

Features

- EL7556C Pin Compatible
- Improved Temperature and Voltage Ranges
- 6A Continuous Load Current
- Precision Internal 1% Reference
- 1.0V to 3.8V Output Voltage
- Internal Power MOSFETs
- >90% Efficiency
- Synchronous Switching
- Adjustable Slope Compensation
- Over Temperature Indicator
- Pulse by Pulse Current Limiting
- Operates up to 1MHz
- 1.5% Typical Output Accuracy
- Adjustable Oscillator w/Sync
- Remote Enable/Disable
- Intel P54 and P55 Compatible
- VCC2DET Interface
- Internal Soft Start

Applications

- PC Motherboards
- Local high power CPU supplies
- 5V to 1.0V DC-DC Conversion
- Portable Electronics/Instruments
- P54 and P55 Regulators
- GTL+ Bus Power Supply

Ordering Information

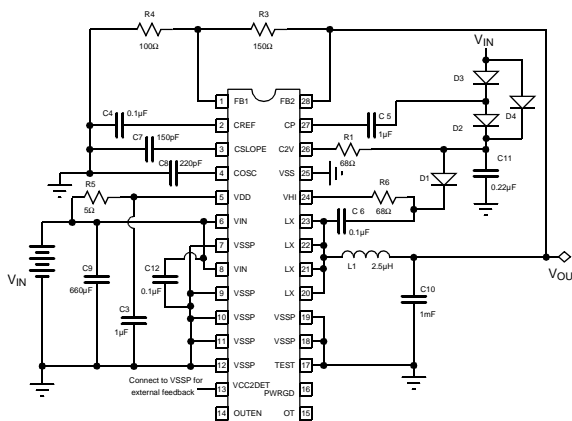
Part No	Temp. Range	Package	Outline #
EL7556ACM	-40°C to +85°C	28-Lead SOIC	MDP0027

General Description

The EL7556AC is an adjustable synchronous DC:DC switching regulator optimized for a 5V input and 1.0-3.8V output. By combining integrated NMOS power FETs with a fused-lead package the EL7556AC can supply up to 6A continuous output current without the use of external power devices or discrete heat sinks, thereby minimizing design effort and overall system cost.

On chip resistorless current sensing is used to achieve stable, highly efficient, current-mode control. The EL7556AC also incorporates the VCC2DET function to directly interface with the Intel P54 and P55 microprocessors. Depending on the state of VCC2DET the output voltage is internally preset to 3.50V or a user adjustable voltage using two external resistors. In both internal and external feedback modes the active-high PWRGD output indicates when the regulator output is within $\pm 10\%$ of the programmed voltage. An on-board sensor monitors die temperature (OT) for over-temperature conditions and can be connected directly to OUTEN to provide automatic thermal shutdown. Adjustable oscillator frequency and slope compensation allow added flexibility in overall system design.

Connection Diagram



EL7556AC

C3, C4, C5, C6, C7, C8 - ceramic
C9, C11 - ceramic or tantalum
C10 - Sprague 694D337X10010R27 2X330uF
C12 - Sprague 694D337X10010R27 3X330uF
L1 - Pulse Engineering PE-53681
D1-D4: BAT54S fast diode

Manufactured under U.S. Patents No. 5,723,974 and No. 5,793,126

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Programmable CPU Power Supply Unit

Absolute Maximum Ratings (T_A = 25 °C)

Storage Temperature Range	-65°C to +150°C	Output Pins	-0.3V below GND, +0.3V above VDD
Supply (V _{IN})	6.0V	Operating Junction Temperature	135°C
Ambient Operating Temperature	-40°C to +85°C	Peak Output Current	9A

Important Note:

All parameters having Min/Max specifications are guaranteed. Typ values are for information purposes only. Unless otherwise noted, all tests are at the specified temperature and are pulsed tests, therefore: T_J = T_C = T_A.

Electrical Characteristics

V_{DD} = V_{IN} = 5V, C_{OSC} = 1nF, C_{SLOPE}=470pF, T_A=25°C unless otherwise specified.

Parameter	Description	Conditions	Min	Typ	Max	Units
General						
I _{DD}	V _{DD} Supply Current	OUTEN=4V, F _{OSC} =120kHz		11	25	mA
I _{DDOFF}	V _{DD} Standby Current	OUTEN=0		0.1		mA
I _{VIN}	V _{IN} No Load Current	OUTEN=0		3	5	mA
V _{OUT1}	Output Initial Accuracy	VCC2DET=4V, IL=3A(See Fig. 1)	3.450	3.500	3.550	V
V _{OUT2}	Output Initial Accuracy	VCC2DET=0V, IL=3A R3=150Ω, R4=100Ω (See Fig. 1)	2.450	2.500	2.550	V
V _{OUTLINE}	Output line Regulation	VDD=5V, ±10%	-1		1	%
V _{OUTLOAD}	Output Load Regulation	0A<I _{LOAD} <6A, Relative to IL=3A. Continuous Mode of Operation (Fig.1)	-1		1	%
R _{SHORT}	Short Circuit Load Resistance	IL=6A Prior to Continuous Application of R _{SHORT} . OUTEN Connected to OT.		100		mΩ
I _{I MAX}	Current Limit			9		A
V _{OUTTC}	Output Tempco	-40°C<T _a <85°C		±1		%
T _{OT}	Over Temperature Threshold			135		°C
T _{HYS}	Over Temperature Hysteresis			40		°C
V _{PWRGD}	Power Good Threshold Relative to Programmed Output Voltage	VCC2SEL=4V, VOUT=3.50V	±6	±10	±14	%
V _{DDOFF}	Minimum VDD for Shutdown		3.15			V
V _{DDON}	Maximum VDD for Startup				4.15	V
V _{HYS}	Input Hysteresis	V _{HYS} =V _{DDON} -V _{DDOFF}		0.5		V
M _{SS}	Soft start slope			7		V/msec
D _{MAX}	Maximum duty cycle			96		%
Controller - Inputs						
I _{PUP}	VCC2DET, OUTEN Pull Up Current	VCC2DET, OUTEN=0	10	14	18	μA
I _{CSLOPE}	Cslope Charging Current		23	28.5	34	μA
I _{FB1}	FB1 Input Pull Up Current			2		μA
R _{OT}	Over Temperature Pull Up Resistance	OT=0V	30	40	50	kΩ
V _{IH}	VCC2DET, OUTEN Input High		4			V
V _{IL}	VCC2DET, OUTEN Input Low				.8	V
V _{OH PWGD}	Powergood Drive High	I _{Load} =1mA	3.5			V
V _{OL PWGD}	Powergood Drive Low	I _{Load} =-1mA			1.0	V
Controller - Reference						
V _{REF}	Reference Accuracy	I _{REF} =0	1.247	1.260	1.273	V
V _{REFTC}	Reference Voltage Tempco			50		ppm/°C
V _{REFLOAD}	Reference Load Regulation	0<I _{LOAD} <100μA	0.5		0.5	%/°C

Electrical Characteristics

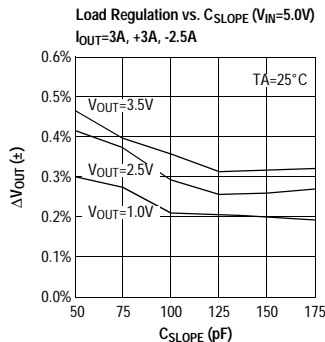
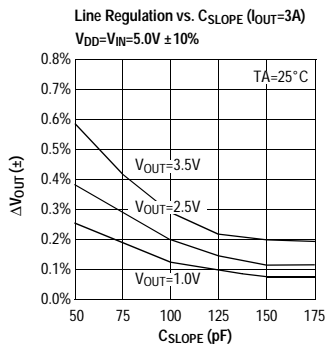
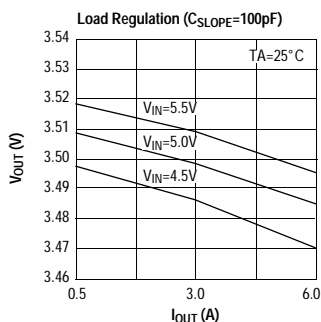
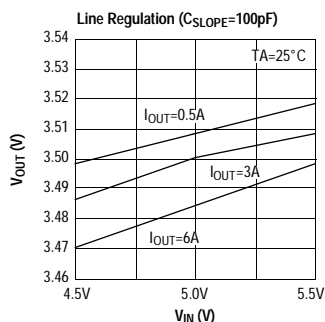
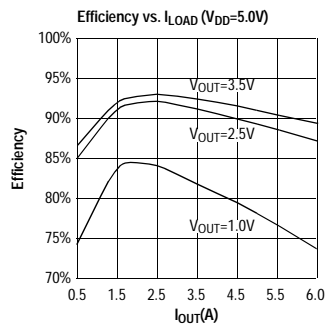
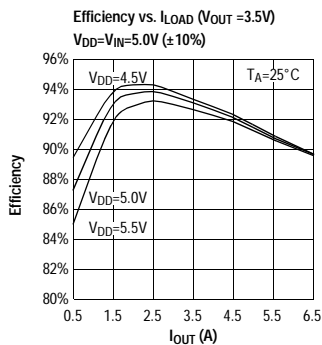
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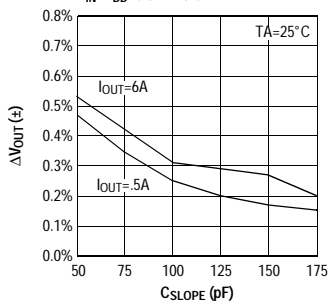
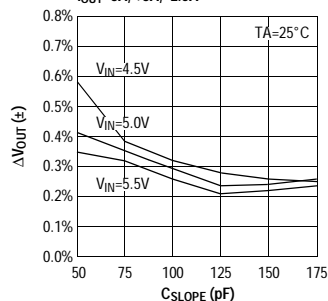
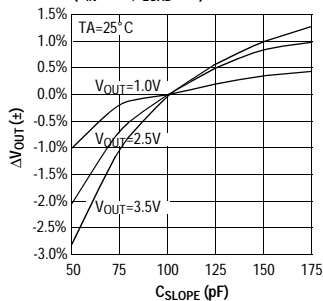
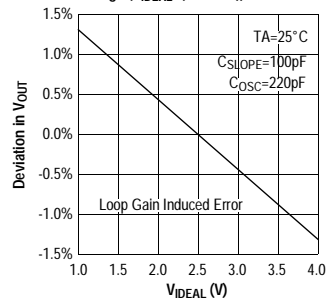
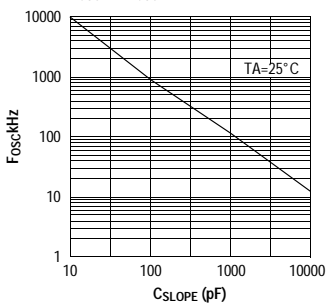
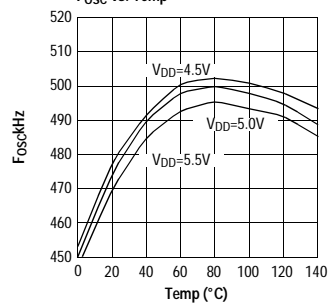
Parameter	Description	Conditions	Min	Typ	Max	Units
Controller - Doubler						
V_{C2V}	Voltage Doubler Output	$V_{dd} = 5V$, $I_{LOAD} = 10mA$	7.1	7.7	8.3	V
Controller - Oscillator						
F_{RAMP}	Oscillator Ramp Amplitude			1.2		V
$I_{OSC\ CHG}$	Oscillator Charge Current	$.2V < V_{OSC} < 1.4V$		150		μA
$I_{OSC\ DIS}$	Oscillator Discharge Current	$.2V < V_{OSC} < 1.4V$		5		mA
F_{OSC}	Oscillator initial accuracy		100	120	140	kHz
t_{sync}	Minimum oscillator sync width			50		ns
Power - FET						
I_{LEAK}	LX Output Leakage to VSS	$LX = 0V$			100	μA
$R_{DS(on)}$	Composite FET Resistance		18		30	m Ω
$R_{DS(on)TC}$	$R_{DS(on)}$ Tempco			0.1		m $\Omega/^\circ C$
t_{brm}	FET break before make delay			10		ns
t_{LEB}	High side FET minimum on time (LEB)			140		ns

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Programmable CPU Power Supply Unit

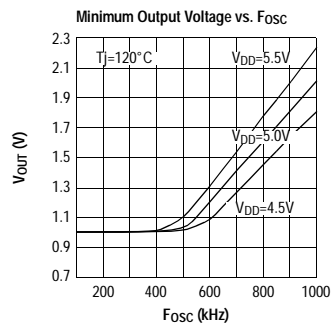
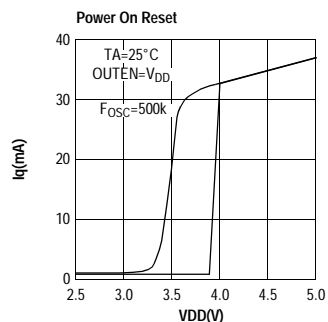
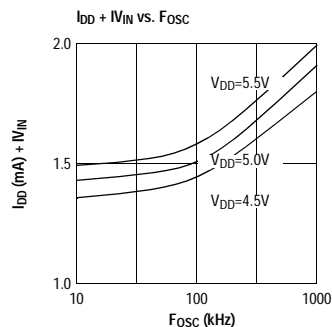
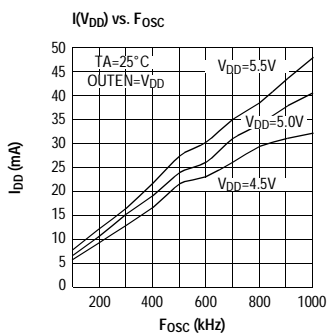
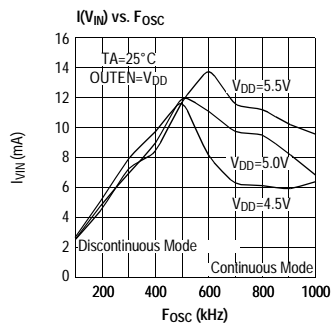
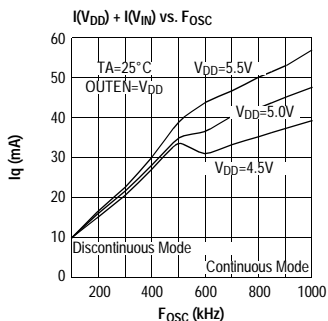
Typical Performance Curves



Line Regulation vs. CSLOPE $V_{IN}=V_{DD}=5.0V \pm 10\%$ **Load Regulation vs. CSLOPE** $I_{OUT}=3A, +3A, -2.5A$  **V_{OUT} vs. CSLOPE**
 $(V_{IN}=5.0V, I_{LOAD}=5A)$  **V_{OUT} Variation vs. Programmed Output Voltage ($V_{IDEAL}=(1+R3/R4)$)** **F_{OSC} vs. C_{OSC}**  **F_{OSC} vs. Temp**

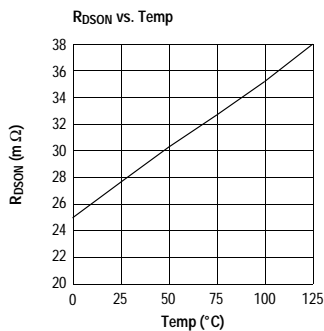
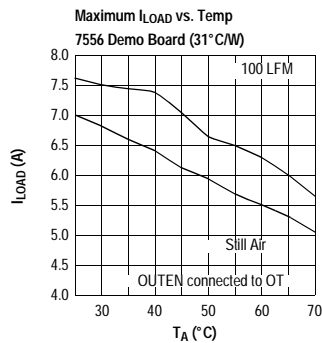
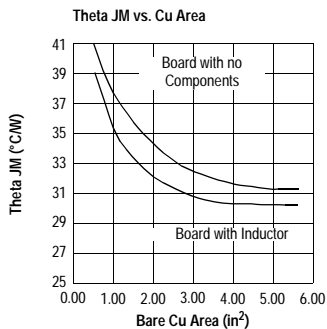
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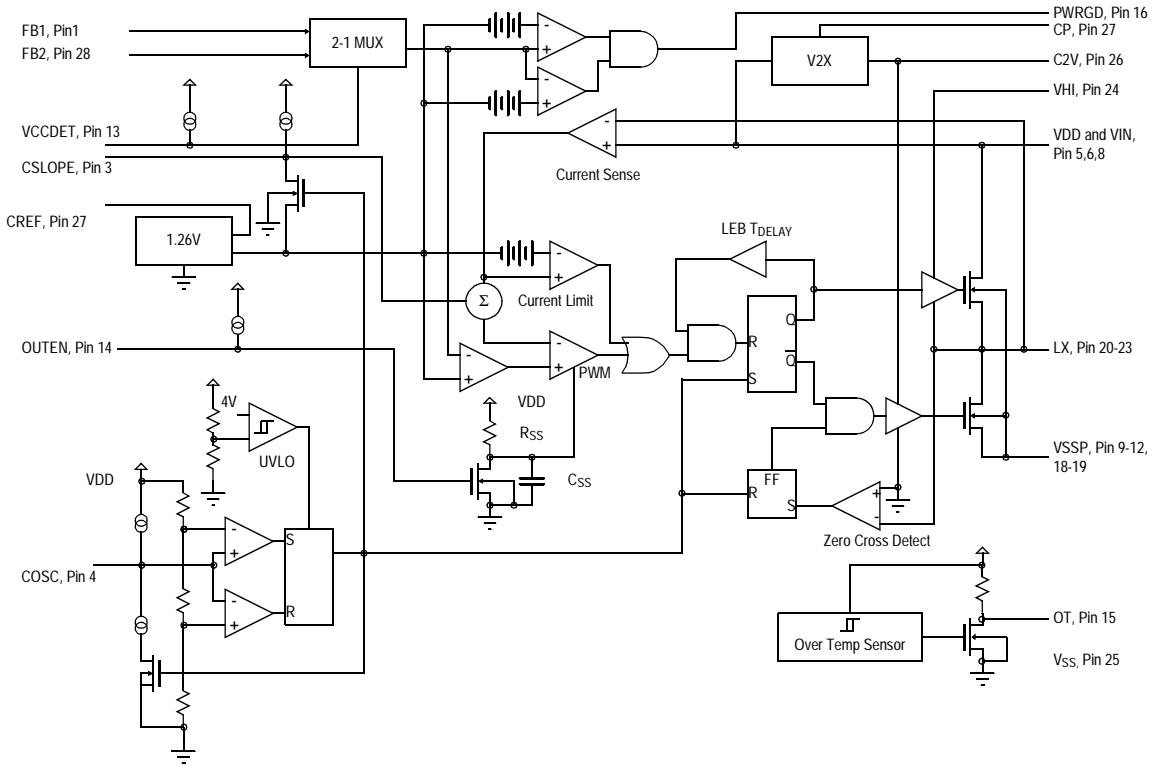
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Pin Description

(I=Input O=Output S=Supply)

Pin Number	Pin Name	Pin Type	Function
1	FB1	I	Voltage feedback pin for the buck regulator. Active when VCC2DET is logic low. Normally connected to external resistor divider between VOUT and GND. A 2μA pull-up current forces VOUT to VSS in the event that FB1 is floating and VCC2DET is inadvertently connected to GND.
2	CREF	I	Bandgap reference bypass capacitor. Typically 0.1μF to VSS.
3	CSLOPE	I	Slope compensation capacitor. Ramp width corresponds to LX duty cycle. CSLOPE to COSC ratio is normally 1:1.5.
4	COSC	I	Oscillator timing capacitor. FOSC(Hz) can be approximated by: FOSC(Hz)= 0.0001/COSC. COSC in Farads.
5	VDD	S	Power Supply for PWM control circuitry. Normally the same potential as VIN.
6	VIN	S	Power supply for the buck regulator. Connected to the drain of the high-side NMOS FET.
7	VSSP	S	Ground return for the buck regulator. Connected to the source of the low-side synchronous NMOS FET.
8	VIN	S	Same as pin 6.
9	VSSP	S	Same as pin 7.
10	VSSP	S	Same as pin 7.
11	VSSP	S	Same as pin 7.
12	VSSP	S	Same as pin 7.
13	VCC2DET	I	VCC2DET interface logic input. When driven to logic 1 VOUT=3.500V. When driven to logic 0 the PWM uses FB1 to determine VOUT: VOUT=1.0V*(1+R3/R4).
14	OUTEN	I	The switching regulator output is enabled when logic 1. The reference voltage output operates whenever the power supply is qualified (VDD>VPOR) regardless of the state of this pin.
15	OT	O	Over temperature indicator. Normally high. Pulls low when die temperature exceeds 135°C, returns to the high state when die temperature has cooled to 100°C.
16	PWRGD	O	Power good window comparator output. Logic 1 when regulator output is within ±10% of programmed voltage.
17	TEST	I	Test pin. Must be connected to VSSP in normal operation.
18	VSSP	S	Same as pin 7.
19	VSSP	S	Same as pin 7.
20	LX	O	Inductor drive pin. High current switching output whose average voltage equals the regulator output voltage.
21	LX	O	Same as pin 20.
22	LX	O	Same as pin 20
23	LX	O	Same as pin 20
24	VHI	I	Gate drive to high-side driver. Bootstrapped from LX with a 0.1μF capacitor.
25	VSS	S	Ground return for the control circuitry.
26	C2V	I	Connected to voltage doubler output. Supplies gate drive to the low-side driver.
27	CP	O	Drives the negative side of charge pump capacitor at one-half the oscillator frequency FOSC.
28	FB2	I	Voltage feedback pin. Active when VCC2DET is logic 1. Internally preset to VOUT=3.5V.

Block Diagram



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Applications Information

Circuit Description

General

The EL7556AC is a fixed frequency, current mode controlled DC:DC converter with integrated N-channel power MOSFETS and a high precision reference. The device incorporates all of the active circuitry required to implement a cost effective, user-programmable 6A synchronous buck converter suitable for use in CPU power supplies. By combining fused-lead packaging technology with an efficient synchronous switching architecture, high power outputs (21W) can be realized without the use of discrete external heat sinks.

Theory of Operation

The EL7556AC is composed of 7 major blocks:

1. PWM Controller
2. Output Voltage Mode Select
3. NMOS Power FETS and Drive Circuitry
4. Bandgap Reference
5. Oscillator
6. Temperature Sensor
7. Power Good and Power On Reset

PWM Controller

The EL7556AC regulates output voltage through the use of current-mode controlled pulse width modulation. The three main elements in a PWM controller are the feedback loop and reference, a pulse width modulator whose duty cycle is controlled by the feedback error signal, and a filter which averages the logic level modulator output. In a step-down (buck) converter, the feedback loop forces the time-averaged output of the modulator to equal the desired output voltage. Unlike pure voltage-mode control systems current-mode control utilizes dual feedback loops to provide both output voltage and inductor current information to the controller. The voltage loop minimizes DC and transient errors in the output voltage by adjusting the PWM duty-cycle in response to changes in line or load conditions. Since the output voltage is equal to the time-average of the modulator output

the relatively large LC time constants found in power supply applications generally results in low bandwidth and poor transient response. By directly monitoring changes in inductor current via a series sense resistor the controller's response time is not entirely limited by the output LC filter and can react more quickly to changes in line or load conditions. This feed-forward characteristic also simplifies AC loop compensation since it adds a zero to the overall loop response. Through proper selection of the current-feedback to voltage-feedback ratio, the overall loop response will approach a one pole system. The resulting system offers several advantages over traditional voltage control systems, including simpler loop compensation, pulse by pulse current limiting, rapid response to line variation and good load step response.

The heart of the controller is a triple-input direct summing comparator which sums voltage feedback, current feedback and slope compensating ramp signals together. Slope compensation is required to prevent system instability which occurs in current-mode topologies operating at duty-cycles greater than 50% and is also used to define the open-loop gain of the overall system. The compensation ramp amplitude is user adjustable and is set using a single external capacitor (CSLOPE). Each comparator input is weighted and determines the load and line regulation characteristics of the system. Current feedback is measured by sensing the inductor current flowing through the high-side switch whenever it is conducting. At the beginning of each oscillator period the high-side NMOS switch is turned on and CSLOPE ramps positively from its reset state (VREF potential). The comparator inputs are gated off for a minimum period of time (LEB) after the high-side switch is turned on to allow the system to settle. The Leading Edge Blanking (LEB) period prevents the detection of erroneous voltages at the comparator inputs due to switching noise. When programming low regulator output voltages the LEB delay will limit the maximum operating frequency of the circuit since the LEB will result in a minimum duty-cycle regardless of the PWM error voltage. This relationship is shown in the performance curves. If the inductor current exceeds the maximum current limit (I_{LMAX}), a secondary over-current com-

parator will terminate the high-side switch. If I_{LMAX} has not been reached, the regulator output voltage is then compared to the reference voltage V_{REF} . The resultant error voltage is summed with the current feedback and slope compensation ramp. The high-side switch remains on until all three comparator inputs have summed to zero, at which time the high-side switch is turned off and the low-side switch is turned on. In order to eliminate cross-conduction of the high-side and low-side switches a 10ns break-before-make delay is incorporated in the switch driver circuitry. In the continuous mode of operation the low-side switch will remain on until the end of the oscillator period. In order to improve the low current efficiency of the EL7556AC, a zero-crossing comparator senses when the inductor transitions through zero. Turning off the low-side switch at zero inductor current prevents forward conduction through the internal clamping diodes (LX to VSSP) when the low-side switch turns off, reducing power dissipation. The output enable (OUTEN) input allows the regulator output to be disabled by an external logic control signal.

Output Voltage Mode Select

The VCC2DET multiplexes the FB1 and FB2 pins to the PWM controller. A logic 1 on VCC2DET selects the FB2 input and forces the output voltage to the internally programmed value of 3.50V. A logic zero on VCC2DET selects FB1 and allows the output to be programmed from 1.0 to 3.8V. In general:

$$V_{out} = 1.0V (1 + R3/R4) \text{ Volt.}$$

However, due to the relatively low open loop gain of the system, gain errors will occur as the output voltage and loop-gain are changed. This is shown in the performance curves. (The output voltage is factory trimmed to minimize error at a 2.50V output). A 2uA pull-up current from FB1 to VIN forces VOUT to GND in the event that FB1 is not used and the VCC2DET is inadvertently toggled between the internal and external feedback mode of operation.

NMOS Power FETS and Drive Circuitry

The EL7556AC integrates low resistance (25mΩ) NMOS FETS to achieve high efficiency at 6A. Gate drive for both the high-side and low-side switches is derived through a charge pump consisting of the CP pin

and external components D1-D3 and C5-C6. The CP output is a low resistance inverter driven at one-half the oscillator frequency. This is used in conjunction with D2-D3 to generate a 7.5V (typical) voltage on the C2V pin which provides gate drive to the low-side NMOS switch and associated level shifter. In order to use an NMOS switch for the high-side drive it is necessary to drive the gate voltage above the source voltage (LX). This is accomplished by boot-strapping the VHI pin above the C2V voltage with capacitor C6 and diode D1. When the low-side switch is turned on the LX voltage is close to GND potential and capacitor C6 is charged through diodes D1-D3 to approximately 6.9V. At the beginning of the next cycle the high side switch turns on and the LX pin begins to rise from GND to VDD potential. As the LX pin rises the positive plate of capacitor C6 follows and eventually reaches a value of approximately 11.2V, for VDD=5V. This voltage is then level shifted and used to drive the gate of the high-side FET, via the VHI pin.

Reference

A 1% temperature compensated band gap reference is integrated in the EL7556AC. The external CREF capacitor acts as the dominant pole of the amplifier and can be increased in size to maximize transient noise rejection. A value of 0.1uF is recommended.

Oscillator

The system clock is generated by an internal relaxation oscillator with a maximum duty-cycle of approximately 96%. Operating frequency can be adjusted through the COSC pin or can be driven by an external clock source. If the oscillator is driven by an external source, care must be taken in the selection of CSLOPE. Since the COSC and CSLOPE values determine the open loop gain of the system, changes to COSC require corresponding changes to CSLOPE in order to maintain a constant gain ratio. The recommended ratio of COSC to CSLOPE is 1.5:1

Temperature Sensor

An internal temperature sensor continuously monitors die temperature. In the event that die temperature exceeds the thermal trip-point, the OT pin will output a logic 0. The upper and lower trip points are set to 135 °C

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and 100 °C respectively. To enable thermal shutdown this pin should be tied directly to OUTEN. Use of this feature is recommended during normal operation

Power Good and Power On Reset

During power up the output regulator will be disabled until VIN reaches a value of approximately 4.0V. Approximately 500mV of hysteresis is present to eliminate noise induced oscillations.

Under-voltage and over-voltage conditions on the regulator output are detected through an internal window comparator. A logic 1 on the PWRGD output indicates that regulated output voltage is within $\pm 10\%$ of the nominally programmed output voltage. Although small, the typical values of the PWRGD threshold will vary with changes to external feedback (and resultant loop gain) of the system. This dependence is shown in the typical performance curves.

Thermal Management

The EL7556AC utilizes fused-lead packaging technology in conjunction with the system board layout to achieve a lower thermal resistance than typically found in standard 28 lead SOIC packages. By fusing multiple leads to the die substrate thermal energy flows through a thermally conductive path (metal) instead of thermally resistive plastic. After conducting heat from the die to the leads, heat transfer occurs by convection. If a sufficient amount of metal area is connected to the package leads a junction-to-ambient resistance of 31°C/W can be achieved compared to 100 °C/W found in standard packages. The general relationship between board area and thermal resistance for this package is shown in the performance curves. It can be readily seen that the thermal resistance approaches an asymptotic value of approximately 31°C/W. Additional information can be found in Application Note #8 (Measuring the Thermal Resistance of Power Surface-Mount Packages), and Application Note #13 (EL75XX Thermal Design Considerations).

If the thermal shutdown pin is connected to OUTEN the IC will enter thermal shutdown when the maximum junction temperature is reached. For a thermal shutdown of 135°C and power dissipation of 2.2W the ambient temperature is limited to a maximum value of 67°C (typical). The ambient temperature range can be extended

with the application of air flow. For example, the addition of 100LFM reduces the thermal resistance by approximately 15% and can extend the operating ambient to 77°C (typical). Since the thermal performance of the IC is heavily dependent on the board layout, the system designer should exercise care during the design phase to ensure that the IC will operate under the worst-case environmental conditions.

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General Disclaimer

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