CHARACTERISTICS†**

2

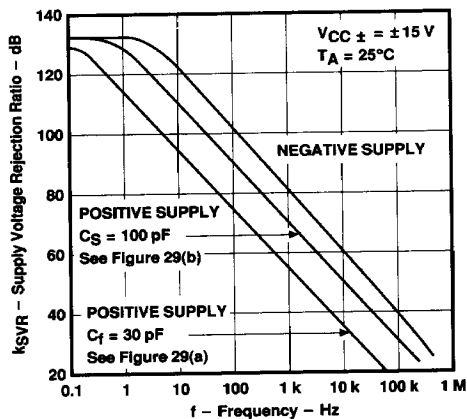
Operational Amplifiers

**COMMON-MODE REJECTION RATIO  
 VS  
 FREQUENCY**



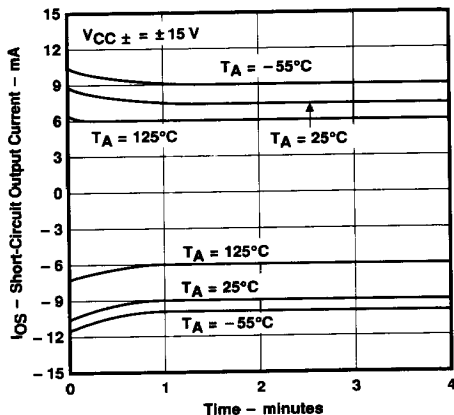
**FIGURE 13**

**SUPPLY-VOLTAGE REJECTION RATIO  
 VS  
 FREQUENCY**



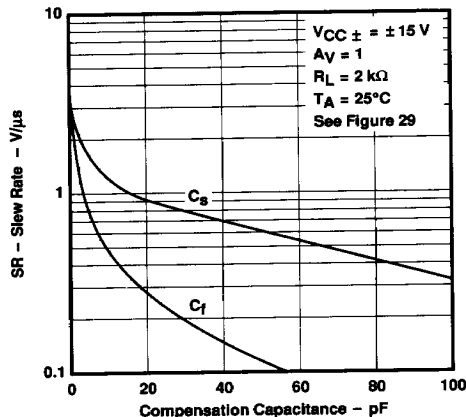
**FIGURE 14**

**SHORT-CIRCUIT OUTPUT CURRENT  
 VS  
 ELAPSED TIME**



**FIGURE 15**

**SLEW RATE  
 VS  
 COMPENSATION CAPACITANCE**



**FIGURE 16**

†Data for temperatures below 0°C and above 70°C are applicable to the LT1008M only.



TYPICAL CHARACTERISTICS

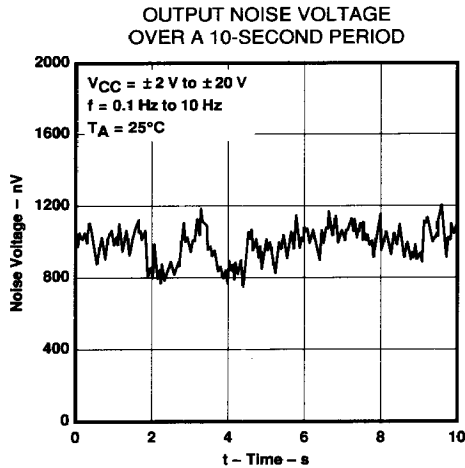


FIGURE 17

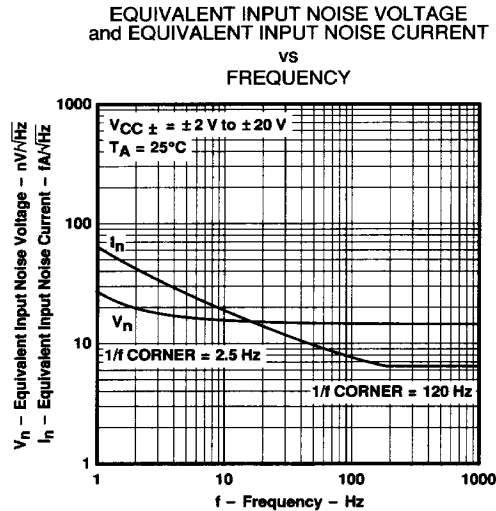


FIGURE 18

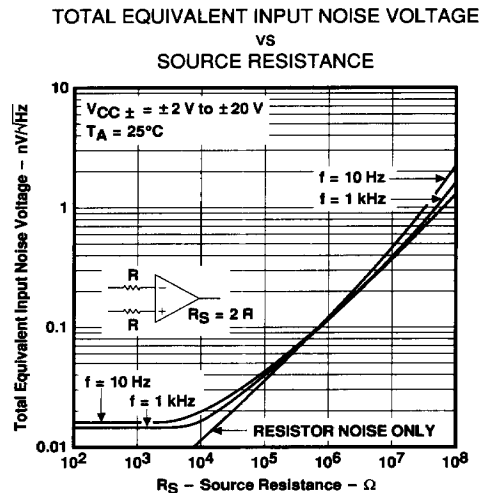


FIGURE 19

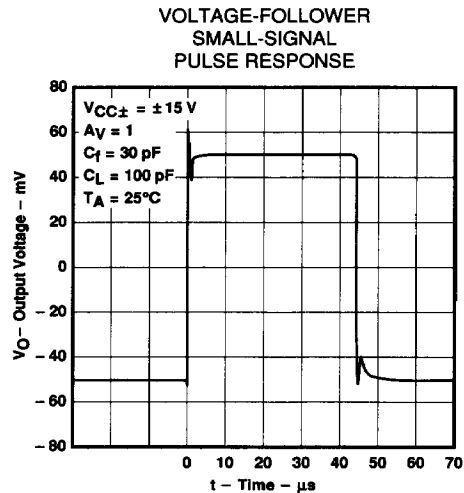


FIGURE 20



TYPICAL CHARACTERISTICS

2

Operational Amplifiers

VOLTAGE-FOLLOWER  
SMALL-SIGNAL  
PULSE RESPONSE

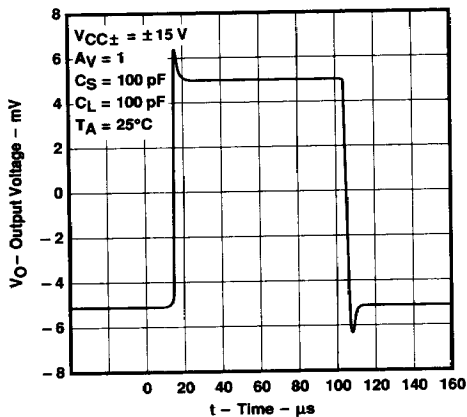


FIGURE 21

VOLTAGE-FOLLOWER  
SMALL-SIGNAL  
PULSE RESPONSE

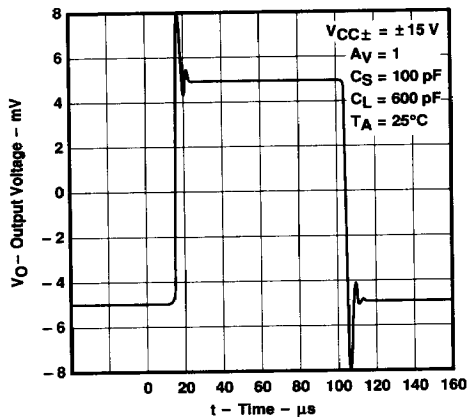


FIGURE 22

VOLTAGE-FOLLOWER  
LARGE-SIGNAL  
PULSE RESPONSE

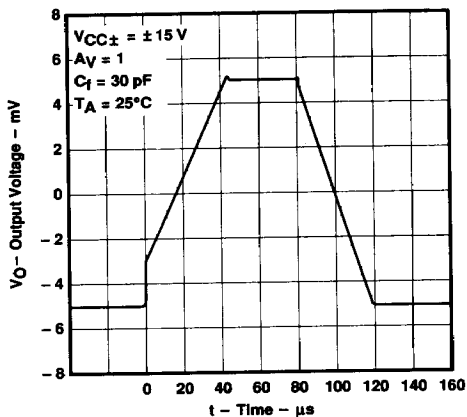


FIGURE 23

VOLTAGE-FOLLOWER  
LARGE-SIGNAL  
PULSE RESPONSE

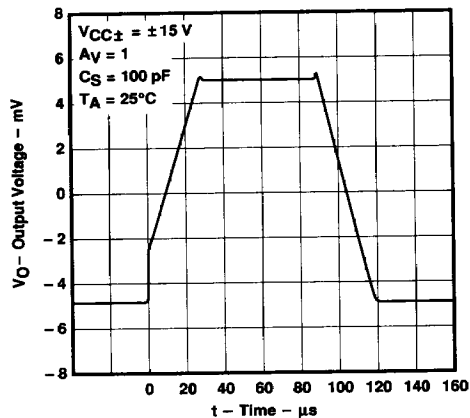


FIGURE 24



## TYPICAL APPLICATION DATA

### achieving picoampere, microvolt performance

Proper care should be exercised to realize the picoampere, microvolt accuracy of the LT1008. Because leakage currents in external circuitry can significantly degrade performance, high-quality insulation should be used (e. g., Teflon, Kel-F). All insulating surfaces should be cleaned to remove fluxes and other residues. Surface coating may be necessary to provide a moisture barrier in high-humidity environments.

Board leakage can be minimized by encircling the input circuitry with a guard ring operated at a potential close to that of the inputs (see Figure 25). In inverting configurations, the guard ring should be tied to ground; in noninverting configurations, the guard ring should be tied to the inverting input (pin 2). Both sides of the printed circuit board should be guarded. Bulk leakage reduction depends on the guard ring width. Nanoampere-level leakage into the compensation terminals can affect input offset voltage and its temperature coefficient (see Figure 26).

Microvolt-level error voltages can also be generated in the external circuitry. Thermocouple effects, caused by temperature gradients across dissimilar metals at the contacts to the input terminals, can exceed the inherent temperature coefficient of the amplifier. Air currents over device leads should be minimized, package leads should be short, and the two input leads should be as close together as possible and maintained at the same temperature. The LT1008 is specified over a wide range of supply voltages from  $\pm 2$  V to  $\pm 18$  V. Operation with lower supplies (down to  $\pm 1$  V) is possible with two Ni-Cad batteries.

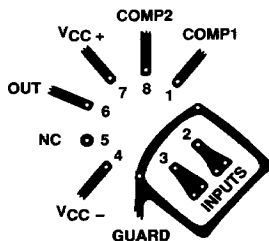
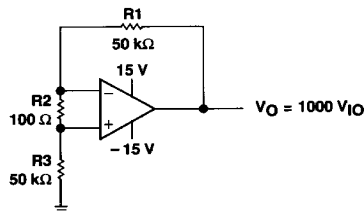


FIGURE 25. GUARD RING



- NOTES: A. Resistors must have low thermoelectric potential.  
 B. This circuit is also used as the burn-in configuration for the LT1008, with supply voltages increased to  $\pm 20$  V,  $R1 = R3 = 20$  k $\Omega$ ,  $R2 = 200$   $\Omega$ , and  $A_V = 100$ .

FIGURE 26. TEST CIRCUIT FOR  $V_{IO}$  AND  $\alpha V_{IO}$

### noise testing

The peak-to-peak equivalent input noise voltage of the LT1008 is measured in the test circuit shown in Figure 27. The frequency response of this noise tester indicates that the 0.1-Hz to 10-Hz noise should not exceed 10 seconds, as this time limit acts as an additional zero to eliminate noise contributions from the frequency band below 0.1 Hz.

An input noise voltage test is recommended when measuring noise in a large number of units. A 10-Hz input noise voltage measurement correlates well with a 0.1-Hz peak-to-peak noise reading because both results are determined by the white noise and the location of the  $1/f$  corner frequency.

Current noise is measured by the current shown in Figure 28 and calculated by the following formula in which the noise of the source resistors is subtracted:

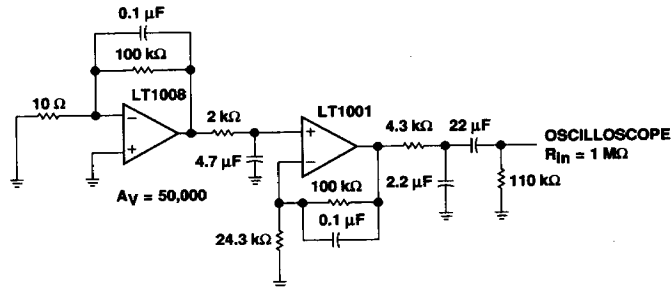
$$I_n = \frac{[V_{no}^2 - (820 \text{ nV})^2]^{1/2}}{40 \text{ M}\Omega \times 100}$$



**LT1008M, LT1008C**  
**PICOAMP INPUT CURRENT, MICROVOLT OFFSET**  
**LOW-NOISE OPERATIONAL AMPLIFIERS**

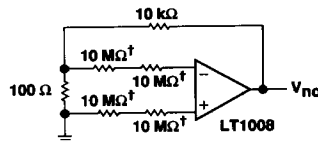
**TYPICAL APPLICATION DATA**

noise testing (continued)



NOTE A: All capacitor values are for nonpolarized capacitors only.

**FIGURE 27. 0.1-Hz TO 10-Hz PEAK-TO-PEAK NOISE VOLTAGE TEST CIRCUIT**

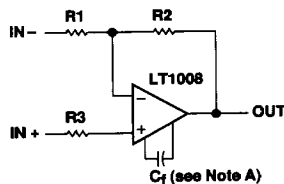


† Metal film.

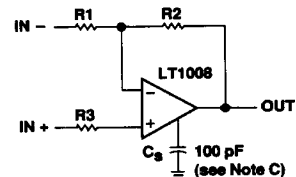
**FIGURE 28. NOISE CURRENT TEST CIRCUIT**

**frequency compensation**

The LT1008 is externally frequency compensated with a single capacitor. The two compensation circuits shown in Figure 29 are identical to the frequency compensation circuits for the LM108A series. Therefore, the LT1008 operational amplifiers can be inserted directly into LM108A or LM308A sockets, with similar ac and upgraded dc performance.



**(a) STANDARD COMPENSATION**



**(b) ALTERNATE COMPENSATION (see Note B)**

- NOTES: A.  $C_f \geq (R_1 \times C_0) / (R_1 + R_2)$ ,  $C_0 = 30$  pF. Bandwidth and slew rate are proportional to  $1/C_f$ .  
 B. This circuit improves the supply voltage rejection ratio by a factor of 5.  
 C. Bandwidth and slew rate are proportional to  $1/C_0$ .  
 D. For  $(R_2/R_1) > 200$ , no external frequency compensation is necessary.

**FIGURE 29. FREQUENCY COMPENSATION CIRCUITS (see Note D)**

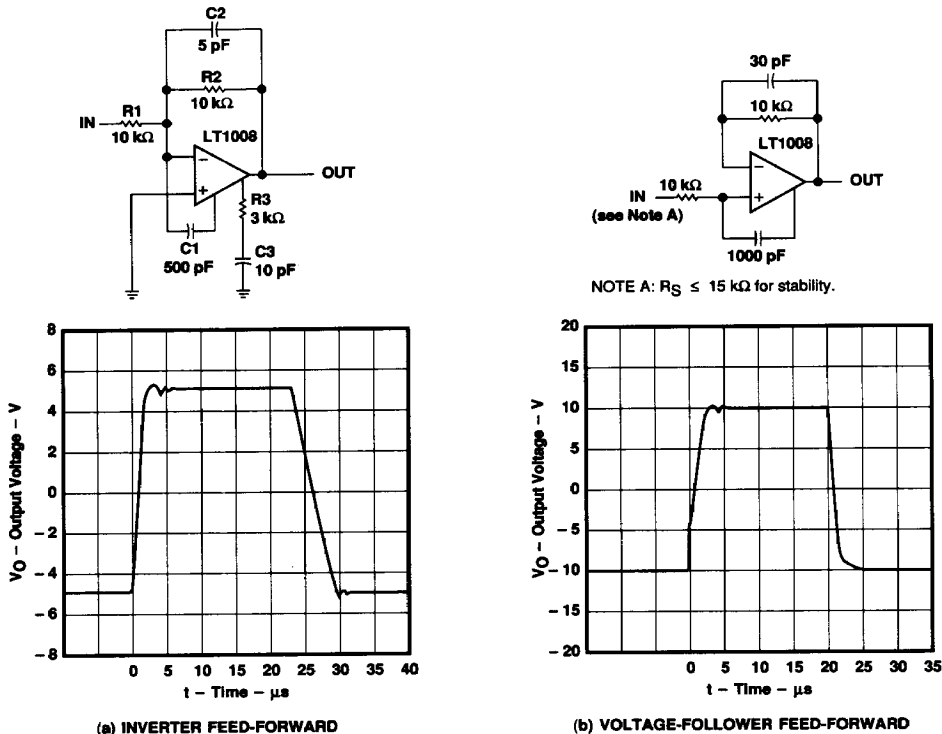


## TYPICAL APPLICATION DATA

### frequency compensation (continued)

External frequency compensation provides additional flexibility in shaping the frequency response of the amplifier. For example, for a voltage gain of 10 and  $C_f = 3 \text{ pF}$ , a gain-bandwidth product of 5 MHz and slew rate of  $1.2 \text{ V}/\mu\text{s}$  can be realized. For closed-loop gains greater than 200, no external compensation is necessary, and the slew rate increases to  $4 \text{ V}/\mu\text{s}$ . The LT1008 can also be overcompensated (e.g.,  $C_f > 30 \text{ pF}$  or  $C_S > 100 \text{ pF}$ ) to improve capacitive-load-handling capability or to narrow noise bandwidth. In applications in which the feedback loop around the amplifier has gain, overcompensation can stabilize the circuit with a single capacitor.

The availability of the compensation terminals permits the use of feed-forward frequency compensation to enhance slew rate in low closed-loop-gain configurations (see Figure 30). The inverter slew rate is increased to  $1.4 \text{ V}/\mu\text{s}$ . The voltage-follower feed-forward scheme bypasses the amplifier's gain stages and slews at nearly  $10 \text{ V}/\mu\text{s}$ .



**FIGURE 30. FREQUENCY COMPENSATION CIRCUITS  
and VOLTAGE-FOLLOWER PULSE RESPONSES**



# LT1008M, LT1008C PICOAMP INPUT CURRENT, MICROVOLT OFFSET LOW-NOISE OPERATIONAL AMPLIFIERS

## TYPICAL APPLICATION DATA

### other considerations

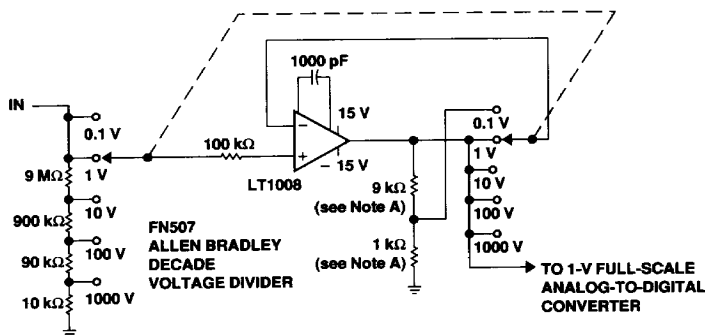
The inputs of the LT1008 are protected by back-to-back diodes. Current-limiting resistors are not used because the leakage of these resistors would prevent the realization of picoampere-level bias currents at elevated temperatures. In the voltage-follower configuration, when the input is driven by a fast, large-signal pulse ( $> 1\text{ V}$ ), the input protection diodes effectively short the output to the input during slewing, and a current, limited only by the output short-circuit protection, flows through the diodes.

The use of a feedback resistor, as shown in the voltage-follower feed-forward diagram, is recommended because this resistor keeps the current below the short-circuit limit, resulting in faster recovery and settling of the output.

2

Operational Amplifiers

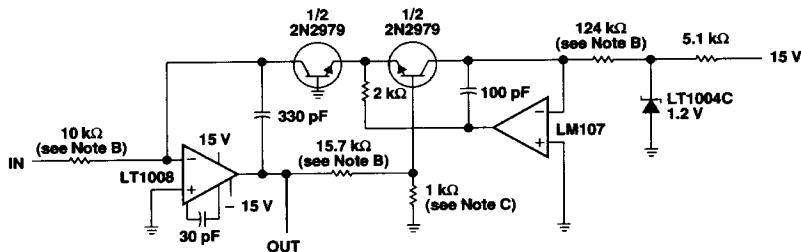
### typical applications



NOTES: A. Ratio match  $\pm 0.01\%$ .

B. This application requires low bias current, low offset voltage and offset voltage temperature coefficient, low noise, and low long-term offset voltage drift.

FIGURE 31. INPUT AMPLIFIER FOR 4 1/2-DIGIT VOLTMETER



NOTES: A. The low bias current and offset voltage of the LT1008 allow 4 1/2 decades of voltage input logging.

B. 1% film resistor.

C. Tel. Labs, Type Q81.

FIGURE 32. LOGARITHMIC AMPLIFIER







## Operational Amplifiers

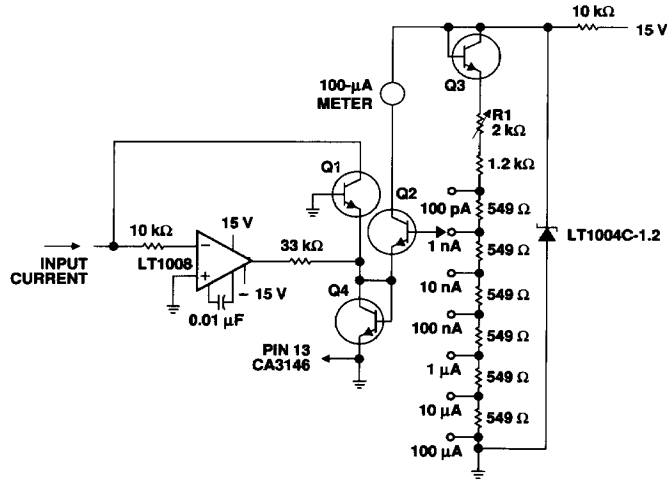
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TYPICAL APPLICATION DATA



- NOTES: A. This ammeter measures currents from 100 pA to 100  $\mu$ A without the use of expensive high-value resistors. Accuracy at 100  $\mu$ A is limited by the offset voltage between Q1 and Q2 and, at 100 pA, by the inverting bias current of the LT1008.  
B. Q1-Q4 RCA CA3146 transistor array.  
C. Adjust R1 for full-scale deflection with 1- $\mu$ A input current.

FIGURE 39. AMMETER WITH 6-DECADE RANGE



## 2 Operational Amplifiers

The circuit diagram shows a 100 Hz sine wave generator. It consists of three op-amp ICs: an LT1008 and two LT311A comparators. The LT1008 is configured as a voltage follower with a 10 kΩ feedback resistor. Its non-inverting input is connected to a 1.5 MΩ resistor and a 1 μF capacitor to ground. The inverting input is connected to a 2 kΩ resistor from the input (IN) and a 1 kΩ resistor to a 15 V supply. The output of the LT1008 is connected to the non-inverting input of the first LT311A comparator. The first LT311A comparator has its inverting input connected to a 15 V supply and its non-inverting input connected to the output of the LT1008. The output of the first LT311A is connected to the inverting input of the second LT311A comparator. The second LT311A comparator has its non-inverting input connected to a 15 V supply and its inverting input connected to a 100 kΩ resistor to ground and a 10 kΩ resistor to the output of the first LT311A. The output of the second LT311A is connected to the output of the LT1008, forming a feedback loop. The output of the circuit is labeled 'OUT'.

B. OPTO-MOS switch, Type OFM1A, Theta-J Corp.

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