

## FEATURES

- Guaranteed 4.5nV/ $\sqrt{\text{Hz}}$  10Hz Noise
- Guaranteed 3.8nV/ $\sqrt{\text{Hz}}$  1kHz Noise
- 0.1Hz to 10Hz Noise, 60nV<sub>P-P</sub> Typical
- Guaranteed 7 Million Min Voltage Gain,  $R_L = 2\text{k}$
- Guaranteed 3 Million Min Voltage Gain,  $R_L = 600\Omega$
- Guaranteed 25 $\mu\text{V}$  Max Offset Voltage
- Guaranteed 0.6 $\mu\text{V}/^{\circ}\text{C}$  Max Drift with Temperature
- Guaranteed 11V/ $\mu\text{s}$  Min Slew Rate (LT1037)
- Guaranteed 117dB Min CMRR

## APPLICATIONS

- Low Noise Signal Processing
- Microvolt Accuracy Threshold Detection
- Strain Gauge Amplifiers
- Direct Coupled Audio Gain Stages
- Sine Wave Generators
- Tape Head Preamplifiers
- Microphone Preamplifiers

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## DESCRIPTION

The LT®1007/LT1037 series features the lowest noise performance available to date for monolithic operational amplifiers: 2.5nV/ $\sqrt{\text{Hz}}$  wideband noise (less than the noise of a 400 $\Omega$  resistor), 1/f corner frequency of 2Hz and 60nV peak-to-peak 0.1Hz to 10Hz noise. Low noise is combined with outstanding precision and speed specifications: 10 $\mu\text{V}$  offset voltage, 0.2 $\mu\text{V}/^{\circ}\text{C}$  drift, 130dB common mode and power supply rejection, and 60MHz gain bandwidth product on the decompensated LT1037, which is stable for closed-loop gains of 5 or greater.

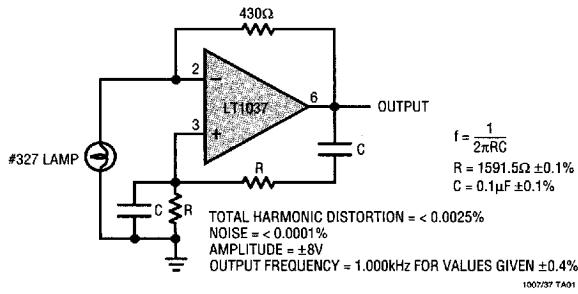
The voltage gain of the LT1007/LT1037 is an extremely high 20 million driving a 2k $\Omega$  load and 12 million driving a 600 $\Omega$  load to  $\pm 10\text{V}$ .

In the design, processing and testing of the device, particular attention has been paid to the optimization of the entire distribution of several key parameters. Consequently, the specifications of even the lowest cost grades (the LT1007C and the LT1037C) have been spectacularly improved compared to equivalent grades of competing amplifiers.

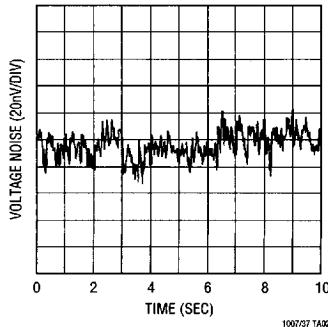
The sine wave generator application shown below utilizes the low noise and low distortion characteristics of the LT1037.

## TYPICAL APPLICATION

Ultrapure 1kHz Sine Wave Generator



0.1Hz to 10Hz Noise

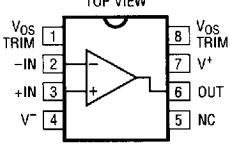
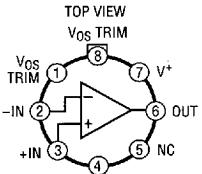
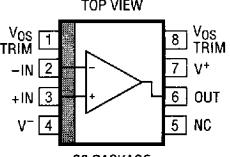


**ABSOLUTE MAXIMUM RATINGS**

Supply Voltage .....  $\pm 22\text{V}$   
 Input Voltage ..... Equal to Supply Voltage  
 Output Short-Circuit Duration ..... Indefinite  
 Differential Input Current (Note 8) .....  $\pm 25\text{mA}$   
 Storage Temperature Range .....  $-65^\circ\text{C}$  to  $150^\circ\text{C}$

Lead Temperature (Soldering, 10 sec.) .....  $300^\circ\text{C}$   
 Operating Temperature Range  
 LT1007/LT1037AC, C .....  $0^\circ\text{C}$  to  $70^\circ\text{C}$   
 LT1007/LT1037I .....  $-40^\circ\text{C}$  to  $85^\circ\text{C}$   
 LT1007/LT1037AM, M .....  $-55^\circ\text{C}$  to  $125^\circ\text{C}$

**PACKAGE/ORDER INFORMATION**

TOP VIEW	TOP VIEW	TOP VIEW			
					
J8 PACKAGE 8-LEAD CERDIP	N8 PACKAGE 8-LEAD PDIP	S8 PACKAGE 8-LEAD PLASTIC SO			
$T_{JMAX} = 150^\circ\text{C}, \theta_{JA} = 100^\circ\text{C/W}$ (J8)	$T_{JMAX} = 150^\circ\text{C}, \theta_{JA} = 130^\circ\text{C/W}$ (N8)	$T_{JMAX} = 150^\circ\text{C}, \theta_{JA} = 190^\circ\text{C/W}$			
ORDER PART NUMBER	ORDER PART NUMBER	ORDER PART NUMBER			
LT1007ACJ8	LT1037ACJ8	LT1007ACH	LT1037ACH	LT1007CS8	LT1037CS8
LT1007ACN8	LT1037ACN8	LT1007AMH	LT1037AMH	LT1007IS8	LT1037IS8
LT1007AMJ8	LT1037AMJ8	LT1007CH	LT1037CH		
LT1007CJ8	LT1037CJ8	LT1007MH	LT1037MH		
LT1007CN8	LT1037CN8				
LT1007IN8	LT1037IN8			1007	1037
LT1007MJ8	LT1037MJ8			1007I	1037I

**ELECTRICAL CHARACTERISTICS**  $V_S = \pm 15\text{V}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	LT1007AC/AM			LT1007C/I/M			UNITS
			MIN	TYP	MAX	MIN	TYP	MAX	
$V_{OS}$	Input Offset Voltage	(Note 1)		10	25		20	60	$\mu\text{V}$
$\frac{\Delta V_{OS}}{\Delta \text{Time}}$	Long Term Input Offset Voltage Stability	(Notes 2, 3)		0.2	1.0		0.2	1.0	$\mu\text{V}/\text{Mo}$
$I_{OS}$	Input Offset Current			7	30		12	50	$\text{nA}$
$I_B$	Input Bias Current			$\pm 10$	$\pm 35$		$\pm 15$	$\pm 55$	$\text{nA}$
$e_n$	Input Noise Voltage	0.1Hz to 10Hz (Notes 3, 5)		0.06	0.13		0.06	0.13	$\mu\text{V}_{\text{P-P}}$
	Input Noise Voltage Density	$f_0 = 10\text{Hz}$ (Notes 3, 4) $f_0 = 1000\text{Hz}$ (Note 3)		2.8	4.5		2.8	4.5	$\text{nV}/\sqrt{\text{Hz}}$
				2.5	3.8		2.5	3.8	$\text{nV}/\sqrt{\text{Hz}}$
$i_n$	Input Noise Current Density	$f_0 = 10\text{Hz}$ (Notes 3, 6) $f_0 = 1000\text{Hz}$ (Notes 3, 6)		1.5	4.0		1.5	4.0	$\text{pA}/\sqrt{\text{Hz}}$
				0.4	0.6		0.4	0.6	$\text{pA}/\sqrt{\text{Hz}}$

**ELECTRICAL CHARACTERISTICS**  $V_S = \pm 15V$ ,  $T_A = 25^\circ C$ , unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	LT1007AC/AM LT1037AC/AM			LT1007C/M LT1037C/I/M			UNITS	
			MIN	TYP	MAX	MIN	TYP	MAX		
	Input Resistance, Common Mode		7			5			$\text{G}\Omega$	
	Input Voltage Range		$\pm 11.0$	$\pm 12.5$		$\pm 11.0$	$\pm 12.5$		V	
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 11V$	117	130		110	126		dB	
PSRR	Power Supply Rejection Ratio	$V_S = \pm 4V$ to $\pm 18V$	110	130		106	126		dB	
$A_{VOL}$	Large-Signal Voltage Gain	$R_L \geq 2k$ , $V_0 = \pm 12V$ $R_L \geq 1k$ , $V_0 = \pm 10V$ $R_L \geq 600\Omega$ , $V_0 = \pm 10V$	7.0 5.0 3.0	20.0 16.0 12.0		5.0 3.5 2.0	20.0 16.0 12.0		$\text{V}/\mu\text{V}$ $\text{V}/\mu\text{V}$ $\text{V}/\mu\text{V}$	
$V_{OUT}$	Maximum Output Voltage Swing	$R_L \geq 2k$ $R_L \geq 600\Omega$	$\pm 13.0$ $\pm 11.0$	$\pm 13.8$ $\pm 12.5$		$\pm 12.5$ $\pm 10.5$	$\pm 13.5$ $\pm 12.5$		V V	
SR	Slew Rate	LT1007 LT1037	$R_L \geq 2k$ $A_{VCL} \geq 5$	1.7 11	2.5 15	1.7 11	2.5 15		$\text{V}/\mu\text{s}$ $\text{V}/\mu\text{s}$	
GBW	Gain Bandwidth Product	LT1007 LT1037	$f_0 = 100\text{kHz}$ (Note 7) $f_0 = 10\text{kHz}$ (Note 7) ( $A_{VCL} \geq 5$ )	5.0 45	8.0 60	5.0 45	8.0 60		MHz MHz	
$Z_0$	Open-Loop Output Resistance		$V_0 = 0V$ , $I_0 = 0$		70		70		$\Omega$	
$P_D$	Power Dissipation	LT1007 LT1037			80 80	120 130		80 85	140 140	mW mW

 $V_S = \pm 15V$ ,  $0^\circ C \leq T_A \leq 70^\circ C$ , unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	LT1007AC LT1037AC			LT1007C LT1037C			UNITS	
			MIN	TYP	MAX	MIN	TYP	MAX		
$V_{OS}$	Input Offset Voltage	(Note 1)	●	20	50	35	110		$\mu\text{V}$	
$\frac{\Delta V_{OS}}{\Delta T_{Temp}}$	Average Input Offset Drift	(Note 9)	●	0.2	0.6	0.3	1.0		$\mu\text{V}/^\circ\text{C}$	
$I_{OS}$	Input Offset Current		●	10	40	15	70		nA	
$I_B$	Input Bias Current		●	$\pm 14$	$\pm 45$	$\pm 20$	$\pm 75$		nA	
	Input Voltage Range		●	$\pm 10.5$	$\pm 11.8$	$\pm 10.5$	$\pm 11.8$		V	
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 10.5V$	●	114	126	106	120		dB	
PSRR	Power Supply Rejection Ratio	$V_S = \pm 4.5V$ to $\pm 18V$	●	106	126	102	120		dB	
$A_{VOL}$	Large-Signal Voltage Gain	$R_L \geq 2k$ , $V_0 = \pm 10V$ $R_L \geq 1k$ , $V_0 = \pm 10V$	● ●	4.0 2.5	18.0 14.0	2.5 2.0	18.0 14.0		$\text{V}/\mu\text{V}$ $\text{V}/\mu\text{V}$	
$V_{OUT}$	Maximum Output Voltage Swing	$R_L \geq 2k$	●	$\pm 12.5$	$\pm 13.6$	$\pm 12.0$	$\pm 13.6$		V	
$P_D$	Power Dissipation		●		90	144		90	160	mW

# LT1007/LT1037

## ELECTRICAL CHARACTERISTICS $V_S = \pm 15V, -40^\circ C \leq T_A \leq 85^\circ C$ , unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	LT1007/LT1037I			UNITS
			MIN	TYP	MAX	
$V_{OS}$	Input Offset Voltage	(Note 1)	●	40	125	$\mu V$
$\Delta V_{OS}$ $\Delta T_{Temp}$	Average Input Offset Drift	(Note 9)	●	0.3	1.0	$\mu V/^\circ C$
$I_{OS}$	Input Offset Current		●	20	80	nA
$I_B$	Input Bias Current		●	$\pm 25$	$\pm 90$	nA
	Input Voltage Range		●	$\pm 10$	$\pm 11.7$	V
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 10.5V$	●	105	120	dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 4.5V$ to $\pm 18V$	●	101	120	dB
$A_{VOL}$	Large-Signal Voltage Gain	$R_L \geq 2k, V_0 = \pm 10V$	●	2.0	15.0	$V/\mu V$
		$R_L \geq 1k, V_0 = \pm 10V$	●	1.5	12.0	$V/\mu V$
$V_{OUT}$	Maximum Output Voltage Swing	$R_L \geq 2k$	●	$\pm 12.0$	$\pm 13.6$	V
$P_D$	Power Dissipation		●	95	165	mW

$V_S = \pm 15V, -55^\circ C \leq T_A \leq 125^\circ C$ , unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	LT1007AM/LT1037AM			LT1007M/LT1037M	UNITS
			MIN	TYP	MAX		
$V_{OS}$	Input Offset Voltage	(Note 1)	●	25	60	50	$\mu V$
$\Delta V_{OS}$ $\Delta T_{Temp}$	Average Input Offset Drift	(Note 9)	●	0.2	0.6	0.3	$\mu V/^\circ C$
$I_{OS}$	Input Offset Current		●	15	50	20	nA
$I_B$	Input Bias Current		●	$\pm 20$	$\pm 60$	$\pm 35$	nA
	Input Voltage Range		●	$\pm 10.3$	$\pm 11.5$	$\pm 10.3$	V
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 10.3V$	●	112	126	104	dB
PSRR	Power Supply Rejection Ratio	$V_S = \pm 4.5V$ to $\pm 18V$	●	104	126	100	dB
$A_{VOL}$	Large-Signal Voltage Gain	$R_L \geq 2k, V_0 = \pm 10V$	●	3.0	14.0	2.0	$V/\mu V$
		$R_L \geq 1k, V_0 = \pm 10V$	●	2.0	10.0	1.5	$V/\mu V$
$V_{OUT}$	Maximum Output Voltage Swing	$R_L \geq 2k$	●	$\pm 12.5$	$\pm 13.5$	$\pm 12.0$	V
$P_D$	Power Dissipation		●	100	150	100	mW

The ● denotes the specifications which apply over the full operating temperature range.

For MIL-STD components, please refer to LTC 883C data sheet for test listing and parameters.

**Note 1:** Input Offset Voltage measurements are performed by automatic test equipment approximately 0.5 seconds after application of power. AM and AC grades are guaranteed fully warmed up.

**Note 2:** Long Term Input Offset Voltage Stability refers to the average trend line of Offset Voltage vs Time over extended periods after the first 30 days of operation. Excluding the initial hour of operation, changes in  $V_{OS}$  during the first 30 days are typically  $2.5\mu V$ . Refer to typical performance curve.

**Note 3:** This parameter is tested on a sample basis only.

**Note 4:** 10Hz noise voltage density is sample tested on every lot. Devices 100% tested at 10Hz are available on request.

**Note 5:** See the test circuit and frequency response curve for 0.1Hz to 10Hz tester in the Applications Information section.

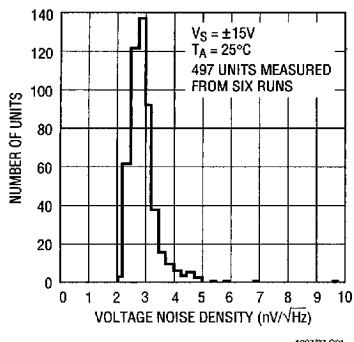
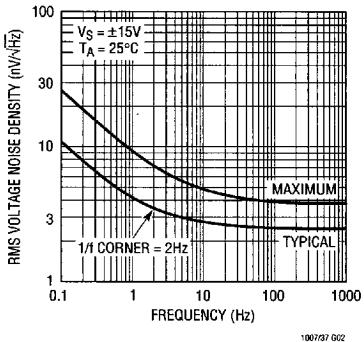
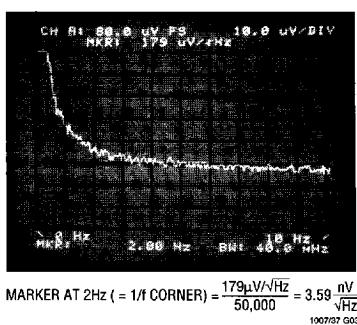
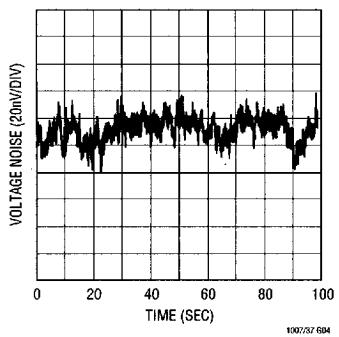
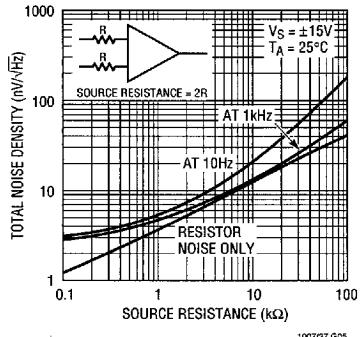
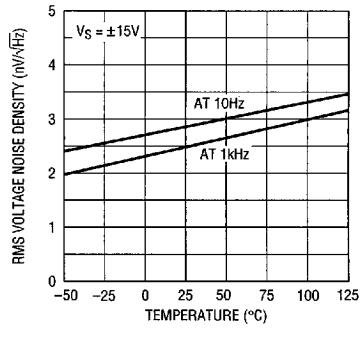
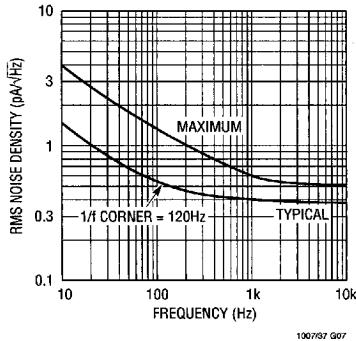
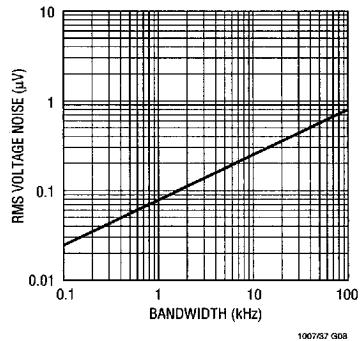
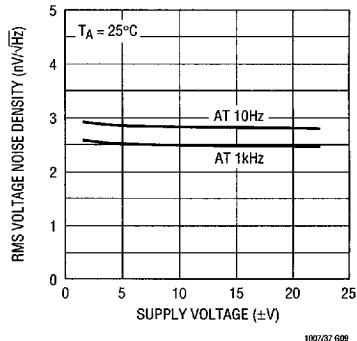
**Note 6:** See the test circuit for current noise measurement in the Applications Information section.

**Note 7:** This parameter is guaranteed by design and is not tested.

**Note 8:** The inputs are protected by back-to-back diodes. Current limiting resistors are not used in order to achieve low noise. If differential input voltage exceeds  $\pm 0.7V$ , the input current should be limited to  $25mA$ .

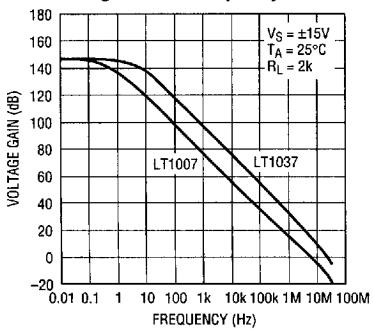
**Note 9:** The Average Input Offset Drift performance is within the specifications unnullled or when nulled with a pot having a range of  $8k\Omega$  to  $20k\Omega$ .

## TYPICAL PERFORMANCE CHARACTERISTICS

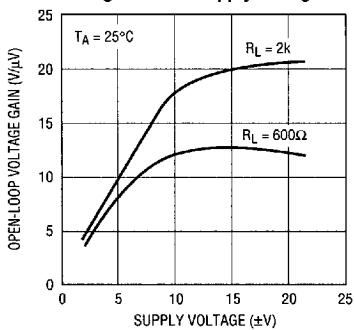
**10Hz Voltage Noise Distribution**

**Voltage Noise vs Frequency**

**0.02Hz to 10Hz RMS Noise. Gain = 50,000  
(Measured on HP3582 Spectrum Analyzer)**

**0.01Hz to 1Hz Peak-to-Peak Noise**

**Total Noise vs Source Resistance**

**Voltage Noise vs Temperature**

**Current Noise vs Frequency**

**Wideband Voltage Noise  
(0.1Hz to Frequency Indicated)**

**Voltage Noise vs Supply Voltage**


## TYPICAL PERFORMANCE CHARACTERISTICS

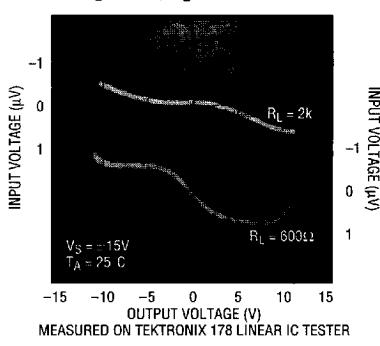
**Voltage Gain vs Frequency**



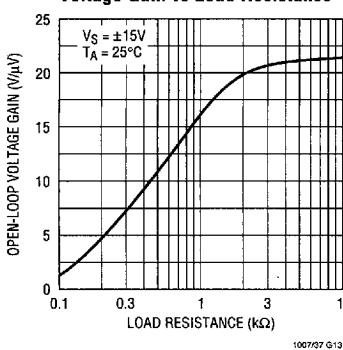
**Voltage Gain vs Supply Voltage**



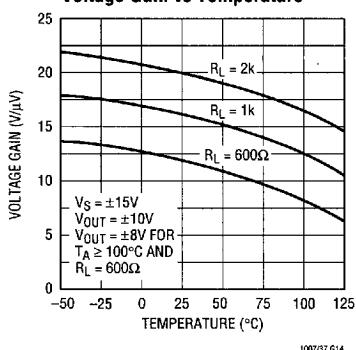
**Voltage Gain,  $R_L = 2k$  and  $600\Omega$**



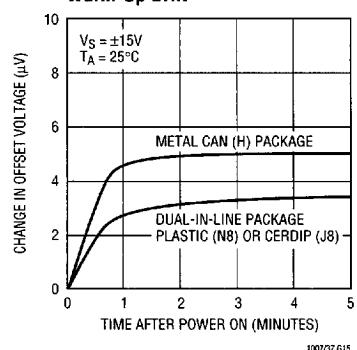
**Voltage Gain vs Load Resistance**



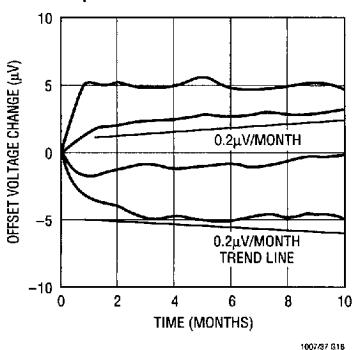
**Voltage Gain vs Temperature**



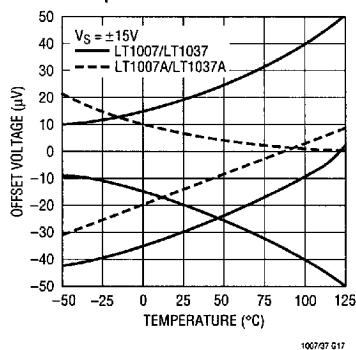
**Warm-Up Drift**



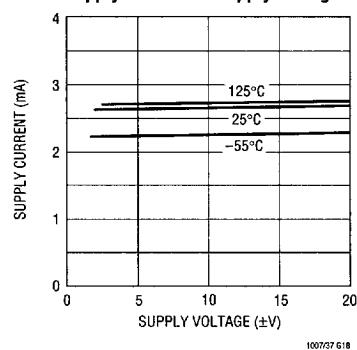
**Long Term Stability of Four Representative Units**



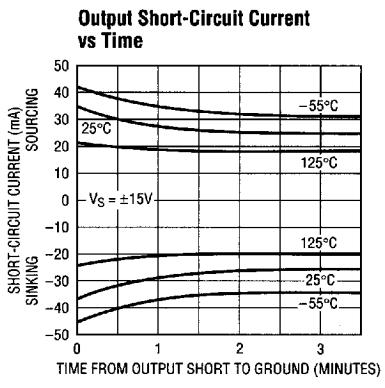
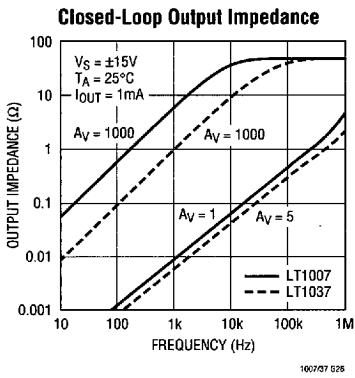
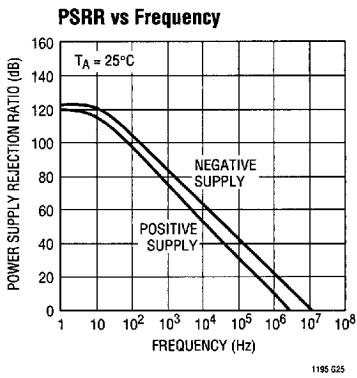
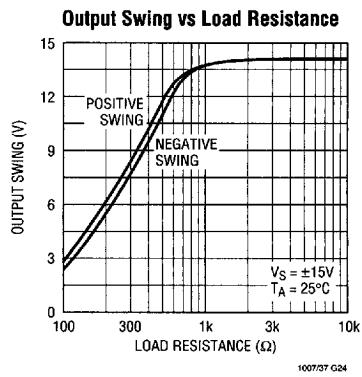
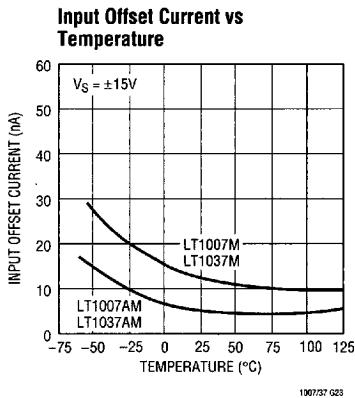
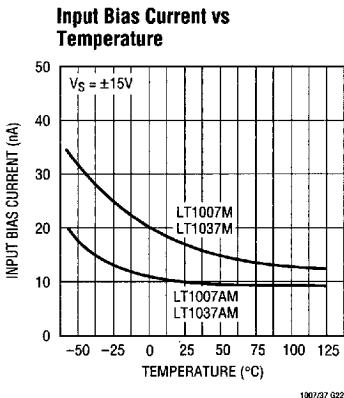
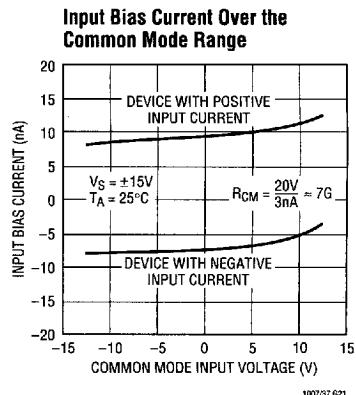
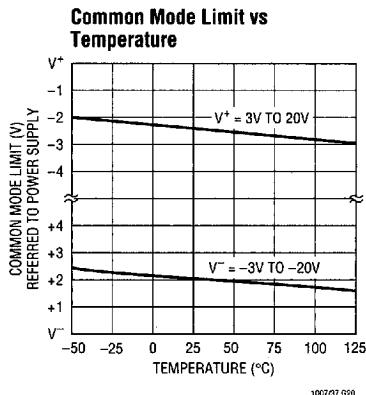
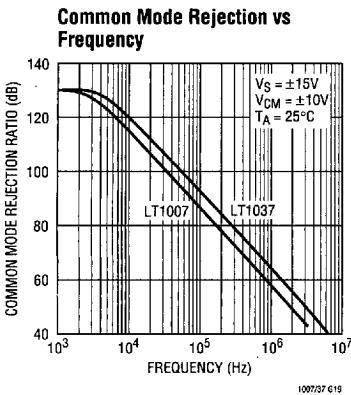
**Offset Voltage Drift with Temperature of Representative Units**



**Supply Current vs Supply Voltage**

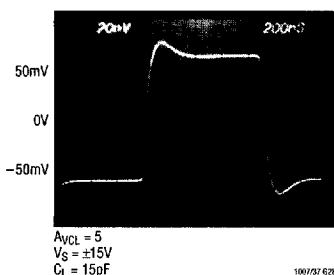


## TYPICAL PERFORMANCE CHARACTERISTICS

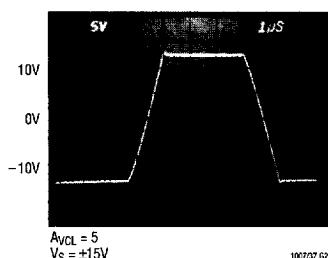


## TYPICAL PERFORMANCE CHARACTERISTICS

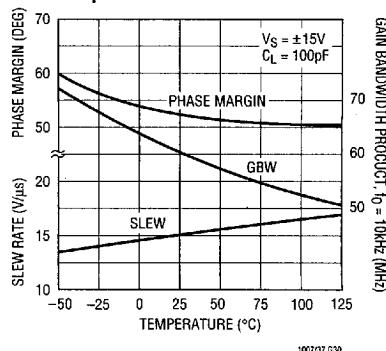
**LT1037 Small-Signal Transient Response**



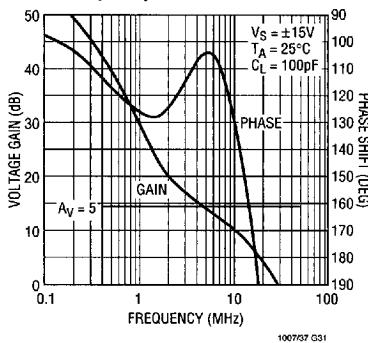
**LT1037 Large-Signal Response**



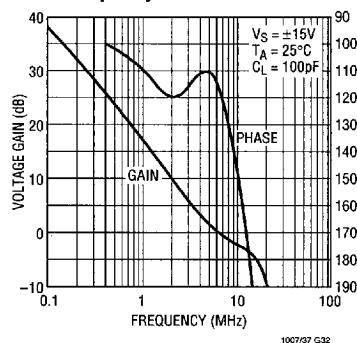
**LT1037 Phase Margin, Gain Bandwidth Product, Slew Rate vs Temperature**



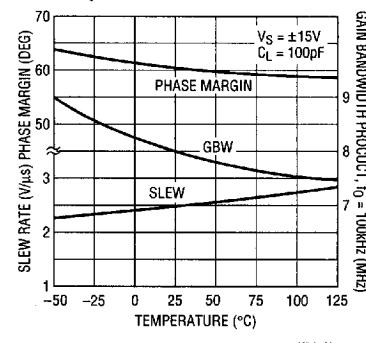
**LT1037 Gain, Phase Shift vs Frequency**



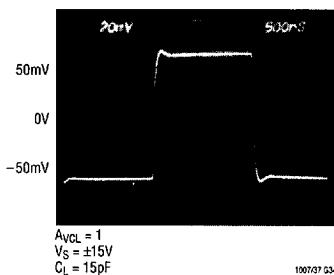
**LT1007 Gain, Phase Shift vs Frequency**



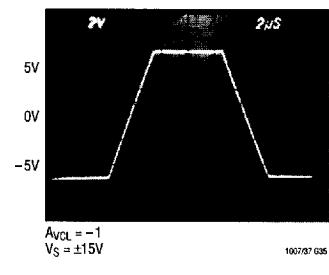
**LT1007 Phase Margin, Gain Bandwidth Product, Slew Rate vs Temperature**



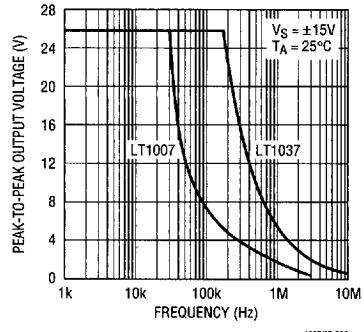
**LT1007 Small-Signal Transient Response**



**LT1007 Large-Signal Response**



**Maximum Undistorted Output vs Frequency**



## APPLICATIONS INFORMATION

### General

The LT1007/LT1037 series devices may be inserted directly into OP-07, OP-27, OP-37 and 5534 sockets with or without removal of external compensation or nulling components. In addition, the LT1007/LT1037 may be fitted to 741 sockets with the removal or modification of external nulling components.

### Offset Voltage Adjustment

The input offset voltage of the LT1007/LT1037 and its drift with temperature, are permanently trimmed at wafer testing to a low level. However, if further adjustment of  $V_{OS}$  is necessary, the use of a  $10k\Omega$  nulling potentiometer will not degrade drift with temperature. Trimming to a value other than zero creates a drift of  $(V_{OS}/300)\mu V/{^\circ}C$ , e.g., if  $V_{OS}$  is adjusted to  $300\mu V$ , the change in drift will be  $1\mu V/{^\circ}C$  (Figure 1).

The adjustment range with a  $10k\Omega$  pot is approximately  $\pm 2.5mV$ . If less adjustment range is needed, the sensitivity and resolution of the nulling can be improved by using a smaller pot in conjunction with fixed resistors. The example has an approximate null range of  $\pm 200\mu V$  (Figure 2).

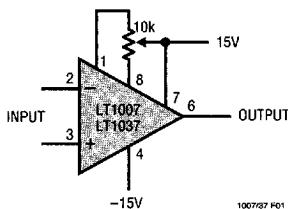


Figure 1. Standard Adjustment

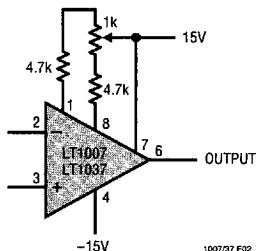


Figure 2. Improved Sensitivity Adjustment

### Offset Voltage and Drift

Thermocouple effects, caused by temperature gradients across dissimilar metals at the contacts to the input terminals, can exceed the inherent drift of the amplifier unless proper care is exercised. Air currents should be minimized, package leads should be short, the two input leads should be close together and maintained at the same temperature.

The circuit shown to measure offset voltage is also used as the burn-in configuration for the LT1007/LT1037, with the supply voltages increased to  $\pm 20V$  (Figure 3).

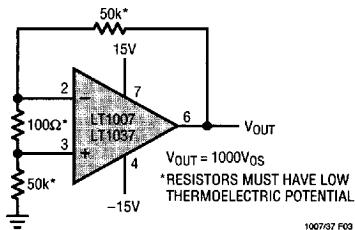


Figure 3. Test Circuit for Offset Voltage and Offset Voltage Drift with Temperature

### Unity-Gain Buffer Application (LT1007 Only)

When  $R_F \leq 100\Omega$  and the input is driven with a fast, large-signal pulse ( $>1V$ ), the output waveform will look as shown in the pulsed operation diagram (Figure 4).

During the fast feedthrough-like portion of the output, the input protection diodes effectively short the output to the input and a current, limited only by the output short-circuit protection, will be drawn by the signal generator. With  $R_F \geq 500\Omega$ , the output is capable of handling the current requirements ( $I_L \leq 20mA$  at  $10V$ ) and the amplifier stays in its active mode and a smooth transition will occur.

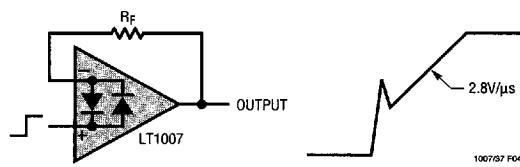


Figure 4. Pulsed Operation

## APPLICATIONS INFORMATION

As with all operational amplifiers when  $R_F > 2k$ , a pole will be created with  $R_F$  and the amplifier's input capacitance, creating additional phase shift and reducing the phase margin. A small capacitor (20pF to 50pF) in parallel with  $R_F$  will eliminate this problem.

### Noise Testing

The 0.1Hz to 10Hz peak-to-peak noise of the LT1007/LT1037 is measured in the test circuit shown (Figure 5a). The frequency response of this noise tester (Figure 5b) indicates that the 0.1Hz corner is defined by only one zero. The test time to measure 0.1Hz to 10Hz noise should not exceed ten seconds, as this time limit acts as an additional zero to eliminate noise contributions from the frequency band below 0.1Hz.

Measuring the typical 60nV peak-to-peak noise performance of the LT1007/LT1037 requires special test precautions:

1. The device should be warmed up for at least five minutes. As the op amp warms up, its offset voltage changes typically 3 $\mu$ V due to its chip temperature increasing 10°C to 20°C from the moment the power supplies are turned on. In the ten-second measurement interval these temperature-induced effects can easily exceed tens of nanovolts.
2. For similar reasons, the device must be well shielded from air currents to eliminate the possibility of thermo-

electric effects in excess of a few nanovolts, which would invalidate the measurements.

3. Sudden motion in the vicinity of the device can also "feedthrough" to increase the observed noise.

A noise voltage density test is recommended when measuring noise on a large number of units. A 10Hz noise voltage density measurement will correlate well with a 0.1Hz to 10Hz peak-to-peak noise reading since both results are determined by the white noise and the location of the 1/f corner frequency.

Current noise is measured in the circuit shown in Figure 6 and calculated by the following formula:

$$i_n = \frac{\left[ (e_{no})^2 - (130\text{nV} \cdot 101)^2 \right]^{1/2}}{(1\text{M}\Omega)(101)}$$

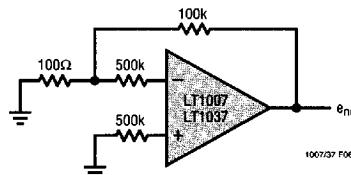


Figure 6

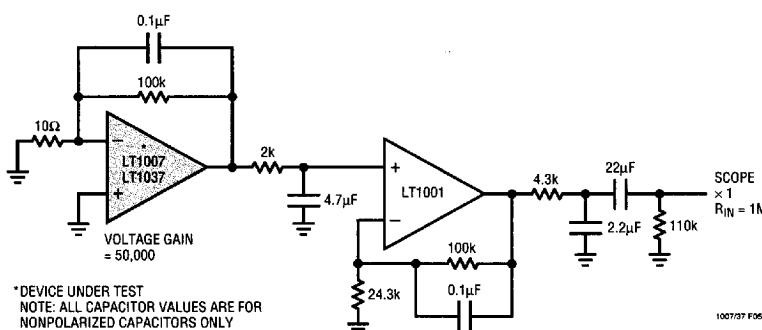


Figure 5a. 0.1Hz to 10Hz Noise Test Circuit

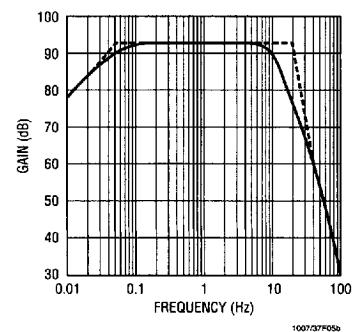


Figure 5b. 0.1Hz to 10Hz Peak-to-Peak Noise Tester Frequency Response

## APPLICATIONS INFORMATION

The LT1007/LT1037 achieve their low noise, in part, by operating the input stage at 120 $\mu$ A versus the typical 10 $\mu$ A of most other op amps. Voltage noise is inversely proportional while current noise is directly proportional to the square root of the input stage current. Therefore, the LT1007/LT1037's current noise will be relatively high. At low frequencies, the low 1/f current noise corner frequency ( $\approx$ 120Hz) minimizes current noise to some extent.

In most practical applications, however, current noise will not limit system performance. This is illustrated in the Total Noise vs Source Resistance plot in the Typical Performance Characteristics section, where:

$$\text{Total Noise} = [( \text{voltage noise})^2 + (\text{current noise} \cdot R_S)^2 + (\text{resistor noise})^2]^{1/2}$$

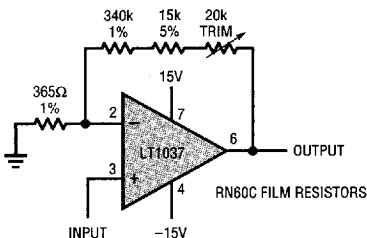
Three regions can be identified as a function of source resistance:

- (i)  $R_S \leq 400\Omega$ . Voltage noise dominates
- (ii)  $400\Omega \leq R_S \leq 50k$  at 1kHz      } Resistor noise  
 $400\Omega \leq R_S \leq 8k$  at 10Hz      } dominates
- (iii)  $R_S > 50k$  at 1kHz      } Current noise  
 $R_S > 8k$  at 10Hz      } dominates

Clearly the LT1007/LT1037 should not be used in region (iii), where total system noise is at least six times higher than the voltage noise of the op amp, i.e., the low voltage noise specification is completely wasted.

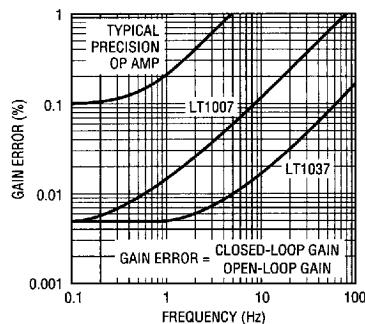
## TYPICAL APPLICATIONS

**Gain 1000 Amplifier with 0.01% Accuracy, DC to 5Hz**



THE HIGH GAIN AND WIDE BANDWIDTH OF THE LT1037 (AND LT1007) IS USEFUL IN LOW FREQUENCY, HIGH CLOSED-LOOP GAIN AMPLIFIER APPLICATIONS. A TYPICAL PRECISION OP AMP MAY HAVE AN OPEN-LOOP GAIN OF ONE MILLION WITH 500kHz BANDWIDTH. AS THE GAIN ERROR PLOT SHOWS, THIS DEVICE IS CAPABLE OF 0.1% AMPLIFYING ACCURACY UP TO 0.3Hz ONLY. EVEN INSTRUMENTATION RANGE SIGNALS CAN VARY AT A FASTER RATE. THE LT1037'S "GAIN PRECISION-BANDWIDTH PRODUCT" IS 200 TIMES HIGHER AS SHOWN.

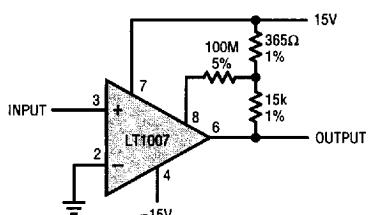
**Gain Error vs Frequency  
Closed-Loop Gain = 1000**



1007/37 TA03

## TYPICAL APPLICATIONS

### Microvolt Comparator with Hysteresis

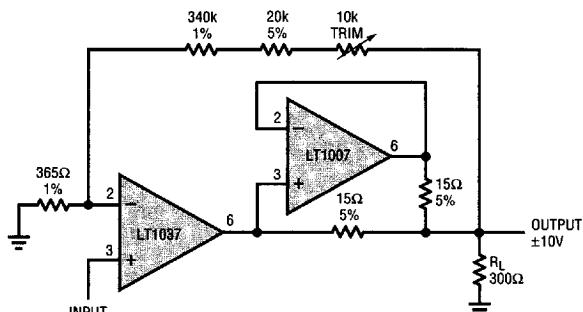


POSITIVE FEEDBACK TO ONE OF THE NULLING TERMINALS  
CREATES APPROXIMATELY 5 $\mu$ V OF HYSTERESIS.  
OUTPUT CAN SINK 16mA.

INPUT OFFSET VOLTAGE IS TYPICALLY CHANGED LESS  
THAN 5 $\mu$ V DUE TO THE FEEDBACK.

1007/97 TA04

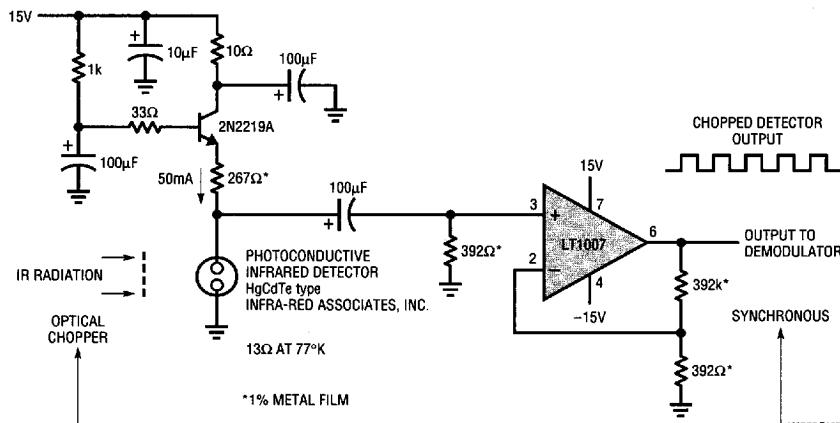
### Precision Amplifier Drives 300Ω Load to $\pm 10V$



THE ADDITION OF THE LT1007 DOUBLES THE AMPLIFIER'S OUTPUT DRIVE  
TO  $\pm 33mA$ . GAIN ACCURACY IS 0.02%, SLIGHTLY DEGRADED COMPARED  
TO ABOVE BECAUSE OF SELF-HEATING OF THE LT1007 UNDER LOAD.

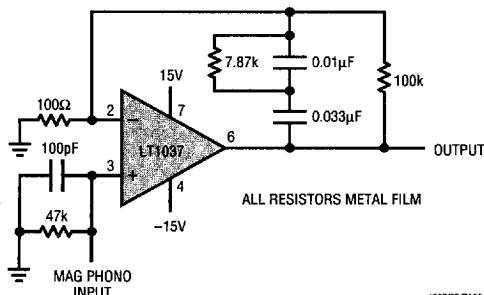
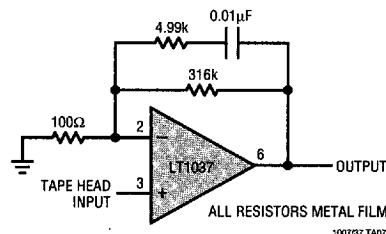
1007/97 TA05

### Infrared Detector Preamplifier



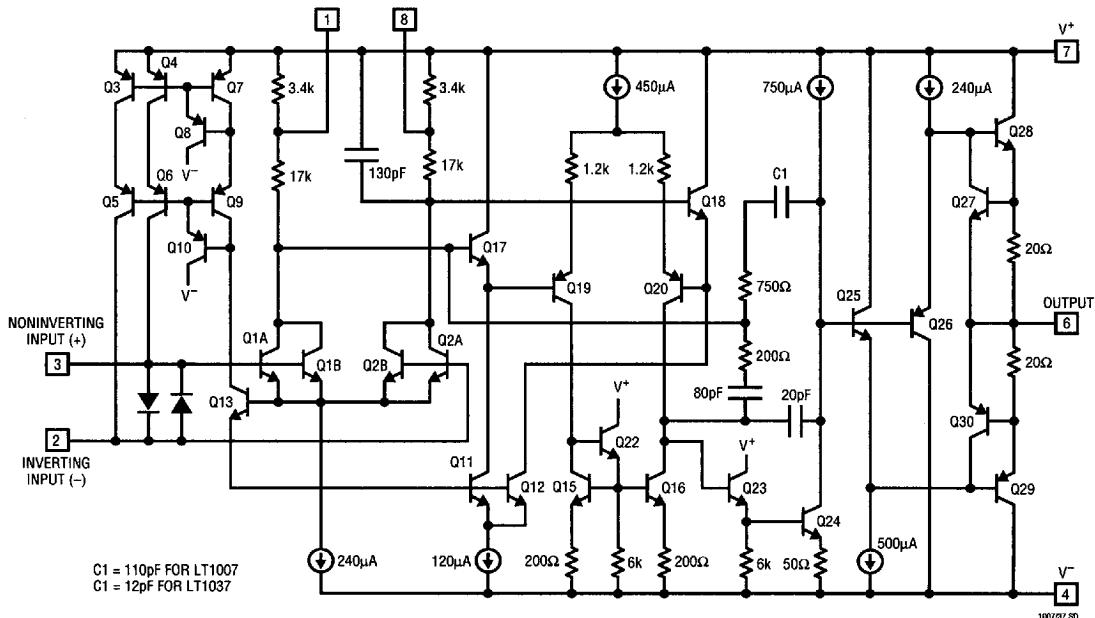
\*1% METAL FILM

1007/97 TA06

**TYPICAL APPLICATIONS****Phono Preamplifier****Tape Head Amplifier**

1007/87 TA06

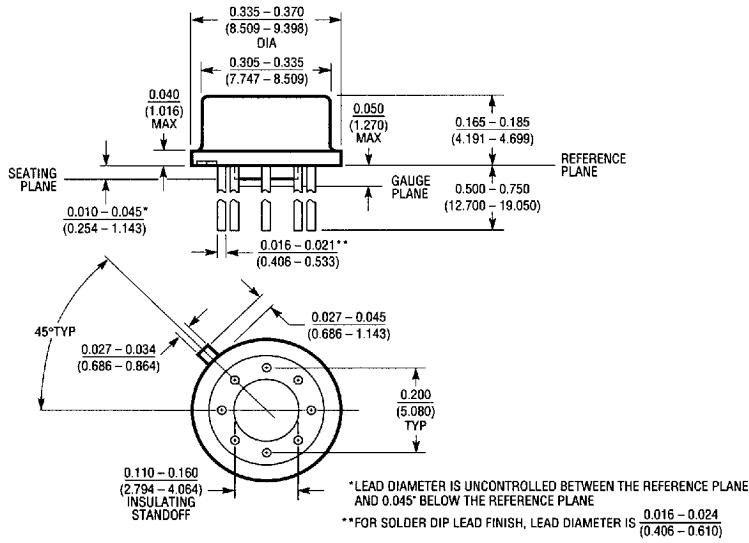
1007/87 TA07

**SIMPLIFIED SCHEMATIC**C1 = 110pF FOR LT1007  
C1 = 12pF FOR LT1037

**PACKAGE DESCRIPTION**

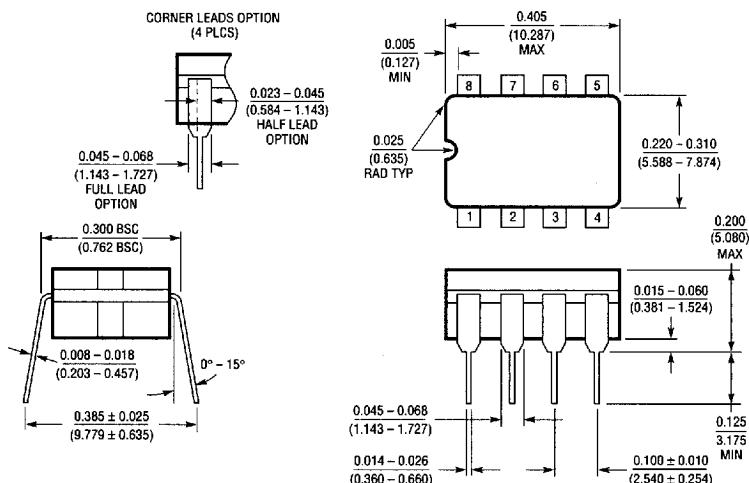
Dimensions in inches (millimeters) unless otherwise noted.

**H Package**  
**8-Lead TO-5 Metal Can (0.200 PCD)**  
(LTC DWG # 05-08-1320)



H8TO-5 0.200 PCD 0995

**J8 Package**  
**8-Lead CERDIP (Narrow 0.300, Hermetic)**  
(LTC DWG # 05-08-1110)



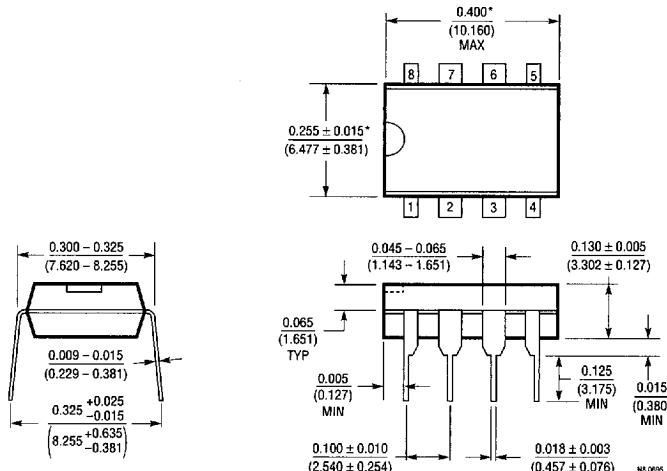
NOTE: LEAD DIMENSIONS APPLY TO SOLDER DIP/PLATE OR TIN PLATE LEADS.

J8 0694

**PACKAGE DESCRIPTION**

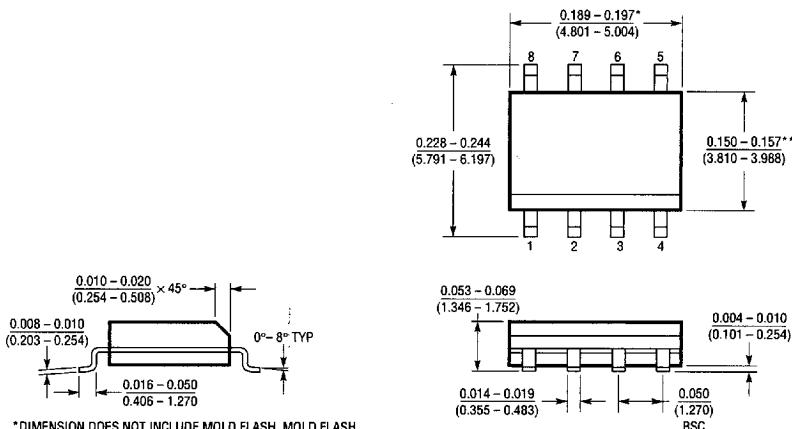
Dimensions in inches (millimeters) unless otherwise noted.

**N8 Package**  
**8-Lead PDIP (Narrow 0.300)**  
(LTC DWG # 05-08-1510)



\*THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.  
MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.010 INCH (0.254mm)

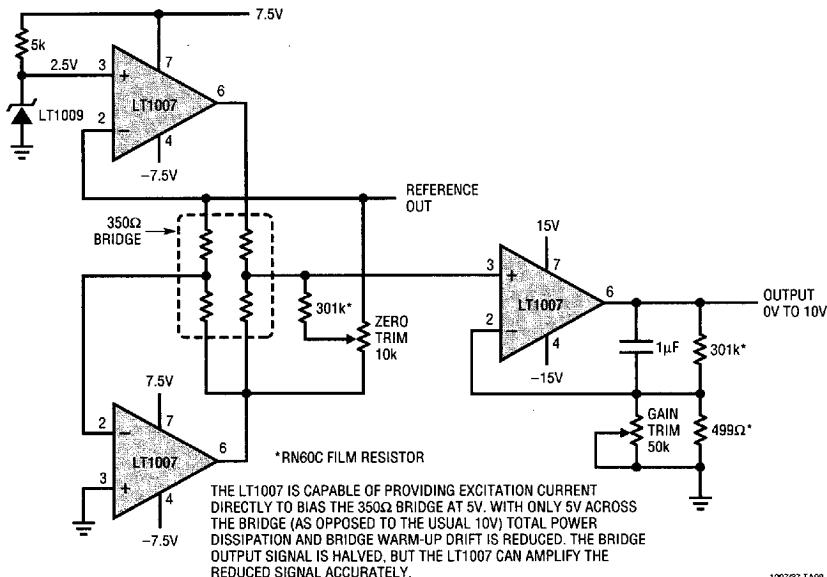
**S8 Package**  
**8-Lead Plastic Small Outline (Narrow 0.150)**  
(LTC DWG # 05-08-1610)



\*DIMENSION DOES NOT INCLUDE MOLD FLASH. MOLD FLASH  
SHALL NOT EXCEED 0.006" (0.152mm) PER SIDE

\*\*DIMENSION DOES NOT INCLUDE INTERLEAD FLASH. INTERLEAD  
FLASH SHALL NOT EXCEED 0.010" (0.254mm) PER SIDE

5518468 0016390 T38

**TYPICAL APPLICATIONS****Strain Gauge Signal Conditioner with Bridge Excitation**

1007/97 TA09

**RELATED PARTS**

PART NUMBER	DESCRIPTION	COMMENTS
LT1028	Ultralow Noise Precision Op Amp	Lowest Noise 0.85mV/√Hz
LT1115	Ultralow Noise, Low distortion Audio Op Amp	0.002% THD, Max Noise 1.2mV/√Hz
LT1124/LT1125	Dual/Quad Low Noise, High Speed Precision Op Amps	Similar to LT1007
LT1126/LT1127	Dual/Quad Decompensated Low Noise, High Speed Precision Op Amps	Similar to LT1037
LT1498/LT1499	10MHz, 5V/μs, Dual/Quad Rail-to-Rail Input and Output Precision C-Load™ Op Amps	

C-Load is a trademark of Linear Technology Corporation.