# PHASE-LOCKED LOOP



The HEF4046B is a phase-locked loop circuit that consists of a linear voltage controlled oscillator (VCO) and two different phase comparators with a common signal input amplifier and a common comparator input. A 7 V regulator (zener) diode is provided for supply voltage regulation if necessary. For functional description see further on in this data.

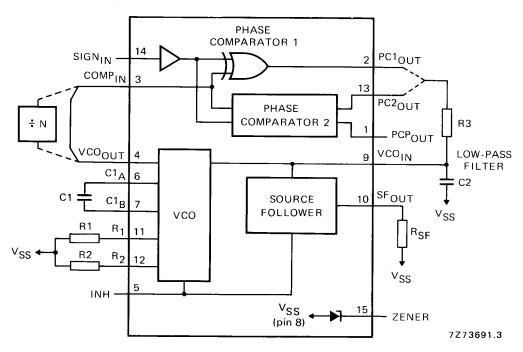


Fig. 1 Functional diagram.

HEF4046BP: 16-lead DIL; plastic (SOT-38Z).

HEF4046BD: 16-lead DIL; ceramic (cerdip) (SOT-74).

HEF4046BT: 16-lead mini-pack; plastic (SO-16; SOT-109A).

FAMILY DATA: see Family Specifications

IDD LIMITS category MSI: see further on in this data.



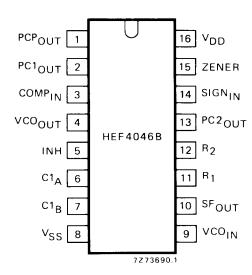


Fig. 2 Pinning diagram.

## **PINNING**

- 1. Phase comparator pulse output
- 2. Phase comparator 1 output
- 3. Comparator input
- 4. VCO output
- 5. Inhibit input
- 6. Capacitor C1 connection A
- 7. Capacitor C1 connection B
- 8. VSS
- 9. VCO input
- 10. Source-follower output
- 11. Resistor R1 connection
- 12. Resistor R2 connection
- 13. Phase comparator 2 output
- 14. Signal input
- 15. Zener diode input for regulated supply.

## **FUNCTIONAL DESCRIPTION**

### VCO part

The VCO requires one external capacitor (C1) and one or two external resistors (R1 or R1 and R2). Resistor R1 and capacitor C1 determine the frequency range of the VCO. Resistor R2 enables the VCO to have a frequency off-set if required. The high input impedance of the VCO simplifies the design of low-pass filters; it permits the designer a wide choice of resistor/capacitor ranges. In order not to load the low-pass filter, a source-follower output of the VCO input voltage is provided at pin 10. If this pin (SF<sub>OUT</sub>) is used, a load resistor (R<sub>SF</sub>) should be connected from this pin to V<sub>SS</sub>; if unused, this pin should be left open. The VCO output (pin 4) can either be connected directly to the comparator input (pin 3) or via a frequency divider. A LOW level at the inhibit input (pin 5) enables the VCO and the source follower, while a HIGH level turns off both to minimize stand-by power consumption.

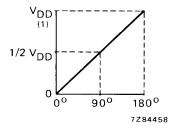
### Phase comparators

The phase-comparator signal input (pin 14) can be direct-coupled, provided the signal swing is between the standard HE4000B family input logic levels. The signal must be capacitively coupled to the self-biasing amplifier at the signal input in case of smaller swings. Phase comparator 1 is an EXCLUSIVE-OR network. The signal and comparator input frequencies must have a 50% duty factor to obtain the maximum lock range. The average output voltage of the phase comparator is equal to ½  $V_{DD}$  when there is no signal or noise at the signal input. The average voltage to the VCO input is supplied by the low-pass filter connected to the output of phase comparator 1. This also causes the VCO to oscillate at the centre frequency ( $f_{D}$ ). The frequency capture range (2  $f_{C}$ ) is defined as the frequency range of input signals on which the PLL will lock if it was initially out of lock. The frequency lock range (2  $f_{C}$ ) is defined as the frequency range of input signals on which the loop will stay locked if it was initially in lock. The capture range is smaller or equal to the lock range.

With phase comparator 1, the range of frequencies over which the PLL can acquire lock (capture range) depends on the low-pass filter characteristics and this range can be made as large as the lock range. Phase comparator 1 enables the PLL system to remain in lock in spite of high amounts of noise in the input signal. A typical behaviour of this type of phase comparator is that it may lock onto input

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frequencies that are close to harmonics of the VCO centre frequency. Another typical behaviour is, that the phase angle between the signal and comparator input varies between 0° and 180° and is 90° at the centre frequency. Figure 3 shows the typical phase-to-output response characteristic.



(1) Average output voltage.

Fig. 3 Signal-to-comparator inputs phase difference for comparator 1.

Figure 4 shows the typical waveforms for a PLL employing phase comparator 1 in locked condition of  $f_0$ .

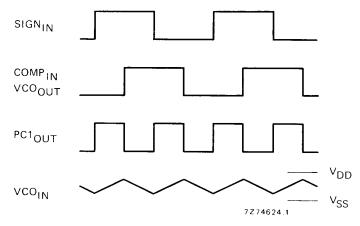


Fig. 4 Typical waveforms for phase-locked loop employing phase comparator 1 in locked condition of  $f_0$ .

### FUNCTIONAL DESCRIPTION (continued)

Phase comparator 2 is an edge-controlled digital memory network. It consists of four flip-flops, control gating and a 3-state output circuit comprising p and n-type drivers having a common output node. When the p-type or n-type drivers are ON, they pull the output up to  $V_{DD}$  or down to  $V_{SS}$  respectively. This type of phase comparator only acts on the positive-going edges of the signals at SIGN<sub>IN</sub> and COMP<sub>IN</sub>. Therefore, the duty factors of these signals are not of importance.

If the signal input frequency is higher than the comparator input frequency, the p-type output driver is maintained ON most of the time, and both the n and p-type drivers are OFF (3-state) the remainder of the time. If the signal input frequency is lower than the comparator input frequency, the n-type output driver is maintained ON most of the time, and both the n and p-type drivers are OFF the remainder of the time. If the signal input and comparator input frequencies are equal, but the signal input lags the comparator input in phase, the n-type output driver is maintained ON for a time corresponding to the phase difference. If the comparator input lags the signal input in phase, the p-type output driver is maintained ON for a time corresponding to the phase difference. Subsequently, the voltage at the capacitor of the low-pass filter connected to this phase comparator is adjusted until the signal and comparator inputs are equal in both phase and frequency. At this stable point, both p and n-type drivers remain OFF and thus the phase comparator output becomes an open circuit and keeps the voltage at the capacitor of the low-pass filter constant.

Moreover, the signal at the phase comparator pulse output (PCP<sub>OUT</sub>) is a HIGH level which can be used for indicating a locked condition. Thus, for phase comparator 2 no phase difference exists between the signal and comparator inputs over the full VCO frequency range. Moreover, the power dissipation due to the low-pass filter is reduced when this type of phase comparator is used because both p and n-type output drivers are OFF for most of the signal input cycle. It should be noted that the PLL lock range for this type of phase comparator is equal to the capture range, independent of the low-pass filter. With no signal present at the signal input, the VCO is adjusted to its lowest frequency for phase comparator 2. Figure 5 shows typical waveforms for a PLL employing this type of phase comparator in locked condition.

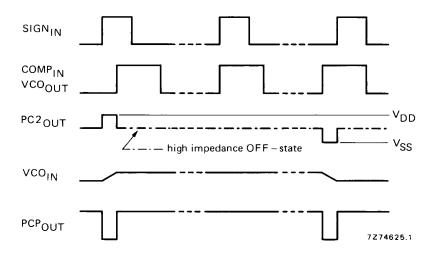
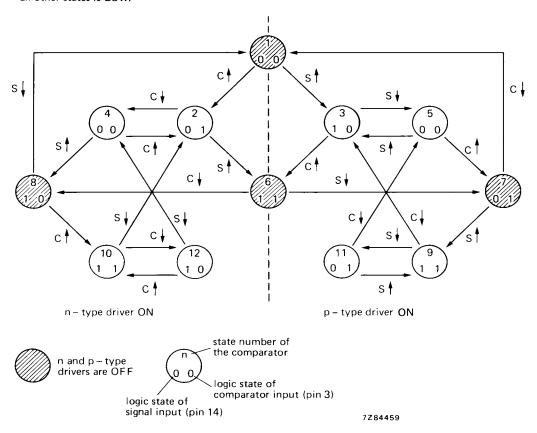


Fig. 5 Typical waveforms for phase-locked loop employing phase comparator 2 in locked condition.

Figure 6 shows the state diagram for phase comparator 2. Each circle represents a state of the comparator. The number at the top, inside each circle, represents the state of the comparator, while the logic state of the signal and comparator inputs are represented by a '0' for a logic LOW or a '1' for a logic HIGH, and they are shown in the left and right bottom of each circle.

The transitions from one to another result from either a logic change at the signal input (S) or the comparator input (C). A positive-going and a negative-going transition are shown by an arrow pointing up or down respectively.

The state diagram assumes, that only one transition on either the signal input or comparator input occurs at any instant. States 3, 5, 9 and 11 represent the condition at the output when the p-type driver is ON, while states 2, 4, 10 and 12 determine the condition when the n-type driver is ON. States 1, 6, 7 and 8 represent the condition when the output is in its high impedance OFF state; i.e. both p and n-type drivers are OFF, and the PCPOUT output is HIGH. The condition at output PCPOUT for all other states is LOW.



S \(\pma: 0\) to 1 transition at the signal input.

 $C \downarrow : 1$  to 0 transition at the comparator input.

Fig. 6 State diagram for comparator 2.

# D.C. CHARACTERISTICS

 $V_{SS} = 0 V$ 

	V <sub>DD</sub> V	symbol	typ.	-40 max.	T <sub>am</sub> + 2 typ.	b ( <sup>O</sup> C) 25 max.	+ typ.	85 max.	
Supply current (note 1)	5 10 15	I <sub>D</sub>	_ _ _		20 300 750	<del>-</del> -	_ _ _	_ _ _	μΑ μΑ μΑ
Quiescent device current (note 2)	5 10 15	IDD	<u>-</u> 	20 40 80	 	20 40 80	_ _ _	150 300 600	μΑ μΑ μΑ

### Notes

- 1. Pin 15 open; pin 5 at  $V_{DD}$ ; pins 3 and 9 at  $V_{SS}$ ; pin 14 open. 2. Pin 15 open; pin 5 at  $V_{DD}$ ; pins 3 and 9 at  $V_{SS}$ ; pin 14 at  $V_{DD}$ ; input current pin 14 not included.

# A.C. CHARACTERISTICS

 $V_{SS}$  = 0 V;  $T_{amb}$  = 25 °C;  $C_L$  = 50 pF; input transition times  $\leq$  20 ns

	V <sub>DD</sub> V	symbol	min.	typ.	max.		
Phase comparators							
Operating supply voltage		V <sub>DD</sub>	3		15 V	.	
Input resistance at SIGN <sub>IN</sub>	5 10 15	R <sub>IN</sub>		750 220 140	k	Ω	at self-bias operating point
A.C. coupled input sensitivity at SIGN <sub>IN</sub>	5 10 15	VIN		150 150 200	m	iV iV iV	peak-to-peak values; R1 = 10 kΩ; R2 = ∞; C1 = 100 pF; independent of the lock range
D.C. coupled input sensitivity at SIGN <sub>IN</sub> ; COMP <sub>IN</sub> LOW level	5 10 15	VIL			1,5 V 3,0 V 4,0 V	'	
HIGH level	5 10 15	V <sub>IH</sub>	3,5 7,0 11,0		,,	,	full temperature range
Input current at SIGN <sub>IN</sub>	5 10 15	+I <sub>IN</sub>		7 30 70	μ. μ. μ.	Α	SIGN <sub>IN</sub> at V <sub>DD</sub>
	5 10 15	-I <sub>IN</sub>		3 18 45	μ. μ. μ.	A	SIGN <sub>IN</sub> at V <sub>SS</sub>

A.C. CHARACTERISTICS  $V_{SS}$  = 0 V;  $T_{amb}$  = 25 °C;  $C_L$  = 50 pF; input transition times  $\leq$  20 ns

	V <sub>DD</sub> V	symbol	min.	typ.	max	ζ.	
VCO Operating supply voltage		V <sub>DD</sub>	3		15 15	V V	as fixed oscillator only phase-locked loop operation
Power dissipation	5 10 15	P		150 2500 9000		μW μW μW	$\begin{cases} f_0 = 10 \text{ kHz; R1} = 1 \text{ M}\Omega; \\ \text{R2} = \infty; \text{ VCO}_{\text{IN}} \text{ at } \frac{1}{2} \text{ V}_{\text{DD}}; \\ \text{see also Figs 10 and 11} \end{cases}$
Maximum operating frequency	5 10 15	f <sub>max</sub>	0,5 1,0 1,3	1,0 2,0 2,7		MHz MHz MHz	$\begin{cases} VCO_{\text{IN}} \text{ at } V_{\text{DD}}; \\ R1 = 10 \text{ k}\Omega; \text{ R2} = \infty; \\ C1 = 50 \text{ pF} \end{cases}$
Temperature/ frequency stability	5 10 15			0,22-0,30 0,04-0,05 0,01-0,05		%/ºC %/ºC %/ºC	no frequency offset (f <sub>min</sub> = 0); see also note 1
	5 10 15			0-0,22 0-0,04 0-0,01		%/ºC %/ºC %/ºC	with frequency offset (f <sub>min</sub> > 0); see also note 1
Linearity	5 10 15			0,50 0,25 0,25		% % %	R1 > 10 kΩ see Fig. 13 R1 > 400 kΩ and Figs 14 R1 = 1 MΩ 15 and 16
Duty factor at VCOOUT	5 10 15	δ		50 50 50		% % %	
Input resistance at VCOIN	5 10 15	R <sub>IN</sub>		10 <sup>6</sup> 10 <sup>6</sup> 10 <sup>6</sup>		$\Omega$ M $\Omega$ M $\Omega$	
Source follower Offset voltage VCO <sub>IN</sub> minus SF <sub>OUT</sub>	5 10 15			1,7 2,0 2,1		V V V	$ \begin{cases} R_{SF} = 10 \text{ k}\Omega; \\ VCO_{IN} \text{ at } \frac{1}{2} \text{ V}_{DD} \end{cases} $
	5 10 15			1,5 1,7 1,8		V V V	$\begin{cases} R_{SF} = 50 \text{ k}\Omega; \\ VCO_{IN} \text{ at } \frac{1}{2} V_{DD} \end{cases}$
Linearity	5 10 15			0,3 1,0 1,3		% % %	$ Arr R_{SF} > 50 \text{ k}\Omega;$ see Fig. 13
Zener diode Zener voltage		\		7 2		V	I = 50A
Dynamic resistance		V <sub>Z</sub> R <sub>Z</sub>		7,3 25		Ω	$I_Z = 50 \mu A$ $I_Z = 1 mA$

# Notes

1. Over the recommended component range.

### **DESIGN INFORMATION**

characteristic	using phase comparator 1	using phase comparator 2				
No signal on SIGN <sub>IN</sub>	VCO in PLL system adjusts to centre frequency (f <sub>o</sub> )	VCO in PLL system adjusts to min. frequency (f <sub>min</sub> )				
Phase angle between SIGN <sub>IN</sub> and COMP <sub>IN</sub>	90° at centre frequency (f <sub>0</sub> ), approaching 0° and 180° at ends of lock range (2 f <sub>L</sub> )	always 0 <sup>o</sup> in lock (positive-going edges)				
Locks on harmonics of centre frequency	yes	no				
Signal input noise rejection	high	low				
Lock frequency range (2 f <sub>L</sub> )	, , ,	the frequency range of the input signal on which the loop will stay locked if it was initially in lock; $2 f_L = full \ VCO \ frequency range = f_{max} - f_{min}$				
Capture frequency range (2 f <sub>C</sub> )	the frequency range of the input signal on which the loop will lock if it was initially out of lock					
	depends on low-pass filter characteristics; $f_{\hbox{\scriptsize C}} < f_{\hbox{\scriptsize L}}$	$f_C = f_L$				
Centre frequency (f <sub>o</sub> )	the frequency of the VCO whe	the frequency of the VCO when VCO $_{ extstyle IN}$ at ${}^{1\!\!/_{ extstyle V}}$ VDD				

### VCO component selection

Recommended range for R1 and R2: 10 k $\Omega$  to 1 M $\Omega$ ; for C1: 50 pF to any practical value.

- 1. VCO without frequency offset (R2 =  $\infty$ ).
  - a. Given fo: use fo with Fig. 7 to determine R1 and C1.
  - b. Given  $f_{max}$ : calculate  $f_0$  from  $f_0 = \frac{1}{2} f_{max}$ ; use  $f_0$  with Fig. 7 to determine R1 and C1.
- 2. VCO with frequency offset.
  - a. Given  $f_0$  and  $f_L$ : calculate  $f_{min}$  from the equation  $f_{min} = f_0 f_L$ ; use  $f_{min}$  with Fig. 8 to determine R2 and C1; calculate

$$\frac{f_{max}}{f_{min}}$$
 from the equation 
$$\frac{f_{max}}{f_{min}} = \frac{f_0 + f_L}{f_0 - f_L}$$
; use 
$$\frac{f_{max}}{f_{min}}$$
 with Fig. 9 to determine the ratio R2/R1 to obtain R1.

b. Given  $f_{min}$  and  $f_{max}$ : use  $f_{min}$  with Fig. 8 to determine R2 and C1; calculate  $\frac{f_{max}}{f_{min}}$ ; use  $\frac{f_{max}}{f_{min}}$ ; with Fig. 9 to determine R2/R1 to obtain R1.

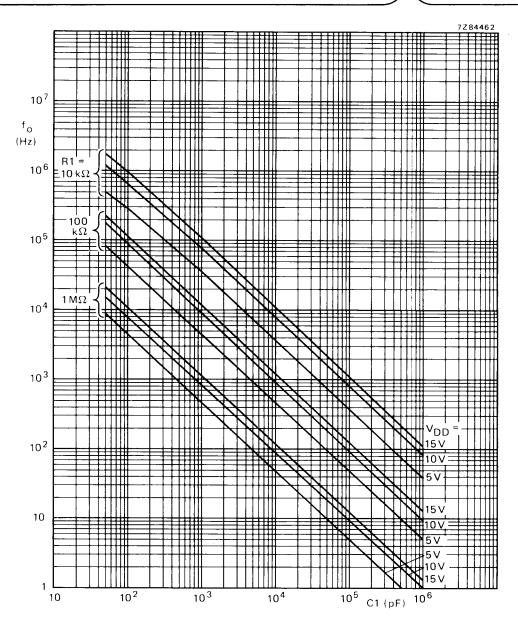


Fig. 7 Typical centre frequency as a function of capacitor C1;  $T_{amb}$  = 25 °C;  $VCO_{IN}$  at  $\frac{1}{2}V_{DD}$ ; INH at  $V_{SS}$ ; R2 =  $\infty$ .

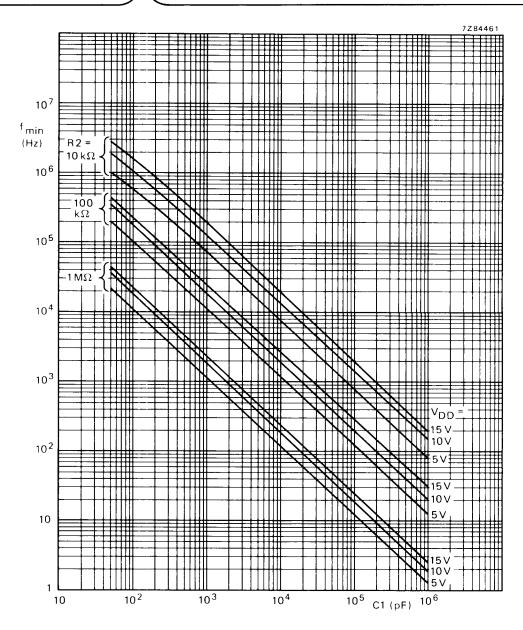


Fig. 8 Typical frequency offset as a function of capacitor C1;  $T_{amb}$  = 25 °C; VCO IN at VSS; INH at VSS; R1 =  $\infty$ .

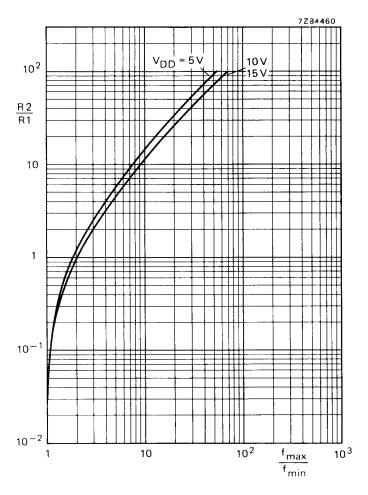


Fig. 9 Typical ratio of R2/R1 as a function of the ratio  $f_{\mbox{\scriptsize max}}/f_{\mbox{\scriptsize min}}.$ 

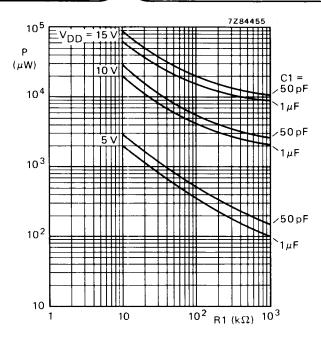


Fig. 10 Power dissipation as a function of R1; R2 =  $\infty$ ; VCO<sub>1N</sub> at ½ V<sub>DD</sub>; C<sub>L</sub> = 50 pF.

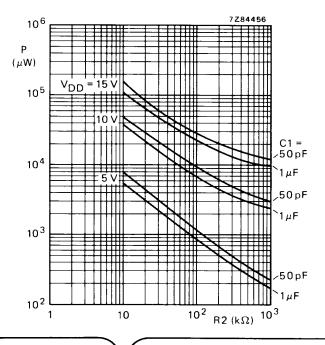


Fig. 11 Power dissipation as a function of R2; R1 =  $\infty$ ; VCO<sub>IN</sub> at VSS (0 V); C<sub>L</sub> = 50 pF.

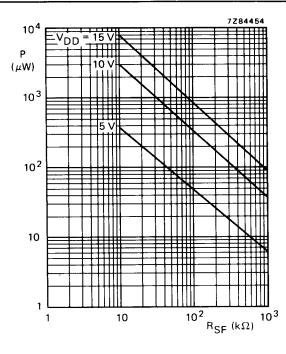


Fig. 12 Power dissipation of source follower as a function of RSF; VCO<sub>IN</sub> at  $\frac{1}{2}$  V<sub>DD</sub>; R1 =  $\infty$ ; R2 =  $\infty$ .

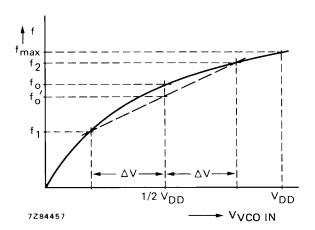


Fig. 13 Definition of linearity (see a.c. characteristics).

For VCO linearity:

$$f'_{0} = \frac{f_{1} + f_{2}}{2}$$
  
Iin. =  $\frac{f'_{0} - f_{0}}{f'_{0}} \times 100\%$ 

Figure 13 and the above formula also apply to source follower linearity: substitute VSF OUT for f.

$$\Delta$$
V = 0,3 V at V<sub>DD</sub> = 5 V  
 $\Delta$ V = 2,5 V at V<sub>DD</sub> = 10 V  
 $\Delta$ V = 5 V at V<sub>DD</sub> = 15 V

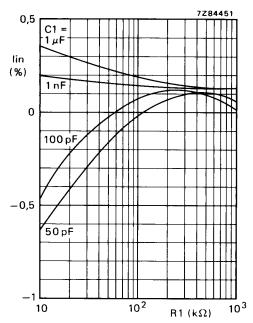
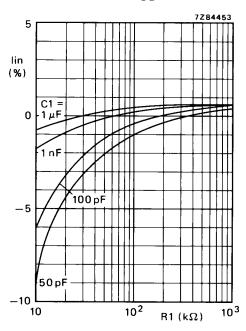


Fig. 14 VCO frequency linearity as a function of R1; R2 =  $\infty$ ; V<sub>DD</sub> = 5 V.



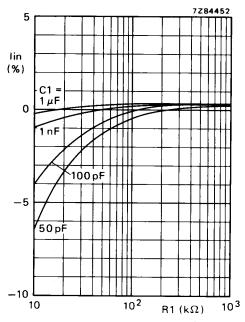


Fig. 15 VCO frequency linearity as a function of R1; R2 =  $\infty$ ; V<sub>DD</sub> = 10 V.

Fig. 16 VCO frequency linearity as a function of R1; R2 =  $\infty$ ; V<sub>DD</sub> = 15 V.